## US-411 Intersections APPLE Study Advance Planning Report

 RPC Project. No. 1289.45November 2022


Prepared For: The City of Moody, St. Clair County,
Regional Planning Commission of Greater Birmingham

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## Executive Summary

## Study Initiation and Study Area

This study was initiated by the City of Moody and St. Clair County through the Advanced Planning, Programming, and Logical Engineering (APPLE) program developed by the Regional Planning Commission of Greater Birmingham (RPCGB). The City and the County requested professional planning assistance in evaluating the feasibility of improvements at the unsignalized intersections along US-411 from Avalon Drive to Stuart Drive and Coupland Road. Ten intersections were evaluated as a part of this study:

- US-411 at Avalon Drive
- US-411 at Washington Drive and Verbena Drive
- US-411 at Robbie Drive
- US-411 at James Taylor Road
- US-411 at High School Drive
- US-411 at Valleybend Lane
- US-411 at Lake Joyce Road
- US-411 at Myers Road and Church Road
- US-411 at Bethel Road
- US-411 at Stuart Drive and Coupland Road

US-411 at Kerr Road was previously studied and selected for an Alabama Transportation Rehabilitation and Improvement Program-II (ATRIP-II) project during the Fiscal Year 2022 cycle; therefore, the Kerr Road intersection was not included in this study effort.

## Purpose of the Study

This study was undertaken to assess the feasibility of improving traffic operations at unsignalized intersections along US-411. This Advance Planning Report includes:

- The process used to identify potential improvement options,
- The resulting improvement options that were developed from that process, and
- An evaluation of potential positive and negative impacts to the area and adjacent properties that may be associated with each potential improvement.

If the City or County chooses to move forward with an improvement project for the area, a more detailed Environmental Planning Study would be required for federally funded projects.

## Improvement Recommendations

Based upon feedback from stakeholders, traffic operations analysis, crash data trends, and field review, the following recommendations have been identified at the study intersections:

- US-411 at Avalon Drive
- Install Northbound Left Turn Lane on US-411.
- US-411 at Washington Drive and Verbena Drive
- Install traffic signal.
- Install Northbound Left Turn Lane on US-411.
- Install Northbound Right Turn Lane on US-411.
- Install Southbound Left Turn Lane on US-411.
- Close access on US-411 south of Verbena Drive.
- US-411 at Robbie Drive
- Install Northbound Left Turn Lane on US-411.
- US-411 at James Taylor Road
- Install Northbound Left Turn Lane on US-411.
- Install Southbound Right Turn Lane on US-411.
- US-41 1 at High School Drive
- Install traffic signal.
- Restripe High School Drive approach.
- Extend southbound left turn lane on US-411.
- US-411 at Valleybend Lane
- No recommendations
- US-411 at Lake Joyce Road
- Install Northbound Left Turn Lane on US-411.
- US-411 at Myers Road and Church Road
- Install Northbound Left Turn Lane on US-411.
- US-411 at Bethel Road
- Cul-de-sac Bethel Road.
- US-411 at Stuart Drive and Coupland Road - Install Northbound Left Turn Lane on US-411.

Additional information regarding the prioritization of recommended improvements can be found in Section 5.2. A total shoulder width of 8 feet, with 4 feet of paved shoulder and 4 feet of grass shoulder, should be included with any turn lane installation on US-411.

## Stakeholder Involvement

A project kickoff meeting was held at Moody City Hall on April 19, 2022. Representatives from the City, the County, RPCGB, and Sain Associates attended the meeting. Stakeholders discussed project background, identified study priorities, and determined expectations for the scope of the study. Out of ten study intersections along US-411, the City identified three priority intersections to study in greater detail: Washington Drive and Verbena Drive, James Taylor Road, and High School Drive.

Another meeting was conducted on July 27, 2022, to discuss preliminary improvement recommendations. Representatives from the City, the County, RPCGB, and Sain Associates were in attendance. Stakeholders reviewed the proposed improvement recommendations and provided feedback to the project team prior to the submission of the report.

## Next Steps

This report documents the study undertaken to further evaluate the traffic operations at ten (10) unsignalized intersections along US-411 from Avalon Drive to Stuart Drive and Coupland Road. In previous sections of this report, transportation analysis and improvement recommendations have been provided.

If the City and the County choose to move forward with implementing any of the recommended improvements using state funding, the next step would be to apply for Fiscal Year 2023 ATRIP-II funding. The application deadline for Fiscal Year 2023 ATRIP-II funding is November 18, 2022. Most recommended improvements, which include the installation of turn lanes to mitigate reported crash trends, could also be eligible for HSIP funding.

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Sources
City of Moody
St. Clair County
Regional Planning Commission of Greater Birmingham (RPCGB)
Alabama Department of Transportation (ALDOT)
Corridor Feasibility Study for Multilane Facility on SR-25 (US-411) - (2018)
Federal Highway Administration (FHWA)
Google Maps
National Cooperative Highway Research Program (NCHRP)
Quality Counts, LLC
Skipper Consulting - Traffic Signal Warrant Assessment Technical Memorandum (2018)
St. Clair County Safety Study - US-4 11 at Kerr Road (2021)
Transportation Research Board (TRB)
University of Alabama Center for Advanced Public Safety (CAPS)
US-4 11 from CR-10 (Park Avenue) to Kerr Road APPLE Study (2015)

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## 1 Introduction

This study was initiated by the City of Moody and the Regional Planning Commission of Greater Birmingham (RPCGB) through the Advanced Planning, Programming, and Logical Engineering (APPLE) program developed by the RPCGB. Sain Associates was tasked with analyzing existing and future traffic operations at ten (10) unsignalized intersections along US-411 from Avalon Drive to Stuart Drive and Coupland Road.

The purpose of this document is to summarize existing traffic operational conditions and deficiencies at the study intersections. The City has experienced significant development, resulting in additional strain on the transportation system. Following this document, an Advanced Planning Report will be prepared that will include the process used to identify potential improvement options, the resulting improvement options that were developed from that process, and an evaluation of potential impacts associated with each improvement.

The study area is along US-411 in western St. Clair County, just north of Interstate 20, between the cities of Moody and Odenville. The study area is illustrated in Figure 1.

## 2 Existing Conditions

Within St. Clair County, US-411 serves as the main artery connecting the cities of Moody and Odenville to Interstate 20. According to the 2020 Census, the population of Moody is 13,170 and the population of St. Clair County is 91,103 . Since 2010, this equates to a $12 \%$ increase in population for the City and a $9 \%$ increase in population for the County, which ranks in the top ten among all Alabama counties.

The study intersections begin with Avalon Drive and end with Stuart Drive and Coupland Road. Land use adjacent to the study area is primarily residential and commercial. Most land uses have direct access to US-411.

US-411 is considered a rural minor arterial with a two-lane cross section within the study area. The posted speed limit on US-411 is 50 MPH from Avalon Drive to Lake Joyce Road and 55 MPH from Myers Road and Church Road to Stuart Drive and Coupland Drive. A flashing beacon is located at High School Drive, near the center of the study area. All other intersections are twoway stop controlled, with the stop sign on the minor street approach. Table 1 identifies the speed limit, functional classification, and typical sections of notable side streets along the US-411 corridor.


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Table 1: Notable Study Area Side Street Characteristics

| Side Street | Speed Limit | Functional Classification | Typical Section |
| :---: | :---: | :---: | :---: |
| Avalon Drive | 20 MPH | Local Road | Two-Lane |
| Washington Drive | 20 MPH | Local Road | Two-Lane |
| Verbena Drive | 20 MPH | Local Road | Two-Lane |
| Robbie Drive | 25 MPH | Local Road | Two-Lane |
| James Taylor Road | 35 MPH | Local Road | Two-Lane |
| High School Drive | Not Posted | Local Road | Two-Lane |
| Valleybend Lane | 25 MPH | Local Road | Two-Lane |
| Lake Joyce Road | 25 MPH | Local Road | Two-Lane |
| Myers Road | 20 MPH | Local Road | Two-Lane |
| Church Road | Not Posted | Local Road | Two-Lane |
| Bethel Road | Not Posted | Local Road | Two-Lane |
| Stuart Drive | Not Posted | Local Road | Two-Lane |
| Coupland Road | Not Posted | Local Road | Two-Lane |

### 2.1 Existing Documents and Adjacent Projects

## APPLE Study - US-411 from CR-10 (Park Avenue) to Kerr Road

RPCGB Project No. 1289.05
Completed by Sain Associates in February 2015, the study was performed to determine the feasibility of improvements to a three-mile segment of US-411 between Park Avenue and Kerr Road. At the time of the study, several residential subdivisions were being developed in the area surrounding the study corridor. The additional traffic volumes generated by these developments resulted in more traffic congestion along US-411, especially at intersections. Among reported crashes, the data indicated a high rate of rear-end collisions.

Several potential improvements were identified for the area. The study did not select a preferred alternative; however, the recommended improvements were listed in priority order based on traffic volumes, crash history, field observations, and expected ease of implementation. The following improvements apply to current study intersections:

1. Install a right turn lane on US-411 northbound at Verbena Drive
2. Install a left turn lane on US-411 northbound at Lake Joyce Road.
3. Install a left turn lane on US-411 northbound at Washington Drive.
4. Install a right turn lane on US-411 southbound at James Taylor Road.
5. Consider widening US-411 from two lanes to a five-lane typical section.

Additional recommendations were provided without consideration for implementation priority:

- Maintain the officers directing traffic at school intersections.
- Conduct a school circulation study for the three schools located on High School Drive.
- Consider requiring traffic impact studies for all future developments in conformance with ALDOT's Access Management Manual.
- Turn lanes along Washington Drive and Verbena Drive may be needed as more properties develop in the adjacent neighborhoods. The developer should be required to perform a traffic impact study. If the study finds that turn lanes are warranted, the developer should be required to install them.


## Corridor Feasibility Study for Multilane Facility on SR-25 (US-411) from Park Avenue to Sanie Road

 ALDOT Project STPAA-0025(549)The Corridor Feasibility Study was completed by Sain Associates in November 2018. The purpose of the study was to determine the feasibility of widening the three-mile section of US-411 between Park Avenue and Sanie Road to provide four travel lanes. The evaluated improvements were aimed at increasing the capacity of US-411 and improving traffic operations along the corridor.

Potential improvements were listed by intersection with no assigned level of priority. The following improvement options apply to current study intersections:

- Avalon Drive
- Install a left turn lane on US-411 northbound at Avalon Drive.
- Washington Drive/Verbena Drive
- Install left and right turn lanes on both US-411 approaches.
- Robbie Drive
- Install a left turn lane on US-411 northbound to Robbie Drive.
- James Taylor Road
- Install a left turn lane on US-411 northbound at James Taylor Road.
- Myers Road/Church Road
- Install left and right turn lanes on both US-411 approaches.
- Bethel Road
- Realign Bethel Road approach to intersect with US-411 at closer to a 90-degree angle.
- Stuart Drive/Coupland Road
- Install a left turn lane on US-411 northbound at Stuart Drive.

The study also recommended widening US-411 to a five-lane typical section between Park Avenue and Sanie Road, but the project did not gain momentum within ALDOT and lacks funding for the foreseeable future.

## US-411 at CR-10 (Park Avenue) and Sanie Road Design Projects

ALDOT Project CMAQ-0025(559)
Improvements are recommended at the intersections of US-411 at Park Avenue and US-411 at Sanie Road. Intersection improvements at Park Avenue include an eastbound left turn lane, an eastbound right turn lane, and a westbound left turn lane. Intersection improvements at Sanie Road include a northbound left turn lane, a southbound left turn lane, the extension of the eastbound right turn lane to 450 feet with a 100 -foot taper, and channelized right turn striping with yield signs. As of June 2022, this project is in the design stage.

## ATRIP II Project - US-411 at Kerr Road

## ALDOT Project ATRP2-58-2022-058

In 2021, Sain Associates conducted a safety APPLE study at the intersection of US-411 and Kerr Road and assisted the County in applying for funding. St. Clair County was awarded Alabama Transportation Rehabilitation Improvement Program (ATRIP-II) funds to construct the project. Improvements at this intersection include the installation of a southbound left turn lane onto US411 and reconfiguring Kerr Road as a two-lane approach. During the field visit for the US-411 project, conducted on May 12, 2022, significant northbound and southbound queues were
observed near Kerr Road during the AM peak hour. The ATRIP project is expected to address queuing issues near Kerr Road; therefore, Kerr Road is excluded from the current US-411 APPLE study. As of June 2022, the Kerr Road project is in the design stage.

### 2.2 Data Collection

On behalf of Sain Associates, Quality Counts, LLC performed traffic data collection within the study area on Wednesday, May 4, 2022. Weekday peak hour turning movement counts were collected during the periods of 7:00 AM to 9:00 AM and 4:00 PM to 6:00 PM at the following intersections:

- US-411 at Avalon Drive
- US-411 at Robbie Drive
- US-411 at James Taylor Road
- US-411 at Myers Road/Church Road
- US-411 at Stuart Drive/Coupland Road
- US-411 at Lake Joyce Road
- US-411 at Valleybend Lane
- US-411 at Bethel Road

Weekday 14-hour turning movement counts were collected from 6:00 AM to 8:00 PM on Wednesday, May 4, 2022, at the following intersections:

- US-411 at Washington Drive/Verbena Drive
- US-411 at High School Drive

The existing peak hour turning movement volumes are illustrated in Figure 2-3.
Weekday 24-hour tube counts, including speed and vehicle classification data, were collected on Wednesday, May 4, 2022, at the following locations:

- US-411 approximately 1200 feet south of James Taylor Road
- ADT = 12,899
- $85^{\text {th }}$ Percentile Speed $=56 \mathrm{MPH}$
- Heavy Vehicle Percentage $=2.5 \%$
- US-41 1 approximately 400 feet north of Bethel Road
- ADT $=14,656$
- $85^{\text {th }}$ Percentile Speed $=56 \mathrm{MPH}$
- Heavy Vehicle Percentage $=1.4 \%$

The raw traffic data can be found in Appendix A.

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Figure 2: Existing Peak Hour Traffic Volumes


Figure 3: Existing Peak Hour Traffic Volumes - Continued

### 2.3 Field Review

Field reviews were performed on Wednesday, May 11, 2022, from 4:00 PM to 6:00 PM and Thursday, May 12, 2022, from 7:00 AM to 9:00 AM. Particular attention was paid to Washington Drive/Verbena Drive and High School Drive, as signal warrants were analyzed at these intersections. During the AM peak hour, traffic flow was heaviest in the southbound direction toward Birmingham. Traffic had noticeably dwindled by approximately 7:45 AM, and even more so by 8:00 AM. Traffic volumes were heaviest in the northbound direction during the PM peak hour.

Overall, motorists entering US-411 from a side street approach experience extended delays before an acceptable gap in traffic occurs. It is common for a driver exiting US-411 to allow another motorist exiting the side street to complete their turn, despite having the right-of-way. Familiar drivers know how difficult it is to find acceptable gaps in traffic during peak hours. Vehicle platoons form in the northbound direction on US-411 closer to Park Avenue during the PM peak hour, which causes unacceptable delays for drivers exiting Verbena Drive and Washington Drive and other side streets. Northbound platoons tend to dissipate over the course of the three-mile segment of US-411 from Park Avenue to Sanie Road, creating more frequent acceptable gaps for drivers entering from side streets.

## US-411 at Avalon Drive

Avalon Drive at US-411 is a three-leg, side-street stop-controlled intersection. The speed limit on Avalon Drive is 20 MPH . It provides access to a Dollar General and the Avalon residential subdivision. Avalon Drive connects to Washington Drive through this subdivision, thereby splitting the volume of traffic from the subdivision between two access connections onto US-411. During the AM peak hour, the southbound queue on US-411 backed up past the Dollar General due to a vehicle making a southbound left turn at Avalon Drive.

Photos 1 and 2 show views of US-411 from the Avalon Drive approach.


Photo 1: Looking Northbound along US-411 from Avalon Drive


Photo 2: Looking Southbound along US-411 from Avalon Drive

## US-411 at Washington Drive and Verbena Drive

This is a four-leg, side-street stop-controlled intersection. The speed limits on both Washington Drive and Verbena Drive are 20 MPH . Verbena Drive provides access to a gas station, a gym, and The Arbors residential subdivision, which contains approximately 165 homes at the time of this study. Avalon Drive connects to Washington Drive through the Avalon subdivision, which contains approximately 310 homes at the time of this study. The westbound left turning movement from Verbena Drive is the movement with the highest delay during peak hours. A sample of westbound left turning vehicles in the AM peak hour observed delays between 20 and 30 seconds per vehicle. A sample of PM peak hour observed delays were often up to 120 seconds of delay per vehicle.

Photos 3-6 show several views from the intersection.


Photo 3: Washington Drive Approach to US-411


Photo 5: Verbena Drive Approach to US-411


Photo 4: Looking Southbound along US-411 from Washington Drive


Photo 6: Looking Northbound along US-411 from Verbena Drive

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## US-411 at Robbie Drive

Robbie Drive at US-411 is a three-leg, side-street stop-controlled intersection. The speed limit on Robbie Drive is 25 MPH. Adjacent land uses include a Tractor Supply and a storage facility. Robbie Drive connects to James Taylor Road approximately 0.5 miles from US-411. Per the City, World Victory Church has purchased a 15-acre parcel on the northwest corner of the intersection. Photos 7 and 8 show views of US-411 from the Robbie Drive approach.


Photo 7: Looking Northbound along US-411 from Avalon Drive


Photo 8: Looking Southbound along US-411 from Avalon Drive

## US-411 at James Taylor Road

James Taylor Road at US-411 is a three-leg, side-street stop-controlled intersection. The speed limit on James Taylor Road is 35 MPH . Adjacent land use is primarily residential. James Taylor Road has a sharp horizontal curve on its approach to the US-411 intersection, but it does intersect at approximately 90 degrees which is preferable to a skewed approach. Photos 9 and 10 show views of US-411 from the James Taylor Road approach.


Photo 9: Looking Northbound along US-41 1 from James Taylor Road


Photo 10: Looking Southbound along US-411 from James Taylor Road

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## US-411 at High School Drive

US-411 at High School Drive is a three-leg, side-street stop-controlled intersection providing access to Moody High School, Moody Middle School, and Moody Junior High School. During the school peak hours at the US-411 intersection with High School Drive, a police officer was directing traffic. The officer would routinely stop US-411 traffic in both directions to allow motorists to exit High School Drive as students were dropped off and picked up on campus. When traffic was stopped on US-411, queveing occurred on the southbound approach of US-411. Despite queuing, the current strategy seemed to be effective in moving traffic on and off of school property. The striping on High School Drive is faded and in poor condition.

A northbound right turn lane and a southbound left turn lane exist on US-411 at High School Drive, and there is a flashing beacon installed at the intersection.

Photo 11 shows the High School Drive approach to US-411.


Photo 11: High School Drive Approach to US-411

## US-411 at Valleybend Lane

Valleybend Lane at US-411 is a three-leg, side-street stop-controlled intersection. The speed limit on Valleybend Lane is 25 MPH . Valleybend Lane serves as the entrance to the Spring Valley Estates neighborhood. This intersection is 670 feet north of High School Drive and within the taper for the southbound left turn lane into High School Drive. The cross-sectional width of the roadway is 36 feet at this location.

Photo 12 shows a view from the Valleybend Lane approach.

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Photo 12: Valleybend Lane Approach to US-411

## US-411 at Lake Joyce Road

Lake Joyce Road at US-411 is a three-leg, side-street stop-controlled intersection. The speed limit on Lake Joyce Road is 25 MPH. Lake Joyce Road provides access to a residential subdivision of single-family homes and Grace Valley Church.

Photos 13 and 14 show views of US-411 from the Lake Joyce Road approach.


## US-411 at Myers Road \& Church Road

This is a four-leg, two-way stop-controlled intersection. The speed limit on Myers Road is 20 MPH, and the speed limit on Church Road is not posted. Bethel Baptist Church is located on Church Road. Other nearby land uses are residential. Church Road also connects to Bethel Road, near the church entrance. During the AM peak hour, a southbound queue backed up from Kerr Road to Church Road ( 0.5 miles). Although the volume on Myers Road is low, there are several open tracts of land nearby, which could be developed in the future.

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Photos 15-18 show views around the intersection of US-411 at Myers Road and Church Road.


Photo 15: Looking Northbound along US-411 from Myers Road


Photo 17: View of SB Queue from Kerr Road to Church Road


Photo 16: View of Church Road from US-411


Photo 18: Looking Southbound along US-411 from Church Road

## US-411 at Bethel Road

Bethel Road at US-41 1 is a three-leg, side-street stop-controlled intersection. The speed limit on Bethel Road is not posted. Adjacent land use is primarily single-family residential. Bethel Road connects to Church Road near the entrance of Bethel Baptist Church. Bethel Road also has a skewed approach angle near the stop sign at US-411. The stop bar is 42 feet away from the stop sign, and a residential driveway and mailbox are located between them. The longest observed queue reached Bethel Road from Kerr Road during the AM peak hour, approximately 1.5 miles to the north of Kerr Road.

Photos 19 and 20 show views of US-411 from Bethel Drive.


Photo 19: Looking Northbound Along US-411 from Bethel Road


Photo 20: View of Bethel Road Approach to US-411

## US-411 at Stuart Drive \& Coupland Road

This is a four-leg, two-way stop-controlled intersection. There are no posted speed limits on either side street. Adjacent land use is residential and commercial. There are several tracts of open land nearby which could be developed in the future. Photo 21-24 show views of the intersection.


Photo 21: Coupland Road Approach to US-411


Photo 23: Looking Southbound along US-411 from Stuart Drive


Photo 22: Stuart Drive Approach to US-411


Photo 24: Looking Northbound along US-411 from Coupland Road

### 2.4 Existing Conditions Capacity Analysis

Using the methods described in the Transportation Research Board's Highway Capacity Manual, Sain Associates analyzed the existing traffic conditions within the study area. According to this method of analysis, traffic capacities are expressed as levels of service (LOS) ranging from "A" (free-flow conditions) to "F" (very congested conditions). A detailed description of each LOS designation is included in Appendix B. Generally, LOS " C " is considered desirable, while LOS " D " is considered acceptable during peak hours of traffic flow. The analysis was conducted using Trafficware's Synchro 10 software.

The results of the existing conditions capacity analysis are summarized in Table 2 and Table 3. Full printouts are provided in Appendix C.

Table 2: Existing Levels of Service

| Intersection | Approach |  | Level of Service |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  | AM Peak | PM Peak |
| Avalon Drive at US-411 <br> (Unsignalized) | EB | Avalon Drive | E | D |
|  | NB | US-411 | A | A |
|  | SB | US-411 | A | A |
| Washington <br> Drive/Verbena Drive at US-411 <br> (Unsignalized) | EB | Washington Drive | F | D |
|  | WB | Verbena Drive | F | F |
|  | NB | US-411 | A | A |
|  | SB | US-411 | A | A |
| Robbie Drive at US-411 <br> (Unsignalized) | EB | Robbie Drive | C | B |
|  | NB | US-411 | A | A |
|  | SB | US-411 | A | A |
| James Taylor Road at US-411 <br> (Unsignalized) | EB | James Taylor Road | F | D |
|  | NB | US-411 | A | A |
|  | SB | US-411 | A | A |
| High School Drive at US-411 <br> (Unsignalized) | WB | High School Drive | F | D |
|  | NB | US-411 | A | A |
|  | SB | US-411 | A | A |
| Valleybend Lane at US-411 <br> (Unsignalized) | EB | Valleybend Lane | C | B |
|  | NB | US-411 | A | A |
|  | SB | US-411 | A | A |

[^0]Table 3: Existing Levels of Service (Continued)

| Intersection |  | Approach | Level of Service |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  | AM Peak | PM Peak |
| Lake Joyce Road at US-411 (Unsignalized) | EB | Lake Joyce Road | C | C |
|  | NB | US-411 | A | A |
|  | SB | US-411 | A | A |
| Myers Road/Church Road at US-411 (Unsignalized) | EB | Myers Road | C | C |
|  | WB | Church Road | E | D |
|  | NB | US-411 | A | A |
|  | SB | US-411 | A | A |
| Bethel Road at US-411 (Unsignalized) | WB | Bethel Road | C | C |
|  | NB | US-411 | A | A |
|  | SB | US-411 | A | A |
| Stuart Drive/ Coupland Road at US-411 <br> (Unsignalized) | EB | Stuart Drive | D | C |
|  | WB | Coupland Road | F | E |
|  | NB | US-411 | A | A |
|  | SB | US-411 | A | A |

As shown in the tables above, the US-411 intersections with Robbie Drive, Valleybend Lane, Lake Joyce Road, and Bethel Road operate at acceptable levels of service. Several intersection approaches to US-411 have unacceptable levels of service (LOS E or F):

- Avalon Drive - LOS E during the AM peak hour.
- Washington Drive - LOS F during the AM peak hour.
- Verbena Drive - LOS F during both the AM and PM peak hours.
- James Taylor Road - LOS F during the AM peak hour.
- High School Drive - LOS F during the AM peak hour. Note that a police officer is posted at this intersection during the AM peak hour, so the Synchro software does not account for this.
- Church Road - LOS E during the AM peak hour.
- Coupland Road - LOS F during the Am peak hour and an LOS E during the PM peak hour.

In general, traffic volumes and delays are higher near the Park Avenue intersection. On highvolume roadways, it is not uncommon for unsignalized approaches to have a poor or failing LOS without needing signalization. Signalization is typically not considered a solution to this unless side-street approach volumes are considerable. This is the case for the US-411 intersections with Washington Drive/Verbena Drive and High School Drive, and signal warrant evaluations were performed at the two intersections. The results are summarized in Section 2.7 of this report.

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### 2.5 Crash Data Analysis

The information presented in this section is exempt from open records, discovery or admission under Alabama Law and 23 U.S.C. §§ 148(h)(4) and 409). The collection of safety data is encouraged to actively address safety issues on regional, local, and site-specific levels. Congress has laws, 23 U.S.C. § 148(h)(4) and 23 U.S.C. § 409 which prohibit the production under open records and the discovery or admission of crash and safety data from being admitted into evidence in a Federal or state court proceeding. This document contains text, charts, tables, graphs, lists, and diagrams for the purpose of identifying and evaluating safety enhancements in the project area. These materials are protected under 23 U.S.C. $\S 409$ and 23 U.S.C. § $148(\mathrm{~h})(4)$. In addition, the Supreme Court in Ex parte Alabama Dept. of Trans., 757 So. $2 d 371$ (Ala. 1999) found that these are sensitive materials exempt from the Alabama Open Records Act.

Crashes are to some degree random events; therefore, crash frequencies naturally fluctuate over time at a given site. This randomness indicates that short-term crash frequencies alone are not a reliable estimator of long-term crash frequency. The crash fluctuation over time makes it difficult to determine whether changes in the observed crash frequency are due to changes in site conditions or are due to natural fluctuations. When a period with high crash frequency is observed, it is statistically probable that the following period will have low crash frequency. This tendency is known as regression-to-the-mean (RTM). Not accounting for the effects of RTM introduces the potential for "RTM bias" (Refer to the Highway Safety Manual for more information).

Crash data for this analysis was provided by the Regional Planning Commission of Greater Birmingham (RPCGB). Data included crash information from January 2017 to December 2021 from the Critical Analysis Reporting Environment (CARE) database maintained by the Center for Advanced Public Safety (CAPS) at The University of Alabama. The data is summarized as follows:

- One hundred seventy-seven (177) total crashes reported,
- Two (2) fatal crashes,
- Six (6) incapacitating injury crashes,
- Twelve (12) non-incapacitating injury crashes,
- Nineteen (19) possible injury crashes, and
- One hundred thirty-six (136) property damage only crashes.
- Two (2) crashes reported no crash severity.

The majority of reported crashes in the dataset involved rear-end collisions, which are typically low-severity crashes. This pattern is common for high-volume roadways such as US-411 with an absence of turn lanes.

Figure 4 illustrates the breakdown of the crash data by collision type.


Figure 4: Crash Data Breakdown by Collision Type
Figure 5 illustrates the breakdown of the crash data by severity.


Figure 5: Crash Data Breakdown by Severity

### 2.6 Existing Turn Lane Warrant Analysis

Utilizing the information contained in NCHRP Report 457, Sain Associates conducted a turn lane warrant analysis under existing conditions at the study intersections. The posted speed limit on US-411 is 50 MPH from Avalon Drive to Lake Joyce Road and 55 MPH from Myers Road and Church Road to Stuart Drive and Coupland Drive.

Satisfaction of a turn lane warrant by volume does not necessarily justify the installation of a turn lane. Recommendation of a turn lane can also be based on traffic safety considerations and observed crash data trends.

Without any growth in traffic volumes or additional development, the following locations satisfy the warrant-by-volume thresholds for the installation of a turn lane during AM and PM peak hours:

- Avalon Drive at US-411
- Northbound Left Turn Lane
- Washington Drive/Verbena Drive at US-411
- Northbound Right Turn Lane
- Northbound Left Turn Lane
- Southbound Left Turn Lane
- Robbie Drive at US-411
- Northbound Left Turn Lane
- Lake Joyce Road at US-411
- Northbound Left Turn Lane
- Stuart Drive/Coupland Road at US-411
- Northbound Left Turn Lane

Existing turn lane warrant evaluation results are shown in Table 4-5, and the turn lane warrant evaluation summaries can be found in Appendix D.

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Table 4: Existing Right Turn Lane Warrant Evaluation (2-lane Roadway)

| Intersection | Peak Period/ Direction | Major-Road Volume (veh/h) | Turn Volume (veh/h) | Limiting Right Turn Volume (veh/h) | Satisfies <br> Warrant? |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Avalon Drive at US-411 | AM/SB | 981 | 4 | 11 | NO |
|  | PM/SB | 606 | 18 | 19 | NO |
| Washington Drive/Verbena Drive at US-411 | AM/NB | 595 | 27 | 20 | YES |
|  | PM/NB | 913 | 78 | 12 | YES |
|  | AM/SB | 903 | 10 | 12 | NO |
|  | PM/SB | 558 | 8 | 21 | NO |
| Robbie Drive at US-411 | AM/SB | 854 | 1 | 13 | NO |
|  | PM/SB | 494 | 0 | 25 | NO |
| James Taylor Road at US-411 | AM/SB | 889 | 40 | 12 | YES |
|  | PM/SB | 481 | 18 | 26 | NO |
| High School Drive at US-411 | AM/NB | 627 | 290 | 19 | YES |
|  | PM/NB | 760 | 67 | 15 | YES |
| Valleybend Lane at US-411 | AM/SB | 781 | 0 | 14 | NO |
|  | PM/SB | 413 | 1 | 31 | NO |
| Lake Joyce Road at US-411 | AM/SB | 723 | 10 | 16 | NO |
|  | PM/SB | 386 | 13 | 33 | NO |
| Myers <br> Road/Church <br> Road at US-411 | AM/NB | 335 | 10 | 22 | NO |
|  | PM/NB | 856 | 27 | 10 | YES |
|  | AM/SB | 927 | 4 | 10 | NO |
|  | PM/SB | 403 | 3 | 19 | NO |
| Bethel Road at US-411 | AM/NB | 325 | 0 | 22 | NO |
|  | PM/NB | 827 | 1 | 11 | NO |
| Stuart Drive/ Coupland Road at US-411 | AM/NB | 333 | 6 | 22 | NO |
|  | PM/NB | 799 | 37 | 11 | YES |
|  | AM/SB | 831 | 9 | 11 | NO |
|  | PM/SB | 413 | 37 | 18 | YES |

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Table 5: Existing Left Turn Lane Warrant Evaluation (2-Iane Roadway)

| Intersection | Peak Period/ Direction | Opposing Volume (veh/h) | Advancing Volume (veh/h) | Turn Volume (veh/h) | Limiting Advancing Volume to Warrant (veh/h) | Satisfies <br> Warrant? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Avalon Drive at US-411 | AM/NB | 981 | 605 | 18 | 313 | YES |
|  | PM/NB | 606 | 990 | 85 | 276 | YES |
| Washington Drive/Verbena Drive at US-411 | AM/NB | 886 | 595 | 5 | 588 | YES |
|  | PM/NB | 545 | 913 | 21 | 587 | YES |
|  | AM/SB | 590 | 903 | 17 | 561 | YES |
|  | PM/SB | 892 | 558 | 13 | 416 | YES |
| Robbie Drive at US-411 | AM/NB | 854 | 592 | 11 | 431 | YES |
|  | PM/NB | 494 | 836 | 68 | 319 | YES |
| James Taylor Road at US-411 | AM/NB | 889 | 587 | 6 | 587 | YES |
|  | PM/NB | 481 | 763 | 16 | 627 | YES |
| Valleybend Lane at US-411 | AM/NB | 781 | 413 | 4 | 652 | NO |
|  | PM/NB | 413 | 737 | 6 | 947 | NO |
| Lake Joyce Road at US-411 | AM/NB | 723 | 417 | 15 | 374 | YES |
|  | PM/NB | 386 | 734 | 31 | 528 | YES |
| Myers Road/ Church Road at US-411 | AM/NB | 924 | 335 | 4 | 518 | NO |
|  | PM/NB | 399 | 856 | 12 | 878 | NO |
|  | AM/SB | 331 | 927 | 3 | 944 | NO |
|  | PM/SB | 844 | 403 | 4 | 559 | NO |
| Bethel Road at US-411 | AM/SB | 325 | 917 | 2 | 950 | NO |
|  | PM/SB | 827 | 407 | 6 | 569 | NO |
| Stuart Drive/ Coupland Road at US-411 | AM/NB | 829 | 333 | 14 | 288 | YES |
|  | PM/NB | 408 | 799 | 71 | 319 | YES |
|  | AM/SB | 319 | 831 | 2 | 956 | NO |
|  | PM/SB | 728 | 413 | 5 | 627 | NO |

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### 2.7 Signal Warrant Evaluation

Unsignalized intersections can be evaluated for suitability of installing a traffic signal to improve safety and operations. Traffic signals promote the orderly movement of vehicular and pedestrian traffic and aim to prevent excessive delay to traffic. It is also common for traffic signals to increase the likelihood of rear end and left turn collisions at an intersection after installation. It should be noted that traffic signals should not be installed unless one of the warrants specified by the Manual on Uniform Traffic Control Devices (MUTCD) has been satisfied.

## Satisfaction of a signal warrant alone does not necessarily justify installation of a traffic signal.

Signal warrant evaluations were performed at two study intersections along the corridor: US-411 at Washington Drive/Verbena Drive and US-411 at High School Drive. Signal warrant evaluations were performed according to the guidelines in the MUTCD. In the state of Alabama, Warrant \# 1 (8-Hour Vehicular Volume) and Warrant \#2 (4-Hour Vehicular Volume) are most commonly used to justify the installation of a traffic signal.

The signal warrant evaluation reports can be found in Appendix E.

## Signal Warrant Evaluation Results

Under Warrant \#1, the minimum threshold of hourly volume primarily depends on lane configuration and speed limit. The minimum hourly volume thresholds for the intersections of Washington Drive/Verbena Drive and High School Drive are shown in Table 6.

Table 6: Warrant \#1 Minimum Hourly Volume Thresholds

| Street Type Description | Minimum Volume Threshold (vehicles per hour) |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Condition $1 \text { A - 100\% }$ | Condition 1B - 100\% |  |  |
| Both Approaches on Major Street | 350 | 525 | 280 | 420 |
| Highest Approach on Minor Street | 105 | 53 | 84 | 42 |

The minimum hourly volume thresholds from Table 6 were compared to the traffic volumes collected at the intersections of Washington Drive/Verbena Drive and High School Drive. Table 7 notes the number of hours satisfied under each condition associated with Warrant \#1. The US411 approach volumes exceed the minimum hourly volume thresholds for eight out of eight hours at both intersections. However, the minor street approach volumes on Verbena Drive and High School Drive were not high enough to satisfy Warrant \#1 Condition A, Warrant \#1 Condition B, or the combined \#1A and \#1B-80\% condition.

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Table 7: Warrant \#1 Results by Condition

| Street Name | Warrant \#1 Condition |  |  |
| :---: | :---: | :---: | :---: |
|  | $\begin{aligned} & \text { Condition 1A - } \\ & 100 \% \end{aligned}$ | $\begin{gathered} \text { Condition 1B- } \\ 100 \% \end{gathered}$ | Condition 1A \& 1B Combined - 80\% |
| US-411 (Major Street) | 8/8 Hours | 8/8 Hours | 8/8 Hours |
| Washington Drive/Verbena Drive (Minor Street) | 1/8 Hours | 3/8 Hours | 1/8 Hours |
| US-411 (Major Street) | 8/8 Hours | 8/8 Hours | 8/8 Hours |
| High School Drive (Minor Street) | 4/8 Hours | 5/8 Hours | 4/8 Hours |

At Washington Drive and Verbena Drive, the condition most likely to warrant in the future is Condition \#1B - 100\%. Despite only three out of eight hours ( 6 AM, 7 AM, 5 PM) meeting the minimum hourly volume threshold, the other five hours ( $8 \mathrm{AM}, 12$ PM, 3 PM, 4 PM, 6 PM) measured volumes were each within 8 vehicles per hour of meeting the minimum hourly volume threshold of 53 vehicles. A plat for 29 additional homes accessing Verbena Drive was approved by the City Council in October 2022. Based on a technical memorandum produced by Skipper Consulting in March 2018, this development is expected to generate enough additional trips to satisfy Condition \#1B - 100\%. The approved plat and technical memorandum are included in Appendix F.

Using Warrant \#2 at both intersections, the minor street approach volumes must meet the minimum hourly volume threshold of 60 vehicles per hour during four hours of the day. At US-411 and Washington Drive and Verbena Drive, two out of four hours ( 6 AM, 7 AM) meet the minimum hourly volume threshold. Two additional hours (8 AM, 5 PM) were each within 10 vehicles per hour of the minimum volume threshold. At US-411 and High School Drive, four out of four hours meet the minimum hourly volume threshold. Therefore, the intersection of US-411 and High School Drive satisfies Warrant \#2.

Table 8 summarizes the results of the existing conditions signal warrant evaluation at each intersection. In general, an intersection satisfying both warrants is a strong, straightforward candidate for signalization. An intersection that only satisfies Warrant \#2 may need additional justification, especially on a state route. With several schools located on High School Drive, that could be used as context in the justification for installation of a traffic signal.

Table 8: Existing Conditions Signal Warrant Evaluation Results

| Intersection | Signal Warrant Result |  |
| :---: | :---: | :---: |
| \#1- Eight Hour | \#2 - Four Hour |  |
| US-411 at Washington Drive and Verbena Drive | No | No |
| US-411 at High School Drive | No | Yes |

## 3 Pre-NEPA Evaluation

In conjunction with a previously performed study, Corridor Feasibility Study for Multilane Facility on SR-25 (US-4 1 l) from Park Avenue to Sanie Road, associated technical studies were prepared. This section summarizes this previously collected data. Should federal funds be used to implement improvements to the study intersections, a NEPA document would be required. Updates to studies will be required for projects utilizing state and/or federal funds.

## Historic Places

A Phase 1 Cultural Resources (CR) Assessment (December 2018) was prepared by MRS Consultants, LLC. in conjunction with the Corridor Feasibility Study for Multilane Facility on SR-25 (US-4 11) from Park Avenue to Sanie Road. The study area for the Phase 1 assessment included: 125 feet beyond the existing US-411 right-of-way between Park Avenue and Sanie Road; 750 feet along each approach leg for Park Avenue and Sanie Road; 500 feet for intersecting roadways at Church Street, Washington Drive/Verbena Drive, Robbie Drive, James Taylor Road, High School Drive, Lake Joyce Road, Kerr Road, Myers Road/Church Road, and Stuart Road/Coupland Road. The Phase 1 assessment concluded that, "no cultural materials, aboveground features, notable depressions, or other features were identified within the survey corridor." Additionally, the Phase 1 assessment states, "No cultural materials were identified during the field survey. As such, the proposed undertaking will have no adverse effect upon any historic properties for direct effect."

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There are no publicly owned parks and/or recreation areas located in the immediate area of the study intersections.

## Threatened and Endangered Species

A threatened and endangered species evaluation (prepared by Environmental Inc.) was prepared and USFWS coordination performed in conjunction with the Corridor Feasibility Study for Multilane Facility on SR-25 (US-411) from Park Avenue to Sanie Road.

Suitable habitat for the white fringeless orchid was noted along the project corridor; however, a survey of the area performed in August 2019 that thoroughly examined the area for the presence of flowering or vegetative stems of the white fringeless orchid, but no specimens were identified.

Suitable summer roosting habitat for the Indiana bat and the Northern long-eared bat exists within the study corridor. Because of this, there are restrictions related to tree and structure removal.

## Streams and Wetlands

A wetlands and streams jurisdictional evaluation report was prepared by Environmental, Inc. in conjunction with the Corridor Feasibility Study for Multilane Facility on SR-25 (US-411) from Park Avenue to Sanie Road. This report identified twelve (12) streams and nine (9) wetlands that would be considered under the jurisdiction of US Army Corps of Engineers (USACE). Of these identified streams and wetlands, four (4) streams and two (2) wetland areas are located in the proximity of intersections included in this APPLE study area:

- 2 streams located just north of Avalon Drive
- 1 stream located across US-411 at Robbie Drive
- Wetlands located at High School Drive
- 1 stream crossing and a wetland area at Coupland Road

Impacts to jurisdictional streams and wetlands could require a USACE permit. This will require an evaluation during design.

## Prime and Unique Farmlands

For highway projects using federal funds, the Farmland Protection Policy Act applies. This means for federal highway projects that have the potential to convert important farmland to a nonfarm use, the land must be evaluated using the NRCS's LESA system. This land evaluation and site assessment system establishes a farmland conversion impact rating score, and this score is used to determine if potential adverse impacts on the farmland exceed the recommended allowable level.

A search of the Natural Resources Conservation Service's (NRCS) Web Soil Survey was used to determine the potential for prime and unique farmlands within the study area. Mapping generated by the Web Soil Survey website is provided in Appendix G. The NRCS Web Soil Survey shows that the study area is made up primarily of prime farmland; however, the current land use adjacent to US-411 is residential with some commercial. It does not appear that properties within the study area are currently being used for farming.

Should the implementation of improvements identified in this study take place, an AD-1006, Farmland Conversion Rating form will be required. The site assessment portion of this form which assesses non-soil related criteria, is completed by the sponsoring agency and the USDA makes the final determination.

## Hazardous Materials

A hazardous materials evaluation was performed in conjunction with the Corridor Feasibility Study for Multilane Facility on SR-25 (US-411) from Park Avenue to Sanie Road. The evaluation revealed several areas of concern within that study corridor; however, there was no evidence

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of hazardous materials from surrounding properties adversely affecting the APPLE intersections study area.

## Environmental Justice

Environmental Justice is a component of the National Environmental Policy Act (NEPA) that seeks to ensure that all socio-economic groups share in the benefits and burdens of Federal transportation projects. Two areas of environmental justice that frequently become a concern are areas with a high minority population or areas where the majority of the inhabitants are members of low-income households.

Table 9 provides a brief overview of the socioeconomic demographics surrounding the study area. The data is from the Environmental Protection Agency's (EPA) Environmental Justice Screening Tool (EJ Screen). When compared to data for the state, the EPA region, and the country, it can be concluded that there are no concerns related to environmental justice. The minority population percentages of the area are below what is seen in the state, the EPA region, and the country. The percentage of families living below the poverty line is also below that of the state, the EPA region, and the country.

Table 9: Environmental Justice Screen Tool Summary

| Socioeconomic <br> Overview | Value | State <br> Average | Percentile <br> in State | EPA <br> Region <br> Average | Percentile <br> in EPA <br> Region | USA <br> Average | Percentile <br> in USA |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Demographic Index | $17 \%$ | $36 \%$ | 18 | $37 \%$ | 16 | $36 \%$ | 23 |
| Minority Population | $11 \%$ | $34 \%$ | 23 | $39 \%$ | 20 | $40 \%$ | 23 |
| Low Income <br> Population | $22 \%$ | $37 \%$ | 25 | $35 \%$ | 29 | $31 \%$ | 39 |
| Linguistically Isolated <br> Population | $1 \%$ | $1 \%$ | 73 | $3 \%$ | 53 | $5 \%$ | 47 |
| Population with Less <br> Than High School <br> Education | $9 \%$ | $14 \%$ | 35 | $13 \%$ | 41 | $12 \%$ | 48 |

If federal monies are used to install improvements, the sponsoring agency will need to ensure that all planning and outreach components of the project comply with environmental justice regulations under NEPA.

## 4 Concept Plan Development and Evaluation

### 4.1 Traffic Volume Forecasting

The 2018 Corridor Study included a technical memorandum which established a straight-line annual growth rate of $2.3 \%$ per year to be used in future conditions traffic analysis. For this study, existing traffic volumes were grown to a ten-year horizon (2032) using the same $2.3 \%$ per year growth rate. Figures 6 and 7 display the traffic volumes used in the future conditions traffic analysis.


Figure 6: Future Peak Hour Traffic Volumes (2032) - Stuart Drive \& Coupland Road to Valleybend Lane


Figure 7: Future Peak Hour Traffic Volumes (2032) - High School Drive to Avalon Drive

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### 4.2 Future Conditions Turn Lane Warrant Evaluation

Using the same methods described in Section 2.6, Sain Associates conducted a turn lane warrant analysis with future forecasted volumes (2032) at the study intersections. In addition to the turn lanes warranted under existing conditions (See Section 2.6), the following turn lane is expected to warrant by the horizon year during AM and PM peak hours due to forecasted growth in traffic volumes:

- US-411 Southbound Right Turn Lane at James Taylor Road.

Future conditions turn lane warrant evaluation reports can be found in Appendix H.

### 4.3 Recommended Improvements at Priority Intersections

Along with the evaluation of traffic signals, turn lanes, and short-term improvements, conceptual layouts and opinions of probable cost were developed as a part of this study for three priority intersections. The opinions of probable cost are summarized in Section 4.4. Each numbered improvement for the three priority intersections corresponds to the labels in Figures 8 - 10. The following three intersections were identified by stakeholders as priority intersections for the study:

- US-411 at Washington Drive and Verbena Drive
- US-411 at James Taylor Road
- US-411 at High School Drive

All recommended minimum turn lane storage lengths and taper lengths are based on Table 4.6 of the ALDOT Access Management Manual (2021).

## US-411 at Washington Drive and Verbena Drive - Figure 8

1. Install a left turn lane along US-411 northbound at Washington Drive and Verbena Drive, with a minimum storage length of 245 feet and a minimum taper length of 180 feet. Construct an 8 feet wide shoulder, consisting of 4 feet of paved shoulder and 4 feet of grass shoulder.
2. Install a right turn lane along US-411 northbound at Washington Drive and Verbena Drive, with a minimum storage length of 245 feet and a minimum taper length of 180 feet. Construct an 8 feet wide shoulder, consisting of 4 feet of paved shoulder and 4 feet of grass shoulder.
3. Install a left turn lane along US-411 southbound at Washington Drive and Verbena Drive, with a minimum storage length of 245 feet and a minimum taper length of 180 feet. Construct an 8 feet wide shoulder, consisting of 4 feet of paved shoulder and 4 feet of grass shoulder.
4. In conjunction with the installation of turn lanes, consider installation of a traffic signal and associated stop lines. If a traffic signal is not approved immediately, perform a signal warrant evaluation if further development occurs along Verbena Drive.
5. Close the access on the east side US-411 approximately 150 feet south of Verbena Drive. If closure is not feasible, convert to a right-in only access with a raised concrete island for channelization.

## US-411 at James Taylor Road - Figure 9

1. Install a left turn lane along US-411 northbound at James Taylor Road, with a minimum storage length of 245 feet and a minimum taper length of 180 feet. Construct an 8 feet wide shoulder, consisting of 4 feet of paved shoulder and 4 feet of grass shoulder.
2. Install a right turn lane along US-411 southbound at James Taylor Road, with a minimum storage length of 245 feet and a minimum taper length of 180 feet. Construct an 8 feet wide shoulder, consisting of 4 feet of paved shoulder and 4 feet of grass shoulder.

US-411 at High School Drive - Figure 10

1. Install a traffic signal at the intersection. In conjunction with the installation of a traffic signal, install stop lines on both US-411 approaches to the intersection.
2. Restripe the High School Drive approach to US-411.
3. Extend the US-411 southbound left turn by restriping existing pavement.

Due to the proximity of proposed improvements at Washington Drive and Verbena Drive to the proposed turn lanes Avalon Drive and Robbie Drive (see Section 4.4), an alternative strategy would be to construct a continuous three-lane typical section along US-411 from the existing five-lane section at Park Avenue to the existing left turn lane at Tractor Supply, which is just north of Robbie Drive. However, constructing a continuous three lane segment would increase the required project funding and could result in additional time in the project life cycle.


Figure 8: US-411 at Washington Drive and Verbena Drive Recommended Improvements



### 4.4 Recommended Improvements at Other Intersections

The remaining seven study intersections were evaluated for the installation of turn lanes and short-term improvements. No conceptual layouts or opinions of probable cost were developed for the following intersections.

## US-411 at Avalon Drive

- Install a left turn lane along US-411 northbound at Avalon Drive, with a minimum storage length of 245 feet and a minimum taper length of 180 feet.


## US-411 at Robbie Drive

- Install a left turn lane along US-411 northbound at Robbie Drive, with a minimum storage length of 245 feet and a minimum taper length of 180 feet.


## US-411 at Valleybend Lane

No recommendations.

## US-411 at Lake Joyce Road

- Install a left turn lane along US-411 northbound at Lake Joyce Road, with a minimum storage length of 245 feet and a minimum taper length of 180 feet.


## US-411 at Myers Road and Church Road

- Install a left turn lane along US-411 northbound at Myers Road and Church Road, with a minimum storage length of 295 feet and a minimum taper length of 180 feet.


## US-411 at Bethel Road

- Consider closing Bethel Road with a cul-de-sac and diverting traffic to the Church Road approach to US-41 1.


## US-411 at Stuart Drive and Coupland Road

- Install a left turn lane along US-411 northbound at Stuart Drive and Coupland Road, with a minimum storage length of 295 feet and a minimum taper length of 180 feet.


## All US-411 Intersections

- For applicable developments accessing US-411 (State Route 25), a traffic study should be conducted according to the guidelines in the ALDOT Access Management Manual (2021). The manual states, "For developments that generate more than 100 total (inbound plus outbound) peak hour vehicle trips, a traffic impact study is required unless indicated otherwise by the ALDOT Engineer."


### 4.5 Future Conditions Capacity Analysis

Using the methods described in the Transportation Research Board's Highway Capacity Manual, Sain Associates analyzed the future traffic conditions within the study area with all recommended improvements installed. A list of recommended improvements for each intersection can be found in Section 5 of this report.

According to this method of analysis, traffic capacities are expressed as levels of service (LOS) ranging from "A" (free-flow conditions) to "F" (very congested conditions). A detailed description of each LOS designation is included in Appendix B. Generally, LOS "C" is considered desirable, while LOS " $D$ " is considered acceptable during peak hours of traffic flow. The analysis was conducted using Trafficware's Synchro 10 software.

The results of the future conditions capacity analysis are summarized in Tables 10 and 11. Full analysis reports are provided in Appendix I.

Table 10: Future Conditions LOS - 2032

| Intersection | Approach |  | Level of Service |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  | AM Peak | PM Peak |
| Avalon Drive at US-411 (Unsignalized) | EB | Avalon Drive | F | F |
|  | NB | US-411 | A | A |
|  | SB | US-411 | A | A |
| Washington <br> Drive/Verbena Drive at US-411 <br> (Signalized) | EB | Washington Drive | D | C |
|  | WB | Verbena Drive | D | C |
|  | NB | US-411 | A | B |
|  | SB | US-411 | C | A |
|  |  | Intersection LOS | B | B |
| Robbie Drive <br> at US-411 <br> (Unsignalized) | EB | Robbie Drive | E | C |
|  | NB | US-411 | A | A |
|  | SB | US-411 | A | A |
| James Taylor Road at US-411 <br> (Unsignalized) | EB | James Taylor Road | F | E |
|  | NB | US-411 | A | A |
|  | SB | US-411 | A | A |

The recommended improvements, which include signalization, are anticipated to improve the Washington Drive and Verbena Drive intersection to LOS B from failing side street approach LOS under existing conditions. While some low-volume approaches possess LOS F in future conditions, this is not uncommon during peak hours at side street approaches to high volume roadways. The turn lanes proposed at James Taylor Road are not necessarily expected to improve the LOS directly, but the improvements would reduce the likelihood of rear end collisions on US-411.

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Table 11: Future Conditions LOS - 2032 (Continued)

| Intersection |  | Approach | Level of Service |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  | AM Peak | PM Peak |
| High School Drive at US-411 (Signalized) | WB | High School Drive | C | C |
|  | NB | US-411 | B | B |
|  | SB | US-411 | B | A |
|  |  | Intersection LOS | C | C |
| Valleybend Lane at US-411 (Unsignalized) | EB | Valleybend Lane | D | C |
|  | NB | US-411 | A | A |
|  | SB | US-411 | A | A |
| Lake Joyce Road at US-411 (Unsignalized) | EB | Lake Joyce Road | E | C |
|  | NB | US-411 | A | A |
|  | SB | US-411 | A | A |
| Myers Road/Church Road at US-411 (Unsignalized) | EB | Myers Road | E | D |
|  | WB | Church Road | F | F |
|  | NB | US-411 | A | A |
|  | SB | US-411 | A | A |
| Bethel Road at US-411 <br> (Unsignalized) | WB | Bethel Road | N/A | N/A |
|  | NB | US-411 | A | A |
|  | SB | US-411 | A | A |
| Stuart Drive/ Coupland Road at US-411 (Unsignalized) | EB | Stuart Drive | F | E |
|  | WB | Coupland Road | F | F |
|  | NB | US-411 | A | A |
|  | SB | US-411 | A | A |

At the High School Drive intersection, the LOS F and LOS D on the side street approach are improved to an intersection LOS C. Similarly to Table 10, Table 11 also shows several approaches with failing LOS. This is not uncommon during peak hours at side street approaches to highvolume roadways.

### 4.6 Opinions of Probable Cos $\dagger$

Planning-level opinions of probable cost were prepared for each of the three priority intersections. The estimates are based on the engineer's experiences and qualifications and represent the engineer's best judgment within the industry. The engineer does not guarantee that proposals, bids, or actual costs will not vary from the engineer's opinions of probable cost. The opinions of probable cost were estimated in 2022 dollars. For budgeting future year projects, these costs will need to be escalated to future year dollars.

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The totals include opinions of probable cost of construction, preliminary engineering ( $15 \%$ ), utility relocation, right-of-way, construction engineering and inspection (15\%), ALDOT indirect costs (10\%), and a $20 \%$ contingency. Table 12 shows the opinions of probable cost, estimated in 2022 dollars, for the recommended improvements at each of the priority intersections. Detailed breakdowns of each intersection's opinion of probable cost can be found in Appendix J.

Table 12: Opinions of Probable Cost for Priority Intersections (2022 Dollars)

| Intersection | Opinion of Probable Cost (2022 Dollars) |
| :---: | :---: |
| US-411 at Washington Drive and Verbena Drive | $\$ 1.8$ million |
| US-411 at James Taylor Road | $\$ 1.4$ million |
| US-411 at High School Drive | $\$ 540,000$ |

At Washington Drive and Verbena Drive, there is enough existing pavement on US-411 to mill and overlay most of the length of the recommended turn lanes as long as the quality and depth of the pavement is acceptable. This also reduces the chances of impacting the utility poles on the southwest corner of the intersection. No cross drains were located within the turn lane limits, but a small quantity of pipe and a few inlets were estimated. Right-of-way acquisition is not anticipated. If any right-of-way acquisition is required, it would likely be limited to small areas on corners of the intersection. Most utilities are located at the back of existing right-of-way. There are existing water lines that currently tee under the existing pavement on the Verbena approach. ALDOT would likely require relocation of water lines in conjunction with construction of the recommended improvements.

At James Taylor Road, right-of-way acquisition would be required on the northeast corner to accommodate installation of the southbound right turn lane. Several utilities will require relocation, including water lines and sanitary sewer lines. Additionally, there is a large culvert on the northbound approach to the intersection that would likely need to be relocated or extended.

At High School Drive, the major cost item is the traffic signal. Additional striping and pavement markings will be required as a part of the traffic signal design. The costs unrelated to the traffic signal include the mill and overlay of a portion of the southbound left turn lane. This is recommended in order to extend the turn lane within the existing striped area on US-411.

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### 4.7 Prioritization of Recommended Improvements

Based on stakeholder input, engineering judgment, anticipated funding availability, and the analysis performed in the study, each of the recommended improvements have been assigned to one of two categories: short-term priority improvements or improvements which are contingent upon development.

Short-term priority improvements are comprised of the priority intersections' recommendations and the northbound left turn lane at Avalon Drive. The Avalon Drive northbound left turn lane was included as a short-term priority based upon its geographic location on the corridor, reported crash data trends, and its effect on the improvements at priority intersections.

## Short-Term Priority

- Washington Drive \& Verbena Drive - Improvements \# 1 - \#5
- High School Drive - Improvements \# 1 - \#3
- James Taylor Road - Improvements \# 1 \& \#2
- Avalon Drive - Install Northbound Left Turn Lane

Recommended improvements categorized as contingent upon development were based on the presence of undeveloped land nearby and the geographic location of the intersections. US-411 is the main artery of the attractive, fast-growing St. Clair County, which presents an opportunity for the County and the City to pass on a percentage of the cost of roadway improvements to developers desiring to take advantage of access to the roadway network.

## Contingent Upon Development

- Robbie Drive - Install Northbound Left Turn Lane
- Myers Road \& Church Road - Install Northbound Left Turn Lane
- Stuart Drive \& Coupland Road - Install Northbound Left Turn Lane
- Lake Joyce Road - Install Northbound Left Turn Lane
- Bethel Road - Close/Cul-de-sac Bethel Road

Priorities tend to change over time through leadership transitions and funding availability. The City and the County may choose to adjust prioritization of improvements as needed.

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## 5 Funding Sources

The County has options for funding the preferred improvements through federal, state, and local government sources.

Due to the nature of the improvements' purpose and need being safety, there is potential for the City and the County to obtain Highway Safety Improvement Program (HSIP) funds administered by ALDOT's Safety Operations Office. HSIP funding is awarded based on an application that the County must complete. The application involves providing evidence of crash reduction resulting from the implementation of improvement measures. If awarded, the funding match for HSIP is $90 \%$ federal and $10 \%$ local. HSIP-funded projects require additional time to account for ALDOT and FHWA involvement including additional plan reviews and more stringent design and construction standards. For these reasons, a timeframe for completing a HSIP funded project is estimated at five to eight years.

The Congestion Mitigation and Air Quality Improvement Program (CMAQ) is an 80\% Federal/20\% Local match program and has been continued through the Infrastructure Investment and Jobs Act (IIJA). CMAQ funding is available to reduce congestion and improve air quality for areas that do not meet the National Ambient Air Quality Standards for various pollutants. Any project must be included in the metropolitan planning organization's (MPO) current transportation plan and transportation improvement plan (TIP).

Alabama Transportation Rehabilitation and Improvement Program-II (ATRIP-II) was created in 2019 by the Rebuild Alabama Act and is administered by ALDOT. Eligible projects include transportation projects that improve any state-maintained highway system. Projects with a primary focus on local roads are not eligible. For ATRIP-Il projects, ALDOT will perform the preliminary engineering as an eligible cost to the project. A project sponsor can request to perform the preliminary engineering; however, preliminary engineering performed by any entity other than ALDOT is not eligible for ATRIP II funding. Right-of-way acquisition is an ATRIP-II eligible activity, but utility relocation is not. A total of $\$ 40$ Million in ATRIP-Il funding has been allocated in Fiscal Year (FY) 2023. The application deadline for FY 2023 funding is November 18, 2022. The maximum requested funding allowed per project is \$2 Million in FY 2023.

The Rebuild Alabama Act authorizes the ALDOT Annual Grant Program, a $\$ 10$ million fund, for which cities and counties may apply. The Program provides the opportunity for cities and counties to partner with the State on larger projects where adequate local funding may not be available. There is not a specified or required match for local governments, but any funds that local governments can leverage to team with ALDOT to fund a project could play a role in the decision-making process. Up to $\$ 250,000$ per project can be awarded from this fund, and funds must be used for construction or a federal match when construction is imminent.

The County has the option to fund the design and construction of their preferred alternative using only local funds. Choosing this route allows the project design and construction to have shorter timelines and the potential for reduced project costs since fewer plan reviews would be required. US-411 is a state route and ALDOT guidelines will govern the design for that project. An ALDOT permit would also be required for any improvements within the right-of-way on US-411.

## 6 Next Steps

This report documents the study undertaken to further evaluate the traffic operations at ten (10) unsignalized intersections along US-411 from Avalon Drive to Stuart Drive and Coupland Road. In previous sections of this report, transportation analysis and improvement recommendations have been provided.

If the City and the County choose to move forward with implementing any of the recommended improvements using state funding, the next step would be to apply for Fiscal Year 2023 ATRIP-II funding. The application deadline for Fiscal Year 2023 ATRIP-II funding is November 18, 2022. Most recommended improvements, which include the installation of turn lanes to mitigate reported crash trends, could also be eligible for HSIP funding at the federal level.

## Appendix A - Raw Traffic Data




Peak-Hour: 7:00 AM -- 8:00 AM
Peak 15-Min: 7:30 AM -- 7:45 AM


| 15-Min Count Period Beginning At | Moody Pkwy (Northbound) |  |  |  | Moody Pkwy (Southbound) |  |  |  | Robbie Dr (Eastbound) |  |  |  | Robbie Dr (Westbound) |  |  |  | Total | Hourly Totals |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U |  |  |
| 7:00 AM | 0 | 111 | 0 | 0 | 0 | 201 | 0 | 0 | 1 | 0 | 13 | 0 | 0 | 0 | 0 | 0 | 326 |  |
| 7:15 AM | 3 | 148 | 0 | 0 | 0 | 188 | 0 | 0 | 2 | 0 | 19 | 0 | 0 | 0 | 0 | 0 | 360 |  |
| 7:30 AM | 5 | 195 | 0 | 0 | 0 | 260 | 1 | 0 | 1 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 472 |  |
| 7:45 AM | 3 | 127 | 0 | 0 | 0 | 204 | 0 | 0 | 2 | 0 | 18 | 0 | 0 | 0 | 0 | 0 | 354 | 1512 |
| 8:00 AM | 4 | 68 | 0 | 0 | 0 | 168 | 0 | 0 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 250 | 1436 |
| 8:15 AM | 4 | 66 | 0 | 0 | 0 | 156 | 1 | 0 | 1 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 238 | 1314 |
| 8:30 AM | 4 | 88 | 0 | 0 | 0 | 131 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 227 | 1069 |
| 8:45 AM | 8 | 65 | 0 | 0 | 0 | 170 | 0 | 0 | 0 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 250 | 965 |
| Peak 15-Min Flowrates | Northbound |  |  |  | Southbound |  |  |  | Eastbound |  |  |  | Westbound |  |  |  | Total |  |
|  | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U |  |  |  |
| All Vehicles | 20 | 780 | 0 | 0 | 0 | 1040 | 4 | 0 | 4 | 0 | 40 | 0 | 0 | 0 | 0 | 0 |  | 88 |
| Heavy Trucks Buses | 0 | 36 | 0 |  | 0 | 36 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  |  | 2 |
| Pedestrians |  | 0 |  |  |  | 0 |  |  |  | 0 |  |  |  | 0 |  |  |  | 0 |
| Bicycles Scooters | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  |  | 0 |

Comments:


Peak-Hour: 4:45 PM -- 5:45 PM
Peak 15-Min: 5:15 PM -- 5:30 PM


| 15-Min Count Period Beginning At | Moody Pkwy (Northbound) |  |  |  | Moody Pkwy (Southbound) |  |  |  | Robbie Dr (Eastbound) |  |  |  | Robbie Dr (Westbound) |  |  |  | Total | Hourly Totals |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U |  |  |
| 4:00 PM | 8 | 189 | 0 | 0 | 0 | 131 | 1 | 0 | 0 | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 337 |  |
| 4:15 PM | 13 | 174 | 0 | 0 | 0 | 91 | 0 | 0 | 1 | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 287 |  |
| 4:30 PM | 12 | 171 | 0 | 0 | 0 | 108 | 0 | 0 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 301 |  |
| 4:45 PM | 18 | 189 | 0 | 0 | 0 | 110 | 0 | 0 | 0 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 324 | 1249 |
| 5:00 PM | 15 | 181 | 0 | 0 | 0 | 120 | 0 | 0 | 1 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 324 | 1236 |
| 5:15 PM | 21 | 211 | 0 | 0 | 0 | 137 | 0 | 0 | 0 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 376 | 1325 |
| 5:30 PM | 15 | 197 | 0 | 0 | 0 | 120 | 0 | 0 | 0 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 339 | 1363 |
| 5:45 PM | 17 | 179 | 0 | 0 | 0 | 117 | 0 | 0 | 0 | 0 | 11 | 0 | 0 | 0 | 0 | 0 | 324 | 1363 |
| Peak 15-Min Flowrates | Northbound |  |  |  | Southbound |  |  |  | Eastbound |  |  |  | Westbound |  |  |  | Total |  |
|  | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U |  |  |  |
| All Vehicles | 84 | 844 | 0 | 0 | 0 | 548 | 0 | 0 | 0 | 0 | 28 | 0 | 0 | 0 | 0 | 0 |  | 04 |
| Heavy Trucks Buses | 0 | 24 | 0 |  | 0 | 20 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  |  | 4 |
| Pedestrians |  | 0 |  |  |  | 0 |  |  |  | 0 |  |  |  | $0$ |  |  |  |  |
| Bicycles Scooters | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | $0$ | 0 |  |  | 0 |

Comments:

Peak-Hour: 7:00 AM -- 8:00 AM
Peak 15-Min: 7:30 AM -- 7:45 AM


| 15-Min Count Period Beginning At | Moody Pkwy (Northbound) |  |  |  | Moody Pkwy (Southbound) |  |  |  | James Taylor Rd (Eastbound) |  |  |  | James Taylor Rd (Westbound) |  |  |  | Total | Hourly Totals |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U |  |  |
| 7:00 AM | 0 | 105 | 0 | 0 | 0 | 197 | 2 | 0 | 9 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 316 |  |
| 7:15 AM | 1 | 149 | 0 | 0 | 0 | 186 | 4 | 0 | 14 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 358 |  |
| 7:30 AM | 0 | 204 | 0 | 0 | 0 | 261 | 22 | 0 | 14 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 503 |  |
| 7:45 AM | 5 | 123 | 0 | 0 | 0 | 205 | 12 | 0 | 11 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 359 | 1536 |
| 8:00 AM | 2 | 66 | 0 | 0 | 0 | 155 | 4 | 0 | 3 | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 238 | 1458 |
| 8:15 AM | 1 | 62 | 0 | 0 | 0 | 142 | 6 | 0 | 3 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 216 | 1316 |
| 8:30 AM | 0 | 84 | 0 | 0 | 0 | 138 | 1 | 0 | 3 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 228 | 1041 |
| 8:45 AM | 2 | 65 | 0 | 0 | 0 | 162 | 1 | 0 | 4 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 237 | 919 |
| Peak 15-Min Flowrates | Northbound |  |  |  | Southbound |  |  |  | Eastbound |  |  |  | Westbound |  |  |  | Total |  |
|  | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U |  |  |  |
| All Vehicles | 0 | 816 | 0 | 0 | 0 | 1044 | 88 | 0 | 56 | 0 | 8 | 0 | 0 | 0 | 0 | 0 |  | 12 |
| Heavy Trucks Buses | 0 | 40 | 0 |  | 0 | 36 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  |  | 6 |
| Pedestrians |  | 0 |  |  |  | 0 |  |  |  | 0 |  |  |  | 0 |  |  |  |  |
| Bicycles Scooters | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  |  |  |

Comments:


Peak-Hour: 5:00 PM -- 6:00 PM
Peak 15-Min: 5:15 PM -- 5:30 PM


| 15-Min Count Period Beginning At | Moody Pkwy (Northbound) |  |  |  | Moody Pkwy (Southbound) |  |  |  | James Taylor Rd (Eastbound) |  |  |  | James Taylor Rd (Westbound) |  |  |  | Total | Hourly Totals |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U |  |  |
| 4:00 PM | 5 | 180 | 0 | 0 | 0 | 121 | 4 | 0 | 3 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 314 |  |
| 4:15 PM | 9 | 163 | 0 | 0 | 0 | 90 | 6 | 0 | 4 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 273 |  |
| 4:30 PM | 5 | 172 | 0 | 0 | 0 | 110 | 4 | 0 | 5 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 297 |  |
| 4:45 PM | 2 | 171 | 0 | 1 | 0 | 108 | 4 | 0 | 3 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 294 | 1178 |
| 5:00 PM | 8 | 179 | 0 | 0 | 0 | 109 | 2 | 0 | 6 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 306 | 1170 |
| 5:15 PM | 4 | 197 | 0 | 0 | 0 | 129 | 4 | 0 | 4 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 342 | 1239 |
| 5:30 PM | 1 | 190 | 0 | 0 | 0 | 116 | 5 | 0 | 7 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 323 | 1265 |
| 5:45 PM | 3 | 181 | 0 | 0 | 0 | 109 | 7 | 0 | 4 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 306 | 1277 |
| Peak 15-Min Flowrates | Northbound |  |  |  | Southbound |  |  |  | Eastbound |  |  |  | Westbound |  |  |  | Total |  |
|  | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U |  |  |  |
| All Vehicles | 16 | 788 | 0 | 0 | 0 | 516 | 16 | 0 | 16 | 0 | 16 | 0 | 0 | 0 | 0 | 0 |  | 68 |
| Heavy Trucks Buses | 0 | 24 | 0 |  | 0 | 16 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  |  | 0 |
| Pedestrians |  | 0 |  |  |  | 0 |  |  |  | $0$ |  |  |  | $0$ |  |  |  | 0 |
| Bicycles Scooters | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | $0$ | 0 |  | 0 | $0$ | 0 |  |  | 0 |

Comments:


Peak-Hour: 7:00 AM -- 8:00 AM
Peak 15-Min: 7:00 AM -- 7:15 AM


| 15-Min Count Period Beginning At | Moody Pkwy (Northbound) |  |  |  | Moody Pkwy (Southbound) |  |  |  | Myers Rd/Church Rd (Eastbound) |  |  |  | Myers Rd/Church Rd (Westbound) |  |  |  | Total | Hourly Totals |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U |  |  |
| 7:00 AM | 0 | 91 | 0 | 0 | 1 | 249 | 1 | 0 | 3 | 0 | 10 | 0 | 1 | 0 | 0 | 0 | 356 |  |
| 7:15 AM | 0 | 64 | 1 | 0 | 1 | 257 | 1 | 0 | 2 | 0 | 8 | 0 | 5 | 0 | 0 | 0 | 339 |  |
| 7:30 AM | 3 | 80 | 4 | 0 | 0 | 224 | 2 | 0 | 0 | 0 | 9 | 0 | 3 | 0 | 0 | 0 | 325 |  |
| 7:45 AM | 1 | 86 | 5 | 0 | 1 | 190 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 285 | 1305 |
| 8:00 AM | 0 | 56 | 3 | 0 | 1 | 148 | 2 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 212 | 1161 |
| 8:15 AM | 1 | 59 | 0 | 1 | 0 | 143 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 207 | 1029 |
| 8:30 AM | 1 | 77 | 0 | 1 | 0 | 130 | 1 | 0 | 1 | 0 | 1 | 0 | 6 | 0 | 1 | 0 | 219 | 923 |
| 8:45 AM | 0 | 69 | 2 | 0 | 0 | 155 | 0 | 0 | 0 | 0 | 2 | 0 | 7 | 0 | 0 | 0 | 235 | 873 |
| Peak 15-Min Flowrates | Northbound |  |  |  | Southbound |  |  |  | Eastbound |  |  |  | Westbound |  |  |  | Total |  |
|  | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U |  |  |  |
| All Vehicles | 0 | 364 | 0 | 0 | 4 | 996 | 4 | 0 | 12 | 0 | 40 | 0 | 4 | 0 | 0 | 0 |  | 24 |
| Heavy Trucks Buses | 0 | 44 | 0 |  | 0 | 16 | 4 |  | 0 | 0 | 4 |  | 0 | 0 | 0 |  |  | 8 |
| Pedestrians |  | 0 |  |  |  | 0 |  |  |  | 0 |  |  |  | 0 |  |  |  |  |
| Bicycles Scooters | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  |  | 0 |

Comments:


| 15-Min Count Period Beginning At | Moody Pkwy (Northbound) |  |  |  | Moody Pkwy (Southbound) |  |  |  | Myers Rd/Church Rd (Eastbound) |  |  |  | Myers Rd/Church Rd (Westbound) |  |  |  | Total | Hourly Totals |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U |  |  |
| 4:00 PM | 5 | 188 | 1 | 0 | 0 | 113 | 1 | 0 | 2 | 0 | 3 | 0 | 1 | 0 | 0 | 0 | 314 |  |
| 4:15 PM | 3 | 176 | 1 | 0 | 0 | 99 | 1 | 0 | 1 | 0 | 2 | 0 | 4 | 0 | 0 | 0 | 287 |  |
| 4:30 PM | 2 | 170 | 4 | 0 | 0 | 109 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 286 |  |
| 4:45 PM | 3 | 183 | 6 | 0 | 0 | 116 | 1 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 1 | 0 | 313 | 1200 |
| 5:00 PM | 2 | 194 | 5 | 0 | 1 | 90 | 1 | 0 | 1 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 297 | 1183 |
| 5:15 PM | 3 | 211 | 3 | 0 | 1 | 116 | 2 | 0 | 1 | 0 | 4 | 0 | 1 | 0 | 3 | 0 | 345 | 1241 |
| 5:30 PM | 4 | 213 | 8 | 0 | 1 | 88 | 0 | 0 | 2 | 0 | 3 | 0 | 3 | 0 | 0 | 0 | 322 | 1277 |
| 5:45 PM | 3 | 199 | 11 | 0 | 1 | 102 | 0 | 0 | 0 | 0 | 1 | 0 | 2 | 0 | 0 | 0 | 319 | 1283 |
| Peak 15-Min Flowrates | Northbound |  |  |  | Southbound |  |  |  | Eastbound |  |  |  | Westbound |  |  |  | Total |  |
|  | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U |  |  |  |
| All Vehicles | 12 | 844 | 12 | 0 | 4 | 464 | 8 | 0 | 4 | 0 | 16 | 0 | 4 | 0 | 12 | 0 |  | 80 |
| Heavy Trucks Buses | 0 | 32 | 0 |  | 0 | 20 | 4 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  |  | 6 |
| Pedestrians |  | 0 |  |  |  | 0 |  |  |  | 0 |  |  |  | 0 |  |  |  |  |
| Bicycles Scooters | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  |  | 0 |

Comments:

Peak-Hour: 7:00 AM -- 8:00 AM
Peak 15-Min: 7:00 AM -- 7:15 AM


| 15-Min Count Period Beginning At | Moody Pkwy (Northbound) |  |  |  | Moody Pkwy (Southbound) |  |  |  | Stuart Dr (Lazy V Lakes Rd)/Copeland Rd (Eastbound) |  |  |  | Stuart Dr (Lazy V Lakes Rd)/Copeland Rd (Westbound) |  |  |  | Total | Hourly Totals |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U |  |  |
| 7:00 AM | 1 | 93 | 2 | 0 | 1 | 223 | 1 | 0 | 8 | 1 | 20 | 0 | 3 | 0 | 1 | 0 | 354 |  |
| 7:15 AM | 5 | 63 | 2 | 0 | 1 | 221 | 2 | 0 | 7 | 0 | 17 | 0 | 11 | 0 | 0 | 0 | 329 |  |
| 7:30 AM | 4 | 67 | 1 | 0 | 0 | 203 | 2 | 0 | 9 | 0 | 20 | 0 | 5 | 0 | 0 | 0 | 311 |  |
| 7:45 AM | 4 | 90 | 1 | 0 | 0 | 173 | 4 | 0 | 0 | 0 | 13 | 0 | 6 | 0 | 0 | 0 | 291 | 1285 |
| 8:00 AM | 2 | 51 | 4 | 0 | 2 | 137 | 2 | 0 | 8 | 0 | 14 | 0 | 5 | 0 | 1 | 0 | 226 | 1157 |
| 8:15 AM | 7 | 57 | 0 | 0 | 1 | 122 | 4 | 0 | 4 | 0 | 8 | 0 | 2 | 0 | 0 | 0 | 205 | 1033 |
| 8:30 AM | 3 | 70 | 3 | 0 | 2 | 122 | 2 | 0 | 4 | 0 | 8 | 0 | 4 | 0 | 0 | 0 | 218 | 940 |
| 8:45 AM | 3 | 61 | 4 | 0 | 0 | 142 | 2 | 0 | 4 | 0 | 4 | 0 | 2 | 0 | 1 | 0 | 223 | 872 |
| Peak 15-Min Flowrates | Northbound |  |  |  | Southbound |  |  |  | Eastbound |  |  |  | Westbound |  |  |  | Total |  |
|  | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U |  |  |  |
| All Vehicles | 4 | 372 | 8 | 0 | 4 | 892 | 4 | 0 | 32 | 4 | 80 | 0 | 12 | 0 | 4 | 0 |  | 16 |
| Heavy Trucks Buses | 0 | 40 | 0 |  | 4 | 24 | 0 |  | 0 | 0 | 0 |  | 4 | 0 | 0 |  |  | 2 |
| Pedestrians |  | 0 |  |  |  | 0 |  |  |  | 0 |  |  |  | 0 |  |  |  | 0 |
| Bicycles Scooters | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  |  | 0 |

Comments:

Report generated on 5/13/2022 12:04 PM
SOURCE: Quality Counts, LLC (http://www.qualitycounts.net) 1-877-580-2212


Report generated on 5/13/2022 12:04 PM
SOURCE: Quality Counts, LLC (http://www.qualitycounts.net) 1-877-580-2212

Peak-Hour: 7:00 AM -- 8:00 AM
Peak 15-Min: 7:30 AM -- 7:45 AM


| 15-Min Count Period Beginning At | Moody Pkwy (Northbound) |  |  |  | Moody Pkwy (Southbound) |  |  |  | Lake Joyce Rd (Eastbound) |  |  |  | Lake Joyce Rd (Westbound) |  |  |  | Total | Hourly Totals |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U |  |  |
| 7:00 AM | 0 | 91 | 0 | 0 | 0 | 190 | 0 | 0 | 6 | 0 | 12 | 0 | 0 | 0 | 0 | 0 | 299 |  |
| 7:15 AM | 1 | 92 | 0 | 0 | 0 | 202 | 3 | 0 | 5 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 313 |  |
| 7:30 AM | 7 | 135 | 0 | 0 | 0 | 163 | 2 | 0 | 6 | 0 | 21 | 0 | 0 | 0 | 0 | 0 | 334 |  |
| 7:45 AM | 7 | 84 | 0 | 0 | 0 | 158 | 5 | 0 | 5 | 0 | 9 | 0 | 0 | 0 | 0 | 0 | 268 | 1214 |
| 8:00 AM | 5 | 58 | 0 | 0 | 0 | 135 | 3 | 0 | 2 | 0 | 11 | 0 | 0 | 0 | 0 | 0 | 214 | 1129 |
| 8:15 AM | 8 | 50 | 0 | 0 | 0 | 131 | 0 | 0 | 1 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 197 | 1013 |
| 8:30 AM | 4 | 67 | 0 | 0 | 0 | 128 | 1 | 0 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 210 | 889 |
| 8:45 AM | 3 | 57 | 0 | 0 | 0 | 143 | 1 | 0 | 2 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 216 | 837 |
| Peak 15-Min Flowrates | Northbound |  |  |  | Southbound |  |  |  | Eastbound |  |  |  | Westbound |  |  |  | Total |  |
|  | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U |  |  |  |
| All Vehicles | 28 | 540 | 0 | 0 | 0 | 652 | 8 | 0 | 24 | 0 | 84 | 0 | 0 | 0 | 0 | 0 |  | 36 |
| Heavy Trucks Buses | 4 | 16 | 0 |  | 0 | 24 | 0 |  | 0 | 0 | 4 |  | 0 | 0 | 0 |  |  | 8 |
| Pedestrians |  | 0 |  |  |  | 0 |  |  |  | 0 |  |  |  | 0 |  |  |  |  |
| Bicycles Scooters | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  |  |  |

Comments:


Peak-Hour: 5:00 PM -- 6:00 PM
Peak 15-Min: 5:15 PM -- 5:30 PM


| 15-Min Count Period Beginning At | Moody Pkwy (Northbound) |  |  |  | Moody Pkwy (Southbound) |  |  |  | Lake Joyce Rd (Eastbound) |  |  |  | Lake Joyce Rd (Westbound) |  |  |  | Total | Hourly Totals |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U |  |  |
| 4:00 PM | 3 | 167 | 0 | 0 | 0 | 111 | 1 | 0 | 3 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 289 |  |
| 4:15 PM | 11 | 150 | 0 | 0 | 0 | 86 | 3 | 0 | 1 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 256 |  |
| 4:30 PM | 11 | 149 | 0 | 0 | 0 | 94 | 7 | 0 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 265 |  |
| 4:45 PM | 14 | 153 | 0 | 0 | 0 | 102 | 4 | 0 | 1 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 281 | 1091 |
| 5:00 PM | 6 | 169 | 0 | 0 | 0 | 81 | 1 | 0 | 1 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 265 | 1067 |
| 5:15 PM | 6 | 181 | 0 | 0 | 0 | 111 | 3 | 0 | 4 | 0 | 9 | 0 | 0 | 0 | 0 | 0 | 314 | 1125 |
| 5:30 PM | 11 | 187 | 0 | 0 | 0 | 89 | 4 | 0 | 4 | 0 | 9 | 0 | 0 | 0 | 0 | 0 | 304 | 1164 |
| 5:45 PM | 8 | 166 | 0 | 0 | 0 | 92 | 5 | 0 | 2 | 0 | 11 | 0 | 0 | 0 | 0 | 0 | 284 | 1167 |
| Peak 15-Min Flowrates | Northbound |  |  |  | Southbound |  |  |  | Eastbound |  |  |  | Westbound |  |  |  | Total |  |
|  | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U |  |  |  |
| All Vehicles | 24 | 724 | 0 | 0 | 0 | 444 | 12 | 0 | 16 | 0 | 36 | 0 | 0 | 0 | 0 | 0 |  | 56 |
| Heavy Trucks Buses | 0 | 28 | 0 |  | 0 | 12 | 0 |  | 0 | 0 | 4 |  | 0 | 0 | 0 |  |  | 4 |
| Pedestrians |  | 0 |  |  |  | 0 |  |  |  | 0 |  |  |  | $0$ |  |  |  | 0 |
| Bicycles Scooters | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | $0$ | 0 |  |  | 0 |

Comments:


Peak-Hour: 7:00 AM -- 8:00 AM
Peak 15-Min: 7:30 AM -- 7:45 AM


| 15-Min Count Period Beginning At | Moody Pkwy (Northbound) |  |  |  | Moody Pkwy (Southbound) |  |  |  | Washington Dr/Verbena Dr (Eastbound) |  |  |  | Washington Dr/Verbena Dr (Westbound) |  |  |  | Total | Hourly Totals |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U |  |  |
| 6:00 AM | 0 | 29 | 1 | 0 | 2 | 127 | 0 | 0 | 0 | 0 | 2 | 0 | 11 | 0 | 3 | 0 | 175 |  |
| 6:15 AM | 1 | 44 | 2 | 0 | 1 | 185 | 0 | 0 | 2 | 0 | 6 | 0 | 15 | 0 | 1 | 0 | 257 |  |
| 6:30 AM | 2 | 59 | 2 | 0 | 1 | 208 | 2 | 0 | 3 | 0 | 6 | 0 | 12 | 0 | 4 | 0 | 299 |  |
| 6:45 AM | 1 | 72 | 2 | 0 | 1 | 208 | 0 | 0 | 2 | 1 | 8 | 0 | 15 | 0 | 5 | 0 | 315 | 1046 |
| 7:00 AM | 2 | 103 | 7 | 0 | 3 | 212 | 0 | 0 | 6 | 1 | 9 | 0 | 20 | 0 | 6 | 0 | 369 | 1240 |
| 7:15 AM | 0 | 152 | 10 | 0 | 2 | 202 | 1 | 0 | 6 | 0 | 11 | 0 | 27 | 0 | 8 | 0 | 419 | 1402 |
| 7:30 AM | 1 | 190 | 6 | 0 | 4 | 253 | 7 | 0 | 6 | 0 | 7 | 0 | 12 | 0 | 11 | 0 | 497 | 1600 |
| 7:45 AM | 2 | 118 | 4 | 0 | 8 | 209 | 2 | 0 | 3 | 0 | 6 | 0 | 20 | 0 | 6 | 0 | 378 | 1663 |
| 8:00 AM | 5 | 81 | 5 | 0 | 4 | 183 | 1 | 0 | 0 | 1 | 6 | 0 | 13 | 0 | 3 | 0 | 302 | 1596 |
| 8:15 AM | 2 | 72 | 5 | 0 | 0 | 167 | 0 | 0 | 1 | 2 | 6 | 0 | 10 | 0 | 4 | 0 | 269 | 1446 |
| 8:30 AM | 1 | 90 | 3 | 0 | 0 | 135 | 0 | 0 | 2 | 0 | 4 | 0 | 7 | 0 | 4 | 0 | 246 | 1195 |
| 8:45 AM | 1 | 77 | 3 | 0 | 1 | 181 | 0 | 0 | 1 | 0 | 4 | 0 | 9 | 0 | 1 | 0 | 278 | 1095 |
| 9:00 AM | 2 | 86 | 1 | 0 | 1 | 170 | 0 | 0 | 0 | 0 | 4 | 0 | 8 | 0 | 1 | 0 | 273 | 1066 |
| 9:15 AM | 3 | 77 | 6 | 0 | 0 | 162 | 3 | 0 | 3 | 0 | 3 | 0 | 4 | 0 | 1 | 0 | 262 | 1059 |
| 9:30 AM | 1 | 81 | 5 | 0 | 3 | 90 | 1 | 0 | 1 | 0 | 1 | 0 | 8 | 0 | 2 | 0 | 193 | 1006 |
| 9:45 AM | 0 | 78 | 4 | 0 | 1 | 112 | 0 | 0 | 0 | 0 | 2 | 0 | 4 | 1 | 2 | 0 | 204 | 932 |
| 10:00 AM | 1 | 86 | 10 | 1 | 2 | 99 | 1 | 0 | 0 | 1 | 0 | 0 | 4 | 0 | 1 | 0 | 206 | 865 |
| 10:15 AM | 1 | 90 | 6 | 0 | 4 | 124 | 1 | 0 | 1 | 0 | 2 | 0 | 10 | 0 | 3 | 0 | 242 | 845 |
| 10:30 AM | 0 | 77 | 2 | 0 | 0 | 100 | 1 | 0 | 1 | 0 | 3 | 0 | 4 | 0 | 3 | 0 | 191 | 843 |
| 10:45 AM | 0 | 84 | 8 | 0 | 1 | 104 | 0 | 0 | 0 | 0 | 1 | 0 | 6 | 0 | 5 | 0 | 209 | 848 |
| 11:00 AM | 4 | 112 | 5 | 0 | 7 | 133 | 0 | 0 | 0 | 1 | 1 | 0 | 7 | 0 | 6 | 0 | 276 | 918 |
| 11:15 AM | 1 | 99 | 7 | 0 | 0 | 102 | 1 | 0 | 2 | 0 | 1 | 0 | 4 | 0 | 3 | 0 | 220 | 896 |
| 11:30 AM | 2 | 109 | 5 | 0 | 2 | 138 | 1 | 0 | 0 | 0 | 3 | 0 | 4 | 0 | 6 | 0 | 270 | 975 |
| 11:45 AM | 5 | 116 | 12 | 0 | 1 | 141 | 0 | 0 | 0 | 2 | 4 | 0 | 9 | 2 | 1 | 0 | 293 | 1059 |
| 12:00 PM | 1 | 117 | 9 | 0 | 4 | 143 | 2 | 0 | 1 | 0 | 1 | 0 | 13 | 1 | 2 | 0 | 294 | 1077 |
| 12:15 PM | 3 | 125 | 6 | 0 | 1 | 148 | 1 | 0 | 2 | 1 | 5 | 0 | 7 | 0 | 4 | 0 | 303 | 1160 |
| 12:30 PM | 4 | 129 | 5 | 0 | 3 | 122 | 0 | 0 | 1 | 1 | 5 | 0 | 8 | 1 | 1 | 0 | 280 | 1170 |
| 12:45 PM | 2 | 125 | 6 | 0 | 1 | 114 | 2 | 0 | 1 | 0 | 3 | 0 | 6 | 0 | 3 | 0 | 263 | 1140 |
| 1:00 PM | 3 | 146 | 6 | 0 | 5 | 107 | 2 | 0 | 0 | 0 | 1 | 0 | 3 | 0 | 3 | 0 | 276 | 1122 |
| 1:15 PM | 4 | 126 | 8 | 0 | 4 | 110 | 0 | 0 | 0 | 0 | 2 | 0 | 10 | 0 | 3 | 0 | 267 | 1086 |
| 1:30 PM | 1 | 161 | 9 | 0 | 1 | 107 | 0 | 0 | 0 | 0 | 0 | 0 | 11 | 0 | 4 | 0 | 294 | 1100 |
| 1:45 PM | 2 | 149 | 8 | 1 | 1 | 115 | 1 | 0 | 1 | 0 | 3 | 0 | 5 | 1 | 4 | 0 | 291 | 1128 |
| 2:00 PM | 0 | 143 | 9 | 0 | 1 | 144 | 1 | 0 | 3 | 0 | 1 | 0 | 4 | 0 | 5 | 0 | 311 | 1163 |
| 2:15 PM | 2 | 147 | 8 | 0 | 3 | 155 | 2 | 0 | 1 | 0 | 4 | 0 | 8 | 0 | 2 | 0 | 332 | 1228 |
| 2:30 PM | 5 | 183 | 9 | 0 | 3 | 124 | 1 | 0 | 5 | 1 | 0 | 0 | 4 | 0 | 6 | 0 | 341 | 1275 |
| 2:45 PM | 2 | 211 | 10 | 0 | 5 | 136 | 5 | 0 | 1 | 0 | 3 | 0 | 4 | 0 | 2 | 0 | 379 | 1363 |
| 3:00 PM | 3 | 163 | 12 | 0 | 10 | 177 | 7 | 0 | 4 | 0 | 2 | 0 | 11 | 0 | 5 | 0 | 394 | 1446 |
| 3:15 PM | 5 | 164 | 8 | 0 | 5 | 177 | 4 | 0 | 1 | 1 | 8 | 0 | 8 | 1 | 7 | 0 | 389 | 1503 |


| 15-Min Count Period Beginning At | Moody Pkwy (Northbound) |  |  |  | Moody Pkwy (Southbound) |  |  |  | Washington Dr/Verbena Dr (Eastbound) |  |  |  | Washington Dr/Verbena Dr (Westbound) |  |  |  | Total | Hourly Totals |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U |  |  |
| 3:30 PM | 3 | 174 | 8 | 0 | 3 | 135 | 4 | 0 | 1 | 0 | 1 | 0 | 4 | 0 | 4 | 0 | 337 | 1499 |
| 3:45 PM | 3 | 167 | 11 | 0 | 7 | 143 | 1 | 0 | 3 | 1 | 3 | 0 | 7 | 1 | 5 | 0 | 352 | 1472 |
| 4:00 PM | 0 | 177 | 16 | 0 | 2 | 152 | 4 | 0 | 0 | 0 | 8 | 0 | 6 | 1 | 7 | 0 | 373 | 1451 |
| 4:15 PM | 8 | 188 | 9 | 0 | 6 | 104 | 0 | 0 | 1 | 0 | 2 | 0 | 9 | 1 | 2 | 0 | 330 | 1392 |
| 4:30 PM | 5 | 176 | 21 | 0 | 5 | 124 | 0 | 0 | 2 | 0 | 1 | 0 | 6 | 1 | 11 | 0 | 352 | 1407 |
| 4:45 PM | 8 | 197 | 9 | 0 | 3 | 125 | 3 | 0 | 0 | 0 | 4 | 0 | 2 | 2 | 6 | 0 | 359 | 1414 |
| 5:00 PM | 6 | 193 | 16 | 0 | 2 | 129 | 4 | 0 | 1 | 1 | 4 | 0 | 5 | 1 | 3 | 0 | 365 | 1406 |
| 5:15 PM | 5 | 234 | 27 | 0 | 4 | 145 | 1 | 0 | 4 | 0 | 3 | 0 | 11 | 0 | 9 | 0 | 443 | 1519 |
| 5:30 PM | 3 | 191 | 20 | 0 | 4 | 136 | 1 | 0 | 1 | 0 | 6 | 0 | 14 | 1 | 2 | 0 | 379 | 1546 |
| 5:45 PM | 7 | 196 | 15 | 0 | 3 | 127 | 2 | 0 | 1 | 0 | 7 | 0 | 6 | 1 | 3 | 0 | 368 | 1555 |
| 6:00 PM | 6 | 186 | 20 | 0 | 4 | 126 | 0 | 0 | 1 | 1 | 6 | 0 | 11 | 0 | 4 | 0 | 365 | 1555 |
| 6:15 PM | 11 | 139 | 8 | 0 | 4 | 106 | 3 | 0 | 2 | 0 | 5 | 0 | 5 | 0 | 4 | 0 | 287 | 1399 |
| 6:30 PM | 5 | 148 | 9 | 0 | 4 | 85 | 2 | 0 | 0 | 0 | 5 | 0 | 11 | 0 | 3 | 0 | 272 | 1292 |
| 6:45 PM | 8 | 128 | 14 | 0 | 3 | 81 | 2 | 0 | 0 | 0 | 6 | 0 | 5 | 0 | 4 | 0 | 251 | 1175 |
| 7:00 PM | 4 | 114 | 12 | 0 | 3 | 66 | 1 | 0 | 1 | 0 | 3 | 0 | 6 | 2 | 1 | 0 | 213 | 1023 |
| 7:15 PM | 2 | 118 | 10 | 0 | 0 | 50 | 0 | 0 | 0 | 2 | 2 | 0 | 6 | 0 | 3 | 0 | 193 | 929 |
| 7:30 PM | 4 | 102 | 7 | 0 | 1 | 68 | 2 | 0 | 1 | 1 | 2 | 0 | 5 | 0 | 1 | 0 | 194 | 851 |
| 7:45 PM | 4 | 118 | 5 | 0 | 1 | 61 | 3 | 0 | 4 | 0 | 5 | 0 | 3 | 0 | 2 | 0 | 206 | 806 |
| Peak 15-Min Flowrates | Northbound |  |  |  | Southbound |  |  |  | Eastbound |  |  |  | Westbound |  |  |  | Total |  |
|  | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U |  |  |  |
| All Vehicles | 4 | 760 | 24 | 0 | 16 | 1012 | 28 | 0 | 24 | 0 | 28 | 0 | 48 | 0 | 44 | 0 |  | 88 |
| Heavy Trucks Buses | 0 | 32 | 0 |  | 0 | 40 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  |  | 72 |
| Pedestrians |  | 0 |  |  |  | 0 |  |  |  | 0 |  |  |  | 0 |  |  |  | 0 |
| Bicycles Scooters | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  |  | 0 |
| Comments: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |



Peak-Hour: 7:00 AM -- 8:00 AM
Peak 15-Min: 7:30 AM -- 7:45 AM


| 15-Min Count Period Beginning At | Moody Pkwy (Northbound) |  |  |  | Moody Pkwy (Southbound) |  |  |  | Valleybend Ln (Eastbound) |  |  |  | Valleybend Ln (Westbound) |  |  |  | Total | Hourly Totals |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U |  |  |
| 7:00 AM | 0 | 84 | 0 | 0 | 0 | 214 | 0 | 0 | 3 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 303 |  |
| 7:15 AM | 0 | 85 | 1 | 0 | 0 | 192 | 0 | 0 | 1 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 282 |  |
| 7:30 AM | 0 | 140 | 0 | 0 | 0 | 192 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 335 |  |
| 7:45 AM | 4 | 100 | 0 | 0 | 0 | 183 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 290 | 1210 |
| 8:00 AM | 2 | 63 | 0 | 0 | 0 | 144 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 210 | 1117 |
| 8:15 AM | 1 | 56 | 0 | 0 | 0 | 142 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 202 | 1037 |
| 8:30 AM | 0 | 69 | 0 | 0 | 0 | 137 | 1 | 0 | 1 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 210 | 912 |
| 8:45 AM | 1 | 65 | 0 | 0 | 0 | 157 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 223 | 845 |
| Peak 15-Min Flowrates | Northbound |  |  |  | Southbound |  |  |  | Eastbound |  |  |  | Westbound |  |  |  | Total |  |
|  | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U |  |  |  |
| All Vehicles | 0 | 560 | 0 | 0 | 0 | 768 | 0 | 0 | 0 | 0 | 12 | 0 | 0 | 0 | 0 | 0 |  | 40 |
| Heavy Trucks Buses | 0 | 12 | 0 |  | 0 | 28 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  |  | 0 |
| Pedestrians |  | 0 |  |  |  | 0 |  |  |  | 0 |  |  |  | 0 |  |  |  | 0 |
| Bicycles Scooters | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  |  | 0 |

Comments:


Peak-Hour: 5:00 PM -- 6:00 PM
Peak 15-Min: 5:15 PM -- 5:30 PM


| 15-Min Count Period Beginning At | Moody Pkwy (Northbound) |  |  |  | Moody Pkwy (Southbound) |  |  |  | Valleybend Ln (Eastbound) |  |  |  | Valleybend Ln (Westbound) |  |  |  | Total | Hourly Totals |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U |  |  |
| 4:00 PM | 3 | 174 | 0 | 0 | 0 | 110 | 1 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 291 |  |
| 4:15 PM | 2 | 163 | 0 | 0 | 0 | 85 | 1 | 0 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 255 |  |
| 4:30 PM | 1 | 152 | 0 | 0 | 0 | 103 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 258 |  |
| 4:45 PM | 1 | 166 | 0 | 0 | 0 | 103 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 273 | 1077 |
| 5:00 PM | 0 | 174 | 0 | 0 | 0 | 92 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 268 | 1054 |
| 5:15 PM | 1 | 192 | 0 | 0 | 0 | 114 | 0 | 0 | 1 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 310 | 1109 |
| 5:30 PM | 3 | 190 | 0 | 0 | 0 | 102 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 297 | 1148 |
| 5:45 PM | 2 | 175 | 0 | 0 | 0 | 104 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 282 | 1157 |
| Peak 15-Min Flowrates | Northbound |  |  |  | Southbound |  |  |  | Eastbound |  |  |  | Westbound |  |  |  | Total |  |
|  | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U |  |  |  |
| All Vehicles | 4 | 768 | 0 | 0 | 0 | 456 | 0 | 0 | 4 | 0 | 8 | 0 | 0 | 0 | 0 | 0 |  | 40 |
| Heavy Trucks Buses | 0 | 28 | 0 |  | 0 | 16 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  |  | 4 |
| Pedestrians |  | 0 |  |  |  | 0 |  |  |  | 0 |  |  |  | 0 |  |  |  |  |
| Bicycles Scooters | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  |  | 0 |

Comments:

Peak-Hour: 7:00 AM -- 8:00 AM
Peak 15-Min: 7:00 AM -- 7:15 AM


| 15-Min Count Period Beginning At | Moody Pkwy (Northbound) |  |  |  | Moody Pkwy (Southbound) |  |  |  | Bethel Rd(Eastbound) |  |  |  | Bethel Rd(Westbound) |  |  |  | Total | Hourly Totals |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U |  |  |
| 7:00 AM | 0 | 95 | 0 | 0 | 0 | 261 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 357 |  |
| 7:15 AM | 0 | 64 | 0 | 0 | 0 | 244 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 308 |  |
| 7:30 AM | 0 | 85 | 0 | 0 | 1 | 223 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 311 |  |
| 7:45 AM | 0 | 81 | 0 | 0 | 1 | 187 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 269 | 1245 |
| 8:00 AM | 0 | 59 | 0 | 0 | 0 | 155 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 215 | 1103 |
| 8:15 AM | 0 | 60 | 0 | 0 | 0 | 133 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 193 | 988 |
| 8:30 AM | 0 | 79 | 0 | 0 | 2 | 130 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 211 | 888 |
| 8:45 AM | 0 | 62 | 0 | 0 | 1 | 148 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 213 | 832 |
| Peak 15-Min Flowrates | Northbound |  |  |  | Southbound |  |  |  | Eastbound |  |  |  | Westbound |  |  |  | Total |  |
|  | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U |  |  |  |
| All Vehicles | 0 | 380 | 0 | 0 | 0 | 1044 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 0 |  | 28 |
| Heavy Trucks Buses | 0 | 44 | 0 |  | 0 | 36 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  |  | 0 |
| Pedestrians |  | 0 |  |  |  | 0 |  |  |  | 0 |  |  |  | 0 |  |  |  | 0 |
| Bicycles Scooters | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  |  | 0 |

Comments:



Peak-Hour: 7:00 AM -- 8:00 AM
Peak 15-Min: 7:30 AM -- 7:45 AM


Quality Counts
DATA THAT DREES COMMUNITES


| $\begin{gathered} \text { 15-Min Count } \\ \text { Period } \\ \text { Beginning At } \end{gathered}$ | Moody Pkwy (Northbound) |  |  |  | Moody Pkwy (Southbound) |  |  |  | High School Dr (Eastbound) |  |  |  | High School Dr (Westbound) |  |  |  | Total | Hourly Totals |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U |  |  |
| 6:00 AM | 0 | 27 | 2 | 0 | 2 | 120 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 153 |  |
| 6:15 AM | 0 | 30 | 13 | 0 | 4 | 177 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 3 | 0 | 231 |  |
| 6:30 AM | 0 | 37 | 25 | 0 | 7 | 178 | 0 | 0 | 0 | 0 | 0 | 0 | 19 | 0 | 3 | 0 | 269 |  |
| 6:45 AM | 0 | 52 | 9 | 0 | 5 | 192 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 0 | 1 | 0 | 266 | 919 |
| 7:00 AM | 0 | 81 | 32 | 0 | 24 | 192 | 0 | 0 | 1 | 0 | 0 | 0 | 7 | 0 | 2 | 0 | 339 | 1105 |
| 7:15 AM | 0 | 77 | 67 | 0 | 21 | 162 | 0 | 0 | 0 | 0 | 0 | 0 | 45 | 0 | 9 | 0 | 381 | 1255 |
| 7:30 AM | 0 | 111 | 121 | 0 | 32 | 174 | 0 | 0 | 0 | 0 | 1 | 0 | 94 | 0 | 34 | 0 | 567 | 1553 |
| 7:45 AM | 0 | 68 | 70 | 0 | 22 | 169 | 0 | 0 | 0 | 0 | 0 | 0 | 58 | 0 | 31 | 0 | 418 | 1705 |
| 8:00 AM | 0 | 59 | 12 | 0 | 6 | 138 | 0 | 0 | 0 | 0 | 0 | 0 | 10 | 0 | 6 | 0 | 231 | 1597 |
| 8:15 AM | 0 | 56 | 10 | 0 | 3 | 140 | 0 | 1 | 0 | 0 | 0 | 0 | 6 | 0 | 0 | 0 | 216 | 1432 |
| 8:30 AM | 0 | 68 | 18 | 0 | 2 | 136 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 0 | 1 | 0 | 233 | 1098 |
| 8:45 AM | 0 | 64 | 6 | 0 | 2 | 153 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 0 | 2 | 0 | 234 | 914 |
| 9:00 AM | 1 | 53 | 7 | 0 | 0 | 157 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 221 | 904 |
| 9:15 AM | 0 | 57 | 19 | 0 | 3 | 125 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 0 | 2 | 0 | 213 | 901 |
| 9:30 AM | 1 | 62 | 16 | 0 | 4 | 87 | 0 | 0 | 0 | 0 | 0 | 0 | 10 | 0 | 4 | 0 | 184 | 852 |
| 9:45 AM | 0 | 64 | 3 | 0 | 1 | 95 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 3 | 0 | 169 | 787 |
| 10:00 AM | 0 | 70 | 7 | 0 | 1 | 90 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 0 | 1 | 0 | 175 | 741 |
| 10:15 AM | 0 | 80 | 4 | 0 | 4 | 112 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 203 | 731 |
| 10:30 AM | 0 | 71 | 7 | 0 | 1 | 104 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 4 | 0 | 188 | 735 |
| 10:45 AM | 0 | 72 | 4 | 0 | 0 | 97 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 1 | 0 | 177 | 743 |
| 11:00 AM | 1 | 84 | 9 | 0 | 3 | 105 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 0 | 2 | 0 | 211 | 779 |
| 11:15 AM | 0 | 95 | 7 | 0 | 3 | 86 | 0 | 1 | 0 | 0 | 0 | 0 | 6 | 0 | 4 | 0 | 202 | 778 |
| 11:30 AM | 0 | 89 | 6 | 0 | 4 | 111 | 0 | 0 | 0 | 0 | 0 | 0 | 9 | 0 | 2 | 0 | 221 | 811 |
| 11:45 AM | 0 | 85 | 11 | 0 | 2 | 103 | 0 | 0 | 0 | 0 | 0 | 0 | 10 | 0 | 3 | 0 | 214 | 848 |
| 12:00 PM | 0 | 99 | 16 | 0 | 2 | 108 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 0 | 1 | 0 | 233 | 870 |
| 12:15 PM | 0 | 95 | 5 | 0 | 1 | 106 | 0 | 1 | 0 | 0 | 0 | 0 | 15 | 0 | 2 | 0 | 225 | 893 |
| 12:30 PM | 0 | 92 | 9 | 0 | 2 | 111 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 2 | 0 | 220 | 892 |
| 12:45 PM | 0 | 109 | 9 | 0 | 4 | 108 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 0 | 1 | 0 | 238 | 916 |
| 1:00 PM | 0 | 106 | 16 | 0 | 3 | 90 | 0 | 0 | 0 | 0 | 0 | 0 | 9 | 0 | 4 | 0 | 228 | 911 |
| 1:15 PM | 0 | 112 | 4 | 0 | 3 | 82 | 0 | 0 | 0 | 0 | 1 | 0 | 13 | 0 | 2 | 0 | 217 | 903 |
| 1:30 PM | 1 | 129 | 3 | 0 | 3 | 113 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 0 | 1 | 0 | 258 | 941 |
| 1:45 PM | 0 | 137 | 10 | 0 | 1 | 76 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 3 | 0 | 231 | 934 |
| 2:00 PM | 1 | 121 | 14 | 0 | 5 | 112 | 0 | 0 | 0 | 0 | 0 | 0 | 23 | 0 | 12 | 0 | 288 | 994 |
| 2:15 PM | 0 | 120 | 16 | 0 | 5 | 111 | 0 | 0 | 0 | 0 | 0 | 0 | 31 | 0 | 6 | 0 | 289 | 1066 |
| 2:30 PM | 0 | 144 | 21 | 0 | 5 | 80 | 0 | 0 | 0 | 0 | 0 | 0 | 24 | 0 | 9 | 0 | 283 | 1091 |
| 2:45 PM | 0 | 160 | 51 | 0 | 15 | 115 | 0 | 0 | 0 | 0 | 0 | 0 | 28 | 0 | 5 | 0 | 374 | 1234 |
| 3:00 PM | 0 | 146 | 16 | 0 | 3 | 78 | 0 | 0 | 0 | 0 | 0 | 0 | 131 | 0 | 48 | 0 | 422 | 1368 |
| 3:15 PM | 0 | 150 | 9 | 0 | 2 | 110 | 0 | 0 | 0 | 0 | 0 | 0 | 66 | 0 | 30 | 0 | 367 | 1446 |


| 15-Min Count Period Beginning At | Moody Pkwy (Northbound) |  |  |  | Moody Pkwy (Southbound) |  |  |  | High School Dr (Eastbound) |  |  |  | High School Dr (Westbound) |  |  |  | Total | Hourly Totals |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U |  |  |
| 3:30 PM | 0 | 162 | 12 | 0 | 3 | 110 | 0 | 0 | 0 | 0 | 0 | 0 | 17 | 0 | 7 | 0 | 311 | 1474 |
| 3:45 PM | 0 | 142 | 15 | 0 | 4 | 121 | 0 | 0 | 0 | 0 | 1 | 0 | 20 | 0 | 13 | 0 | 316 | 1416 |
| 4:00 PM | 0 | 171 | 14 | 0 | 8 | 106 | 0 | 0 | 0 | 0 | 0 | 0 | 19 | 0 | 9 | 0 | 327 | 1321 |
| 4:15 PM | 0 | 157 | 8 | 0 | 0 | 85 | 0 | 0 | 0 | 0 | 0 | 0 | 9 | 0 | 5 | 0 | 264 | 1218 |
| 4:30 PM | 0 | 150 | 17 | 0 | 3 | 103 | 0 | 0 | 0 | 0 | 0 | 0 | 9 | 0 | 3 | 0 | 285 | 1192 |
| 4:45 PM | 0 | 161 | 13 | 0 | 5 | 101 | 0 | 0 | 0 | 0 | 0 | 0 | 16 | 0 | 6 | 0 | 302 | 1178 |
| 5:00 PM | 0 | 164 | 22 | 0 | 7 | 83 | 0 | 0 | 0 | 0 | 0 | 0 | 23 | 0 | 11 | 0 | 310 | 1161 |
| 5:15 PM | 0 | 184 | 22 | 0 | 7 | 109 | 0 | 0 | 0 | 0 | 0 | 0 | 23 | 0 | 8 | 0 | 353 | 1250 |
| 5:30 PM | 0 | 184 | 10 | 0 | 2 | 101 | 0 | 0 | 0 | 0 | 0 | 0 | 19 | 0 | 9 | 0 | 325 | 1290 |
| 5:45 PM | 0 | 170 | 6 | 0 | 2 | 106 | 0 | 0 | 0 | 0 | 0 | 0 | 13 | 0 | 4 | 0 | 301 | 1289 |
| 6:00 PM | 0 | 172 | 4 | 0 | 0 | 108 | 0 | 0 | 0 | 0 | 0 | 0 | 11 | 0 | 5 | 0 | 300 | 1279 |
| 6:15 PM | 0 | 142 | 4 | 0 | 0 | 91 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 0 | 5 | 0 | 248 | 1174 |
| 6:30 PM | 0 | 121 | 0 | 0 | 0 | 74 | 0 | 0 | 0 | 0 | 0 | 0 | 9 | 0 | 1 | 0 | 205 | 1054 |
| 6:45 PM | 0 | 113 | 3 | 0 | 0 | 68 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 186 | 939 |
| 7:00 PM | 0 | 112 | 1 | 0 | 0 | 59 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 174 | 813 |
| 7:15 PM | 0 | 104 | 3 | 1 | 0 | 47 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 155 | 720 |
| 7:30 PM | 0 | 98 | 2 | 0 | 0 | 51 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 155 | 670 |
| 7:45 PM | 0 | 119 | 6 | 0 | 0 | 65 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 191 | 675 |
| Peak 15-Min Flowrates | Northbound |  |  |  | Southbound |  |  |  | Eastbound |  |  |  | Westbound |  |  |  | Total |  |
|  | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U |  |  |  |
| All Vehicles | 0 | 444 | 484 | 0 | 128 | 696 | 0 | 0 | 0 | 0 | 4 | 0 | 376 | 0 | 136 | 0 |  |  |
| Heavy Trucks Buses | 0 | 20 | 32 |  | 4 | 20 | 0 |  | 0 | 0 | 0 |  | 8 | 0 | 0 |  |  |  |
| Pedestrians |  | 0 |  |  |  | 0 |  |  |  | 0 |  |  |  | 0 |  |  |  |  |
| Bicycles Scooters | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  |  |  |
| Comments: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

Type of report: Tube Count - Volume Data


Type of report: Tube Count - Volume Data


Type of report: Tube Count - Speed Data

| LOCATION: Moody Pkwy approx. 1200' south of James Taylor Rd SPECIFIC LOCATION: <br> CITY/STATE: Moody, AL |  |  |  |  |  |  |  |  |  |  |  |  |  |  | QC JOB \#: 15768816 DIRECTION: NB, SB DATE: May 42022 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | 1 | 16 | 21 | 26 | 31 | 36 | 41 | 46 | 51 | 56 | 61 | 66 | 71 |  | Total | Pace Speed | Number in Pace |
|  | 15 | 20 | 25 | 30 | 35 | 40 | 45 | 50 | 55 | 60 | 65 | 70 | 75 | 999 |  |  |  |
| 12:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 18 | 17 | 13 | 6 | 0 | 0 | 0 | 59 | 46-55 | 35 |
| 01:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 9 | 13 | 2 | 2 | 0 | 0 | 0 | 30 | 46-55 | 22 |
| 02:00 AM | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 6 | 18 | 6 | 1 | 0 | 0 | 0 | 35 | 46-55 | 24 |
| 03:00 AM | 1 | 0 | 0 | 0 | 0 | 0 | 2 | 13 | 21 | 18 | 4 | 1 | 1 | 0 | 61 | 51-60 | 39 |
| 04:00 AM | 1 | 0 | 1 | 0 | 0 | 0 | 3 | 34 | 57 | 52 | 7 | 3 | 2 | 1 | 161 | 51-60 | 109 |
| 05:00 AM | 5 | 0 | 0 | 0 | 0 | 0 | 8 | 62 | 189 | 135 | 22 | 1 | 0 | 0 | 422 | 51-60 | 324 |
| 06:00 AM | 29 | 2 | 1 | 0 | 0 | 0 | 20 | 139 | 443 | 215 | 27 | 2 | 1 | 0 | 879 | 51-60 | 658 |
| 07:00 AM | 126 | 15 | 1 | 0 | 9 | 36 | 193 | 525 | 391 | 103 | 5 | 0 | 0 | 0 | 1404 | 46-55 | 916 |
| 08:00 AM | 30 | 2 | 0 | 8 | 11 | 8 | 26 | 170 | 396 | 192 | 41 | 6 | 0 | 1 | 891 | 51-60 | 588 |
| 09:00 AM | 44 | 4 | 0 | 0 | 0 | 5 | 29 | 192 | 354 | 146 | 18 | 3 | 0 | 1 | 796 | 46-55 | 546 |
| 10:00 AM | 28 | 1 | 2 | 0 | 4 | 15 | 57 | 219 | 281 | 110 | 19 | 0 | 0 | 0 | 736 | 46-55 | 500 |
| 11:00 AM | 47 | 1 | 0 | 0 | 2 | 4 | 52 | 206 | 325 | 174 | 25 | 2 | 0 | 0 | 838 | 46-55 | 531 |
| 12:00 PM | 52 | 2 | 0 | 0 | 1 | 3 | 57 | 241 | 402 | 126 | 19 | 4 | 0 | 0 | 907 | 46-55 | 643 |
| 01:00 PM | 64 | 5 | 3 | 4 | 3 | 13 | 83 | 258 | 317 | 153 | 26 | 3 | 1 | 0 | 933 | 46-55 | 575 |
| 02:00 PM | 81 | 8 | 0 | 1 | 4 | 25 | 153 | 460 | 330 | 101 | 12 | 2 | 0 | 0 | 1177 | 46-55 | 790 |
| 03:00 PM | 96 | 4 | 0 | 1 | 3 | 27 | 146 | 449 | 404 | 117 | 15 | 0 | 0 | 0 | 1262 | 46-55 | 853 |
| 04:00 PM | 46 | 3 | 5 | 0 | 1 | 0 | 26 | 90 | 101 | 17 | 2 | 0 | 0 | 1 | 292 | 46-55 | 191 |
| 05:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1-10 | 0 |
| 06:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1-10 | 0 |
| 07:00 PM | 38 | 4 | 2 | 1 | 2 | 13 | 66 | 234 | 305 | 83 | 13 | 2 | 0 | 0 | 763 | 46-55 | 539 |
| 08:00 PM | 13 | 0 | 0 | 4 | 2 | 20 | 73 | 207 | 165 | 69 | 7 | 3 | 2 | 0 | 565 | 46-55 | 372 |
| 09:00 PM | 4 | 0 | 0 | 0 | 0 | 2 | 38 | 129 | 140 | 58 | 15 | 3 | 0 | 0 | 389 | 46-55 | 269 |
| 10:00 PM | 4 | 0 | 0 | 0 | 0 | 0 | 16 | 52 | 77 | 31 | 10 | 0 | 0 | 0 | 190 | 46-55 | 129 |
| 11:00 PM | 1 | 0 | 1 | 0 | 1 | 0 | 6 | 35 | 36 | 20 | 6 | 1 | 0 | 2 | 109 | 46-55 | 71 |
| Day Total | 710 | 51 | 16 | 19 | 43 | 172 | 1066 | 3748 | 4782 | 1941 | 302 | 36 | 7 | 6 |  |  |  |
| Percent | 5.5\% | 0.4\% | 0.1\% | 0.1\% | 0.3\% | 1.3\% | 8.3\% | 29.1\% | 37.1\% | 15\% | 2.3\% | 0.3\% | 0.1\% | 0\% | 12899 | 46-55 | 8530 |
|  |  |  |  |  |  |  |  |  |  |  |  | - |  |  |  |  |  |
| AM Peak Volume | $\begin{gathered} \hline 7: 00 \mathrm{AM} \\ 126 \end{gathered}$ | $\begin{gathered} \hline 7: 00 \mathrm{AM} \\ 15 \\ \hline \end{gathered}$ | $\begin{gathered} \hline 10: 00 \mathrm{AM} \\ 2 \\ \hline \end{gathered}$ | $\begin{gathered} \hline 8: 00 \text { AM } \\ 8 \\ \hline \end{gathered}$ | $\begin{gathered} \hline 8: 00 \text { AM } \\ 11 \\ \hline \end{gathered}$ | $\begin{gathered} 7: 00 \mathrm{AM} \\ 36 \\ \hline \end{gathered}$ | $\begin{gathered} \hline 7: 00 \mathrm{AM} \\ 193 \\ \hline \end{gathered}$ | $\begin{gathered} \hline 7: 00 \mathrm{AM} \\ 525 \\ \hline \end{gathered}$ | $\begin{gathered} \text { 6:00 AM } \\ 443 \end{gathered}$ | $\begin{gathered} \hline 6: 00 \mathrm{AM} \\ 215 \\ \hline \end{gathered}$ | $\begin{gathered} 8: 00 \mathrm{AM} \\ 41 \\ \hline \end{gathered}$ | $\begin{gathered} \hline 8: 00 \mathrm{AM} \\ 6 \\ \hline \end{gathered}$ | $\begin{gathered} \hline 4: 00 \mathrm{AM} \\ 2 \\ \hline \end{gathered}$ | $\begin{gathered} \hline 4: 00 \mathrm{AM} \\ 1 \\ \hline \end{gathered}$ | $\begin{gathered} \hline 7: 00 \mathrm{AM} \\ 1404 \\ \hline \end{gathered}$ |  |  |
| PM Peak Volume | $\begin{gathered} 3: 00 \text { PM } \\ 96 \end{gathered}$ | $\begin{gathered} \text { 2:00 PM } \\ 8 \end{gathered}$ | $\begin{gathered} 4: 00 \text { PM } \\ 5 \end{gathered}$ | $\begin{gathered} \text { 1:00 PM } \\ 4 \end{gathered}$ | $\begin{gathered} 2: 00 \text { PM } \\ 4 \end{gathered}$ | $\begin{gathered} 3: 00 \text { PM } \\ 27 \end{gathered}$ | $\begin{gathered} \text { 2:00 PM } \\ 153 \end{gathered}$ | $\begin{gathered} \hline \text { 2:00 PM } \\ 460 \end{gathered}$ | $\begin{gathered} 3: 00 \mathrm{PM} \\ 404 \end{gathered}$ | $\begin{gathered} \hline \text { 1:00 PM } \\ 153 \end{gathered}$ | $\begin{gathered} \text { 1:00 PM } \\ 26 \end{gathered}$ | $\begin{gathered} 12: 00 \mathrm{PM} \\ 4 \end{gathered}$ | $\begin{gathered} \text { 8:00 PM } \\ 2 \end{gathered}$ | $\begin{gathered} 11: 00 ~ P M \\ 2 \end{gathered}$ | $\begin{gathered} \text { 3:00 PM } \\ 1262 \end{gathered}$ |  |  |
| Comments: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |


| LOCATION: M SPECIFIC LOC CITY/STATE: | ody Pk ION: <br> ody, |  | $200 \mathrm{~s}$ | of Ja | $5 \text { Tayl }$ |  |  |  |  |  |  |  |  |  |  | $\begin{gathered} \hline \text { QC JOB } \\ \text { DIREC } \\ \text { DATE } \end{gathered}$ | 15768816 ON: NB, SB May 42022 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Speed Range | $\begin{gathered} 1 \\ \hline 15 \end{gathered}$ | $\begin{aligned} & 16 \\ & 20 \end{aligned}$ | $\begin{aligned} & 21 \\ & 25 \end{aligned}$ | $\begin{aligned} & 26 \\ & 30 \end{aligned}$ | $\begin{aligned} & 31 \\ & 35 \end{aligned}$ | $\begin{aligned} & 36 \\ & 40 \end{aligned}$ | $\begin{aligned} & 41 \\ & 45 \end{aligned}$ | $\begin{aligned} & 46 \\ & 50 \end{aligned}$ | $\begin{aligned} & 51 \\ & 55 \end{aligned}$ | $\begin{aligned} & 56 \\ & 60 \end{aligned}$ | $\begin{aligned} & \hline 61 \\ & 65 \end{aligned}$ | $\begin{aligned} & \hline 66 \\ & 70 \end{aligned}$ | $\begin{aligned} & 71 \\ & 75 \end{aligned}$ | $\begin{gathered} \hline 76 \\ 999 \end{gathered}$ | Total | Pace Speed | Number in Pace |
| Grand Total Percent | $\begin{gathered} \hline 710 \\ 5.5 \% \end{gathered}$ | $\begin{gathered} 51 \\ 0.4 \% \end{gathered}$ | $\begin{gathered} \hline 16 \\ 0.1 \% \end{gathered}$ | $\begin{gathered} \hline 19 \\ 0.1 \% \end{gathered}$ | $\begin{gathered} \hline 43 \\ 0.3 \% \end{gathered}$ | $\begin{gathered} \hline 172 \\ 1.3 \% \end{gathered}$ | $\begin{aligned} & \hline 1066 \\ & 8.3 \% \end{aligned}$ | $\begin{aligned} & \hline 3748 \\ & 29.1 \% \end{aligned}$ | $\begin{aligned} & \hline 4782 \\ & 37.1 \% \end{aligned}$ | $\begin{gathered} \hline 1941 \\ 15 \% \end{gathered}$ | $\begin{gathered} \hline 302 \\ 2.3 \% \end{gathered}$ | $\begin{gathered} \hline 36 \\ 0.3 \% \end{gathered}$ | $\begin{gathered} \hline 7 \\ 0.1 \% \end{gathered}$ | $\begin{gathered} 6 \\ 0 \% \end{gathered}$ | 12899 | 46-55 | 8530 |
| Cumulative Percent | 5.5\% | 5.9\% | 6\% | 6.2\% | 6.5\% | 7.8\% | 16.1\% | 45.2\% | 82.2\% | 97.3\% | 99.6\% | 99.9\% | 100\% | 100\% |  |  |  |
| $\begin{aligned} & \text { ADT } \\ & 12899 \end{aligned}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 85th Perce Speed(Aver | ile: 56 MPH <br> e): 50 MPH <br> an: 51 MPH <br> de: 53 MPH |
| Comments: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

Type of report: Tube Count - Vehicle Classification Data

| LOCATION: SPECIFIC LO CITY/STATE: | oody Pkwy ap TION: <br> Moody, AL | $\text { prox. } 120$ | south of | mes Tayl |  |  |  |  |  |  |  |  |  | QC JOB DIRECT DATE: |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Motorcycles |  <br> Trailer | 2 Axle Long | Buses | 2 Axle 6 Tire | 3 Axle Single | 4 Axle Single | <5 Axle Double | 5 Axle Double | >6 Axle Double | <6 Axle <br> Multi | 6 Axle Multi | >6 Axle Multi | Not Classified | Total |
| 12:00 AM | 0 | 31 | 19 | 2 | 6 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 59 |
| 01:00 AM | 0 | 24 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 30 |
| 02:00 AM | 0 | 21 | 11 | 0 | 1 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 35 |
| 03:00 AM | 0 | 35 | 22 | 0 | 2 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 61 |
| 04:00 AM | 0 | 95 | 50 | 0 | 12 | 2 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 161 |
| 05:00 AM | 2 | 223 | 131 | 5 | 46 | 4 | 0 | 5 | 1 | 0 | 0 | 0 | 0 | 5 | 422 |
| 06:00 AM | 7 | 510 | 218 | 10 | 80 | 6 | 1 | 13 | 6 | 0 | 0 | 0 | 0 | 28 | 879 |
| 07:00 AM | 41 | 749 | 340 | 31 | 73 | 9 | 5 | 28 | 4 | 3 | 0 | 0 | 0 | 121 | 1404 |
| 08:00 AM | 5 | 511 | 250 | 10 | 58 | 3 | 1 | 17 | 6 | 2 | 0 | 0 | 0 | 28 | 891 |
| 09:00 AM | 14 | 436 | 207 | 12 | 56 | 4 | 2 | 18 | 4 | 0 | 0 | 0 | 0 | 43 | 796 |
| 10:00 AM | 9 | 398 | 208 | 9 | 58 | 2 | 1 | 16 | 7 | 1 | 0 | 0 | 0 | 27 | 736 |
| 11:00 AM | 10 | 444 | 236 | 9 | 56 | 6 | 1 | 24 | 4 | 1 | 0 | 0 | 0 | 47 | 838 |
| 12:00 PM | 6 | 486 | 265 | 5 | 60 | 7 | 4 | 19 | 2 | 2 | 0 | 0 | 0 | 51 | 907 |
| 01:00 PM | 10 | 519 | 239 | 8 | 55 | 8 | 3 | 26 | 2 | 0 | 0 | 0 | 0 | 63 | 933 |
| 02:00 PM | 20 | 661 | 274 | 22 | 74 | 8 | 4 | 33 | 4 | 1 | 0 | 1 | 0 | 75 | 1177 |
| 03:00 PM | 17 | 698 | 323 | 30 | 60 | 7 | 4 | 22 | 4 | 1 | 0 | 0 | 0 | 96 | 1262 |
| 04:00 PM | 10 | 145 | 73 | 4 | 13 | 2 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 42 | 292 |
| 05:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 06:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:00 PM | 9 | 462 | 200 | 3 | 33 | 2 | 2 | 10 | 4 | 0 | 0 | 0 | 0 | 38 | 763 |
| 08:00 PM | 7 | 389 | 120 | 2 | 23 | 4 | 1 | 2 | 2 | 0 | 0 | 0 | 0 | 15 | 565 |
| 09:00 PM | 3 | 271 | 97 | 0 | 10 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 4 | 389 |
| 10:00 PM | 0 | 134 | 38 | 0 | 5 | 0 | 0 | 3 | 6 | 0 | 0 | 0 | 0 | 4 | 190 |
| 11:00 PM | 1 | 75 | 21 | 1 | 6 | 0 | 0 | 0 | 3 | 0 | 1 | 0 | 0 | 1 | 109 |
| Day Total | 171 | 7317 | 3348 | 163 | 787 | 74 | 29 | 239 | 68 | 11 | 1 | 1 | 0 | 690 | 12899 |
| Percent | 1.3\% | 56.7\% | 26\% | 1.3\% | 6.1\% | 0.6\% | 0.2\% | 1.9\% | 0.5\% | 0.1\% | 0\% | 0\% | 0\% | 5.3\% | 12899 |
| $\begin{gathered} \text { ADT } \\ 12899 \end{gathered}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| AM Peak Volume | $\begin{gathered} \hline 7: 00 \mathrm{AM} \\ 41 \end{gathered}$ | $\begin{gathered} \hline 7: 00 \mathrm{AM} \\ 749 \end{gathered}$ | $\begin{gathered} \hline 7: 00 \mathrm{AM} \\ 340 \end{gathered}$ | $\begin{gathered} \hline 7: 00 \mathrm{AM} \\ 31 \end{gathered}$ | $\begin{gathered} \hline 6: 00 \mathrm{AM} \\ 80 \end{gathered}$ | $\begin{gathered} 7: 00 \mathrm{AM} \\ 9 \end{gathered}$ | $\begin{gathered} 7: 00 \mathrm{AM} \\ 5 \end{gathered}$ | $\begin{gathered} 7: 00 \mathrm{AM} \\ 28 \end{gathered}$ | $\begin{gathered} \text { 10:00 AM } \\ 7 \\ \hline \end{gathered}$ | $\begin{gathered} \hline 7: 00 \mathrm{AM} \\ 3 \\ \hline \end{gathered}$ | $\begin{gathered} 12: 00 \mathrm{AM} \\ 0 \end{gathered}$ | $\begin{gathered} \text { 12:00 AM } \\ 0 \end{gathered}$ | $\begin{gathered} 12: 00 \mathrm{AM} \\ 0 \end{gathered}$ | $\begin{gathered} 7: 00 \text { AM } \\ 121 \end{gathered}$ | $\begin{gathered} \hline 7: 00 \mathrm{AM} \\ 1404 \end{gathered}$ |
| PM Peak | 2:00 PM | 3:00 PM | 3:00 PM | 3:00 PM | 2:00 PM | 1:00 PM | 12:00 PM | 2:00 PM | 10:00 PM | 12:00 PM | 11:00 PM | 2:00 PM | 12:00 PM | 3:00 PM | 3:00 PM |
| Volume | 20 | 698 | 323 | 30 | 74 | 8 | 4 | 33 | 6 | 2 | 1 | 1 | 0 | 96 | 1262 |
| Comments: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |



Type of report: Tube Count - Volume Data


Type of report: Tube Count - Speed Data


| LOCATION: M SPECIFIC LOC CITY/STATE: | dy Pk <br> ION: <br> ody, |  | $\overline{100^{\prime} \mathrm{nd}}$ | of Be |  |  |  |  |  |  |  |  |  |  |  | QC JOB DIREC DATE: | $: 15768817$ <br> ON: NB, SB <br> May 42022 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Speed Range | $\begin{gathered} \hline 1 \\ 15 \end{gathered}$ | $\begin{aligned} & 16 \\ & 20 \end{aligned}$ | $\begin{aligned} & 21 \\ & 25 \end{aligned}$ | $\begin{aligned} & 26 \\ & 30 \end{aligned}$ | $\begin{aligned} & 31 \\ & 35 \end{aligned}$ | $\begin{aligned} & 36 \\ & 40 \end{aligned}$ | $\begin{aligned} & 41 \\ & 45 \end{aligned}$ | $\begin{aligned} & 46 \\ & 50 \end{aligned}$ | $\begin{aligned} & 51 \\ & 55 \end{aligned}$ | $\begin{aligned} & \hline 56 \\ & 60 \end{aligned}$ | $\begin{aligned} & \hline 61 \\ & 65 \end{aligned}$ | $\begin{aligned} & \hline 66 \\ & 70 \end{aligned}$ | $\begin{aligned} & 71 \\ & 75 \end{aligned}$ | $\begin{gathered} \hline 76 \\ 999 \end{gathered}$ | Total | Pace Speed | Number in Pace |
| Grand Total Percent | $\begin{gathered} \hline 568 \\ 3.9 \% \end{gathered}$ | $\begin{gathered} 12 \\ 0.1 \% \end{gathered}$ | $\begin{gathered} 22 \\ 0.2 \% \end{gathered}$ | $\begin{gathered} \hline 36 \\ 0.2 \% \end{gathered}$ | $\begin{gathered} \hline 108 \\ 0.7 \% \end{gathered}$ | $\begin{gathered} \hline 374 \\ 2.6 \% \end{gathered}$ | $\begin{aligned} & \hline 1413 \\ & 9.6 \% \end{aligned}$ | $\begin{aligned} & \hline 4631 \\ & 31.6 \% \end{aligned}$ | $\begin{aligned} & \hline 5145 \\ & 35.1 \% \end{aligned}$ | $\begin{gathered} \hline 1702 \\ 11.6 \% \end{gathered}$ | $\begin{gathered} \hline 492 \\ 3.4 \% \end{gathered}$ | $\begin{gathered} \hline 118 \\ 0.8 \% \end{gathered}$ | $\begin{gathered} \hline 20 \\ 0.1 \% \end{gathered}$ | $\begin{gathered} 15 \\ 0.1 \% \end{gathered}$ | 14656 | 46-55 | 9776 |
| Cumulative Percent | 3.9\% | 4\% | 4.1\% | 4.4\% | 5.1\% | 7.6\% | 17.3\% | 48.9\% | 84\% | 95.6\% | 99\% | 99.8\% | 99.9\% | 100\% |  |  |  |
| $\begin{aligned} & \text { ADT } \\ & 14656 \end{aligned}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 85th Perce n Speed(Aver Med | ile: 56 MPH <br> e): 50 MPH <br> an: 51 MPH <br> de: 53 MPH |
| Comments: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

Type of report: Tube Count - Vehicle Classification Data

| LOCATION: SPECIFIC LO CITY/STATE | oody Pkwy ap TION: <br> Moody, AL | $\text { prox. } 400$ | north of B | hel Rd |  |  |  |  |  |  |  |  |  | QC JOB \# DIRECT DATE: | $\begin{aligned} & 15768817 \\ & \text { N: NB, SB } \\ & \text { lay } 42022 \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Motorcycles |  <br> Trailer | 2 Axle Long | Buses | 2 Axle 6 Tire | 3 Axle Single | 4 Axle Single | <5 Axle Double | 5 Axle Double | >6 Axle Double | <6 Axle <br> Multi | 6 Axle Multi | >6 Axle <br> Multi | Not Classified | Total |
| 12:00 AM | 0 | 36 | 26 | 2 | 5 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 70 |
| 01:00 AM | 0 | 20 | 5 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 26 |
| 02:00 AM | 0 | 27 | 16 | 0 | 2 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 47 |
| 03:00 AM | 0 | 49 | 16 | 0 | 9 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 76 |
| 04:00 AM | 0 | 97 | 55 | 1 | 20 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 176 |
| 05:00 AM | 2 | 256 | 133 | 6 | 72 | 3 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 1 | 476 |
| 06:00 AM | 5 | 569 | 255 | 4 | 93 | 8 | 0 | 6 | 4 | 0 | 0 | 0 | 0 | 20 | 964 |
| 07:00 AM | 3 | 766 | 288 | 5 | 70 | 2 | 0 | 7 | 8 | 2 | 0 | 0 | 0 | 32 | 1183 |
| 08:00 AM | 2 | 490 | 238 | 6 | 56 | 2 | 0 | 11 | 5 | 2 | 0 | 0 | 0 | 19 | 831 |
| 09:00 AM | 2 | 401 | 166 | 8 | 72 | 6 | 0 | 14 | 4 | 0 | 0 | 0 | 0 | 23 | 696 |
| 10:00 AM | 5 | 397 | 177 | 6 | 51 | 4 | 0 | 11 | 5 | 1 | 0 | 0 | 0 | 16 | 673 |
| 11:00 AM | 4 | 444 | 216 | 8 | 49 | 5 | 2 | 8 | 3 | 0 | 0 | 0 | 0 | 26 | 765 |
| 12:00 PM | 3 | 499 | 205 | 8 | 54 | 8 | 0 | 11 | 5 | 1 | 0 | 0 | 0 | 35 | 829 |
| 01:00 PM | 4 | 514 | 231 | 8 | 54 | 4 | 0 | 11 | 4 | 1 | 0 | 0 | 0 | 30 | 861 |
| 02:00 PM | 9 | 602 | 236 | 11 | 58 | 6 | 1 | 7 | 4 | 0 | 0 | 0 | 0 | 47 | 981 |
| 03:00 PM | 7 | 650 | 289 | 8 | 85 | 4 | 1 | 11 | 3 | 0 | 1 | 0 | 0 | 67 | 1126 |
| 04:00 PM | 3 | 654 | 320 | 5 | 73 | 2 | 0 | 7 | 2 | 0 | 0 | 0 | 0 | 44 | 1110 |
| 05:00 PM | 10 | 678 | 284 | 2 | 85 | 5 | 1 | 11 | 0 | 0 | 0 | 0 | 0 | 88 | 1164 |
| 06:00 PM | 5 | 520 | 197 | 2 | 48 | 0 | 1 | 13 | 2 | 0 | 0 | 0 | 0 | 57 | 845 |
| 07:00 PM | 2 | 397 | 166 | 1 | 34 | 1 | 0 | 4 | 2 | 0 | 0 | 0 | 0 | 14 | 621 |
| 08:00 PM | 1 | 348 | 120 | 0 | 18 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 13 | 501 |
| 09:00 PM | 1 | 240 | 76 | 0 | 14 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 3 | 336 |
| 10:00 PM | 4 | 150 | 32 | 0 | 3 | 0 | 0 | 5 | 2 | 0 | 0 | 0 | 0 | 0 | 196 |
| 11:00 PM | 0 | 82 | 19 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 103 |
| Day Total | 72 | 8886 | 3766 | 91 | 1028 | 60 | 6 | 145 | 58 | 7 | 1 | 0 | 0 | 536 |  |
| Percent | 0.5\% | 60.6\% | 25.7\% | 0.6\% | 7\% | 0.4\% | 0\% | 1\% | 0.4\% | 0\% | 0\% | 0\% | 0\% | 3.7\% | 14656 |
| $\begin{gathered} \text { ADT } \\ 14656 \end{gathered}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| AM Peak Volume | $\begin{gathered} 6: 00 \mathrm{AM} \\ 5 \end{gathered}$ | $\begin{gathered} 7: 00 \mathrm{AM} \\ 766 \end{gathered}$ | $7: 00 \mathrm{AM}$ 288 | $\begin{gathered} 9: 00 \mathrm{AM} \\ 8 \end{gathered}$ | $\begin{gathered} \text { 6:00 AM } \\ 93 \end{gathered}$ | $\begin{gathered} \text { 6:00 AM } \\ 8 \end{gathered}$ | $\begin{gathered} 11: 00 \mathrm{AM} \\ 2 \end{gathered}$ | 9:00 AM 14 | 7:00 AM 8 | 7:00 AM 2 | $\begin{gathered} 12: 00 \mathrm{AM} \\ 0 \end{gathered}$ | $\begin{gathered} 12: 00 \mathrm{AM} \\ 0 \end{gathered}$ | $\begin{gathered} \text { 12:00 AM } \\ 0 \end{gathered}$ | 7:00 AM 32 | $\begin{gathered} \hline 7: 00 \mathrm{AM} \\ 1183 \end{gathered}$ |
| PM Peak | 5:00 PM | 5:00 PM | 4:00 PM | 2:00 PM | 3:00 PM | 12:00 PM | 2:00 PM | 6:00 PM | 12:00 PM | 12:00 PM | 3:00 PM | 12:00 PM | 12:00 PM | 5:00 PM | 5:00 PM |
| Volume | 10 | 678 | 320 | 11 | 85 | 8 | 1 | 13 | 5 | 1 | 1 | 0 | 0 | 88 | 1164 |
| Comments: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

Type of report: Tube Count - Vehicle Classification Data SUMMARY - Tube Count - Vehicle Classification Data
LOCATION: Moody Pkwy approx. 400' north of Bethel Rd

| LOCATION: SPECIFIC LOC CITY/STATE: | ody Pkwy ap TION: <br> oody, AL | $\text { rox. } 400$ | rth of | el Rd |  |  |  |  |  |  |  |  |  | QC JOB DIREC DATE | $\begin{aligned} & 15768817 \\ & \text { N: NB, SB } \\ & \text { ay } 42022 \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Motorcycles | Cars \& Trailer | 2 Axle Long | Buses | 2 Axle 6 Tire | 3 Axle Single | 4 Axle Single | <5 Axle Double | 5 Axle Double | >6 Axle Double | $\begin{gathered} \hline<6 \text { Axle } \\ \text { Multi } \end{gathered}$ | 6 Axle Multi | $\begin{gathered} \hline>6 \text { Axle } \\ \text { Multi } \end{gathered}$ | Not Classified | Total |
| Grand Total Percent | $\begin{gathered} \hline 72 \\ 0.5 \% \end{gathered}$ | $\begin{gathered} \hline 8886 \\ 60.6 \% \end{gathered}$ | $\begin{gathered} \hline 3766 \\ 25.7 \% \end{gathered}$ | $\begin{gathered} \hline 91 \\ 0.6 \% \end{gathered}$ | $\begin{gathered} 1028 \\ 7 \% \end{gathered}$ | $\begin{gathered} 60 \\ 0.4 \% \end{gathered}$ | $\begin{gathered} \hline 6 \\ 0 \% \\ \hline \end{gathered}$ | $\begin{gathered} \hline 145 \\ 1 \% \end{gathered}$ | $\begin{gathered} 58 \\ 0.4 \% \end{gathered}$ | $\begin{gathered} \hline 7 \\ 0 \% \end{gathered}$ | $\begin{gathered} 1 \\ 0 \% \end{gathered}$ | $\begin{gathered} \hline 0 \\ 0 \% \end{gathered}$ | $\begin{gathered} \hline 0 \\ 0 \% \end{gathered}$ | $\begin{gathered} \hline 536 \\ 3.7 \% \end{gathered}$ | 14656 |
| $\begin{gathered} \text { ADT } \\ 14656 \end{gathered}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Comments: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

## Appendix B - Level of Service Description

## Levels of Service Signalized Intersections

Level of service criteria for signalized intersections is defined in terms of delay. Delay is a measure of driver discomfort, frustration, fuel consumption, and lost travel time. Specifically, level-of-service criteria are stated in terms of the average stopped delay per vehicle for a 15-minute analysis period.

Level of service A describes operations with very low delay, less than 10 seconds per vehicle. This occurs when progression is extremely favorable, and most vehicles arrive during the green phase. Most vehicles do not stop at all. Short cycle lengths may also contribute to low delay.

Level of service B describes operations with delay in the range of > 10 to 20 seconds per vehicle. This generally occurs with good progression and/or short cycle lengths. More vehicles stop than for LOS A, causing higher levels of average delay.

Level of service C describes operations with delay in the range of > 20 to 35 seconds per vehicle. These higher delays may result from fair progression and/or longer cycle lengths. Individual cycle failures may begin to appear in this level. The number of vehicles stopping is significant at this level, although many still pass through the intersection without stopping.

Level of service $D$ describes operations with delay in the range of $>35$ to 55 seconds per vehicle. At level D , the influence of congestion becomes more noticeable. Longer delays may result from some combination of unfavorable progression, long cycle lengths, or high vehicle/capacity ratios. Many vehicles stop, and the proportion of vehicles not stopping declines. Individual cycle failures are noticeable.

Level of service E describes operations with delay in the range of $>55$ to 80 seconds per vehicle. This is considered to be the limit of acceptable delay. These high delay values generally indicate poor progression, long cycle lengths, and high vehicle/capacity ratios. Individual cycle failures are frequent occurrences.

Level of service $F$ describes operations with delay in excess of 80 seconds per vehicle. This is considered to be unacceptable to most drivers. This condition often occurs with over saturation, i.e., when arrival flow rates exceed the capacity of the intersection. Poor progression and long cycle lengths may also be major contributing causes to such delay levels.

## Levels of Service Unsignalized Intersections

Level of service criteria for unsignalized intersections is stated in terms of average control delay. Control delay is defined as the total elapsed time from a vehicle joining the queue until its departure from the stopped position at the head of the queue. The criteria for each level of service are cited in the table below.

| Level of <br> Service | Average Control Delay <br> (seconds/vehicle) |
| :---: | :---: |
| A | $0-10$ |
| B | $>10-15$ |
| C | $>15-25$ |
| D | $>25-35$ |
| E | $>50-50$ |
| F |  |

## Levels of Service Daily Volume

The criteria for daily level of service are derived from ALDOT defined roadway capacities for urban 2-lane and 3-lane arterials and are cited in the table below.

| Level of <br> Service | Daily Service Volume |  |
| :---: | ---: | ---: |
|  | 2-lane | 3-lane |
| A | 6,500 | 8,200 |
| B | 9,400 | 11,600 |
| C | 11,600 | 14,400 |
| D | 14,000 | 17,500 |
| E | 18,700 | 23,300 |
| F | $>18,700$ | $>23,300$ |

## Levels of Service: Unsignalized Intersections

Level of service criteria for unsignalized intersections is stated in terms of average control delay. Control delay is defined as the total elapsed time from a vehicle joining the queue until its departure from the stopped position at the head of the queve. The criteria for each level of service are cited in the table below.

| Level of Service | Average Control Delay <br> (seconds/vehicle) |
| :---: | :---: |
| A | $0-10$ |
| B | $>10-15$ |
| C | $>15-25$ |
| D | $>25-35$ |
| E | $>35-50$ |
| F | $>50$ |

## Appendix C - Existing Conditions Capacity Analysis Reports



| Major/Minor | Minor2 |  | Major1 |  | Major2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 1742 | 1064 | 1066 | 0 | - | 0 |
| Stage 1 | 1064 | - | - | - | - | - |
| Stage 2 | 678 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | 4.12 | - | - | - |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | 2.218 | - | - | - |
| Pot Cap-1 Maneuver | 95 | 271 | 654 | - | - | - |
| Stage 1 | 332 | - | - | - | - | - |
| Stage 2 | 504 | - | - | - | - | - |
| Platoon blocked, \% |  |  |  | - | - | - |
| Mov Cap-1 Maneuver | 91 | 271 | 654 | - | - | - |
| Mov Cap-2 Maneuver | 91 | - | - | - | - | - |
| Stage 1 | 316 | - | - | - | - | - |
| Stage 2 | 504 | - | - | - | - | - |
|  |  |  |  |  |  |  |
| Approach | SE |  | NE |  | SW |  |
| HCM Control Delay, s | 35.5 |  | 0.3 |  | 0 |  |
| HCM LOS | E |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NEL | NET SELn1 |  | SWT | SWR |
| Capacity (veh/h) |  | 654 | - | 216 | - | - |
| HCM Lane V/C Ratio |  | 0.03 | - | 0.468 | - | - |
| HCM Control Delay (s) |  | 10.7 | 0 | 35.5 | - | - |
| HCM Lane LOS |  | B | A | E | - | - |
| HCM 95th \%tile Q(veh) |  | 0.1 | - | 2.3 | - | - |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 22 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | SEL | SET | SER | NWL | NWT | NWR | NEL | NET | NER | SWL | SWT | SWR |
| Lane Configurations |  | $\ddagger$ |  |  | * |  |  | \& |  |  | * |  |
| Traffic Vol, veh/h | 21 | 1 | 33 | 79 | 0 | 31 | 5 | 563 | 27 | 17 | 876 | 10 |
| Future Vol, veh/h | 21 | 1 | 33 | 79 | 0 | 31 | 5 | 563 | 27 | 17 | 876 | 10 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 23 | 1 | 36 | 86 | 0 | 34 | 5 | 612 | 29 | 18 | 952 | 11 |



| Minor Lane/Major Mvmt | NEL | NET | NERNWLn1 SELn1 | SWL | SWT | SWR |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 715 | - | - | 88 | 133 | 943 | - |

## Notes

```
~: Volume exceeds capacity $: Delay exceeds 300s +: Computation Not Defined *: All major volume in platoon
```

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1.1 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | -1 | $\boldsymbol{F}$ |  | Mr |  |
| Traffic Vol, veh/h | 11 | 581 | 853 | 1 | 6 | 60 |
| Future Vol, veh/h | 11 | 581 | 853 | 1 | 6 | 60 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 12 | 632 | 927 | 1 | 7 | 65 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 2.2 |  |  |  |  |  |
| Movement | SEL | SER | NEL | NET | SWT | SWR |
| Lane Configurations | M |  |  | $\uparrow$ | $\uparrow$ |  |
| Traffic Vol, veh/h | 48 | 12 | 6 | 581 | 849 | 40 |
| Future Vol, veh/h | 48 | 12 | 6 | 581 | 849 | 40 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 52 | 13 | 7 | 632 | 923 | 43 |


| Major/Minor | Minor2 |  | Major1 |  | Major2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 1591 | 945 | 966 | 0 | - | 0 |
| Stage 1 | 945 | - | - | - | - | - |
| Stage 2 | 646 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | 4.12 | - | - | - |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | 2.218 | - | - | - |
| Pot Cap-1 Maneuver | 118 | 318 | 713 | - | - | - |
| Stage 1 | 378 | - | - | - | - | - |
| Stage 2 | 522 | - | - | - | - | - |
| Platoon blocked, \% |  |  |  | - | - | - |
| Mov Cap-1 Maneuver | 116 | 318 | 713 | - | - | - |
| Mov Cap-2 Maneuver | 116 | - | - | - | - | - |
| Stage 1 | 372 | - | - | - | - | - |
| Stage 2 | 522 | - | - | - | - | - |
|  |  |  |  |  |  |  |
| Approach | SE |  | NE |  | SW |  |
| HCM Control Delay, s | 55.7 |  | 0.1 |  | 0 |  |
| HCM LOS | F |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NEL | NET SELn1 |  | SWT | SWR |
| Capacity (veh/h) |  | 713 | - | 133 | - | - |
| HCM Lane V/C Ratio |  | 0.009 | - | 0.49 | - | - |
| HCM Control Delay (s) |  | 10.1 | 0 | 55.7 | - | - |
| HCM Lane LOS |  | B | A | F | - | - |
| HCM 95th \%tile Q(veh) |  | 0 | - | 2.3 | - | - |


| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 38.4 |  |  |  |  |  |  |
| Movement N | NWL | NWR | NET | NER | SWL | SWT |
| Lane Configurations | ${ }^{1}$ | 「 | 4 | 「 | ${ }^{7}$ | 4 |
| Traffic Vol, veh/h 204 | 204 | 76 | 337 | 290 | 99 | 697 |
| Future Vol, veh/h 204 | 204 | 76 | 337 | 290 | 99 | 697 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control Stop | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length 17 | 175 | 0 | - | 250 | 150 | - |
| Veh in Median Storage, \# | \# 0 | - | 0 | - | - | 0 |
| Grade, \% |  | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 222 | 83 | 366 | 315 | 108 | 758 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.3 |  |  |  |  |  |
| Movement | SEL | SER | NEL | NET | SWT | SWR |
| Lane Configurations | Mr |  |  | - | F |  |
| Traffic Vol, veh/h | 4 | 11 | 4 | 409 | 781 | 0 |
| Future Vol, veh/h | 4 | 11 | 4 | 409 | 781 | 0 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 4 | 12 | 4 | 445 | 849 | 0 |


| Major/Minor | Minor2 |  | Major1 |  | Major2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 1302 | 849 | 849 | 0 | - | 0 |
| Stage 1 | 849 | - | - | - | - | - |
| Stage 2 | 453 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | 4.12 | - | - | - |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | 2.218 | - | - | - |
| Pot Cap-1 Maneuver | 177 | 361 | 789 | - | - | - |
| Stage 1 | 419 | - | - | - | - | - |
| Stage 2 | 640 | - | - | - | - | - |
| Platoon blocked, \% |  |  |  | - | - | - |
| Mov Cap-1 Maneuver | 176 | 361 | 789 | - | - | - |
| Mov Cap-2 Maneuver | 176 | - | - | - | - | - |
| Stage 1 | 416 | - | - | - | - | - |
| Stage 2 | 640 | - | - | - | - | - |
|  |  |  |  |  |  |  |
| Approach | SE |  | NE |  | SW |  |
| HCM Control Delay, s | 18.5 |  | 0.1 |  | 0 |  |
| HCM LOS | C |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NEL | NET SELn1 |  | SWT | SWR |
| Capacity (veh/h) |  | 789 | - | 282 | - | - |
| HCM Lane V/C Ratio |  | 0.006 | - | 0.058 | - | - |
| HCM Control Delay (s) |  | 9.6 | 0 | 18.5 | - | - |
| HCM Lane LOS |  | A | A | C | - | - |
| HCM 95th \%tile Q(veh) |  | 0 | - | 0.2 | - | - |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1.4 |  |  |  |  |  |
| Movement | SEL | SER | NEL | NET | SWT | SWR |
| Lane Configurations | Mr |  |  | -1 | F |  |
| Traffic Vol, veh/h | 22 | 52 | 15 | 402 | 713 | 10 |
| Future Vol, veh/h | 22 | 52 | 15 | 402 | 713 | 10 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 24 | 57 | 16 | 437 | 775 | 11 |


| Major/Minor | Minor2 |  | Major1 |  | Major2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 1250 | 781 | 786 | 0 | - | 0 |
| Stage 1 | 781 | - | - | - | - | - |
| Stage 2 | 469 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | 4.12 | - | - | - |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | 2.218 | - | - | - |
| Pot Cap-1 Maneuver | 191 | 395 | 833 | - | - | - |
| Stage 1 | 451 | - | - | - | - | - |
| Stage 2 | 630 | - | - | - | - | - |
| Platoon blocked, \% |  |  |  | - | - | - |
| Mov Cap-1 Maneuver | 186 | 395 | 833 | - | - | - |
| Mov Cap-2 Maneuver | 186 | - | - | - | - | - |
| Stage 1 | 440 | - | - | - | - | - |
| Stage 2 | 630 | - | - | - | - | - |
|  |  |  |  |  |  |  |
| Approach | SE |  | NE |  | SW |  |
| HCM Control Delay, s | 21.6 |  | 0.3 |  | 0 |  |
| HCM LOS | C |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NEL | NET SELn1 |  | SWT | SWR |
| Capacity (veh/h) |  | 833 | - | 296 | - | - |
| HCM Lane V/C Ratio |  | 0.02 | - | 0.272 | - | - |
| HCM Control Delay (s) |  | 9.4 | 0 | 21.6 | - | - |
| HCM Lane LOS |  | A | A | C | - | - |
| HCM 95th \%tile Q(veh) |  | 0.1 | - | 1.1 | - | - |




| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0 |  |  |  |  |  |
| Movement | NBT | NBR | SBL | SBT | NWL | NWR |
| Lane Configurations | $\boldsymbol{\beta}$ |  |  | $\uparrow$ | Mr |  |
| Traffic Vol, veh/h | 325 | 0 | 2 | 915 | 1 | 2 |
| Future Vol, veh/h | 325 | 0 | 2 | 915 | 1 | 2 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 353 | 0 | 2 | 995 | 1 | 2 |


| Major/Minor | Major1 |  | Major2 |  | Minor1 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 0 | 0 | 353 | 0 | 1352 | 353 |
| Stage 1 | - | - | - | - | 353 | - |
| Stage 2 | - | - | - | - | 999 | - |
| Critical Hdwy | - | - | 4.12 | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | - | - | 2.218 | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | - | - | 1206 | - | 165 | 691 |
| Stage 1 | - | - | - | - | 711 | - |
| Stage 2 | - | - | - | - | 356 | - |
| Platoon blocked, \% | - | - |  | - |  |  |
| Mov Cap-1 Maneuver | - | - | 1206 | - | 164 | 691 |
| Mov Cap-2 Maneuver | - | - | - | - | 164 | - |
| Stage 1 | - | - | - | - | 711 | - |
| Stage 2 | - | - | - | - | 355 | - |
|  |  |  |  |  |  |  |
| Approach | NB |  | SB |  | NW |  |
| HCM Control Delay, s | 0 |  | 0 |  | 15.9 |  |
| HCM LOS |  |  |  |  | C |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBT | NBRNWLn1 |  | SBL | SBT |
| Capacity (veh/h) |  | - | - | 334 | 1206 | - |
| HCM Lane V/C Ratio |  | - | - | 0.01 | 0.002 | - |
| HCM Control Delay (s) |  | - | - | 15.9 | 8 | 0 |
| HCM Lane LOS |  | - | - | C | A | A |
| HCM 95th \%tile Q(veh) |  | - | - | 0 | 0 | - |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 3.3 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | NBL | NBT | NBR | SBL | SBT | SBR | SEL | SET | SER | NWL | NWT | NWR |
| Lane Configurations |  | * |  |  | * |  |  | * |  |  | \& |  |
| Traffic Vol, veh/h | 14 | 313 | 6 | 2 | 820 | 9 | 24 | 1 | 70 | 25 | 0 | 1 |
| Future Vol, veh/h | 14 | 313 | 6 | 2 | 820 | 9 | 24 | 1 | 70 | 25 | 0 | 1 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control F | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 15 | 340 | 7 | 2 | 891 | 10 | 26 | 1 | 76 | 27 | 0 | 1 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1.5 |  |  |  |  |  |
| Movement | SEL | SER | NEL | NET | SWT | SWR |
| Lane Configurations | M |  |  | - | b |  |
| Traffic Vol, veh/h | 10 | 56 | 85 | 905 | 588 | 18 |
| Future Vol, veh/h | 10 | 56 | 85 | 905 | 588 | 18 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 11 | 61 | 92 | 984 | 639 | 20 |


| Major/Minor | Minor2 |  | Major1 |  | Major2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 1817 | 649 | 659 | 0 | - | 0 |
| Stage 1 | 649 | - | - | - | - | - |
| Stage 2 | 1168 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | 4.12 | - | - | - |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | 2.218 | - | - | - |
| Pot Cap-1 Maneuver | 86 | 470 | 929 | - | - | - |
| Stage 1 | 520 | - | - | - | - | - |
| Stage 2 | 296 | - | - | - | - | - |
| Platoon blocked, \% |  |  |  | - | - | - |
| Mov Cap-1 Maneuver | 67 | 470 | 929 | - | - | - |
| Mov Cap-2 Maneuver | 67 | - | - | - | - | - |
| Stage 1 | 407 | - | - | - | - | - |
| Stage 2 | 296 | - | - | - | - | - |
|  |  |  |  |  |  |  |
| Approach | SE |  | NE |  | SW |  |
| HCM Control Delay, s | 25.5 |  | 0.8 |  | 0 |  |
| HCM LOS | D |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NEL | NET SELn1 |  | SWT | SWR |
| Capacity (veh/h) |  | 929 | - | 246 | - | - |
| HCM Lane V/C Ratio |  | 0.099 | - | 0.292 | - | - |
| HCM Control Delay (s) |  | 9.3 | 0 | 25.5 | - | - |
| HCM Lane LOS |  | A | A | D | - | - |
| HCM 95th \%tile Q(veh) |  | 0.3 | - | 1.2 | - | - |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 3.7 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | SEL | SET | SER | NWL | NWT | NWR | NEL | NET | NER | SWL | SWT | SWR |
| Lane Configurations |  | \& |  |  | \& |  |  | $\uparrow$ |  |  | $\uparrow$ |  |
| Traffic Vol, veh/h | 7 | 1 | 20 | 36 | 3 | 17 | 21 | 814 | 78 | 13 | 537 | 8 |
| Future Vol, veh/h | 7 | 1 | 20 | 36 | 3 | 17 | 21 | 814 | 78 | 13 | 537 | 8 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 8 | 1 | 22 | 39 | 3 | 18 | 23 | 885 | 85 | 14 | 584 | 9 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.7 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | -1 | 1 |  | 4 |  |
| Traffic Vol, veh/h | 68 | 768 | 494 | 0 | 1 | 32 |
| Future Vol, veh/h | 68 | 768 | 494 | 0 | 1 | 32 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 74 | 835 | 537 | 0 | 1 | 35 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.8 |  |  |  |  |  |
| Movement | SEL | SER | NEL | NET | SWT | SWR |
| Lane Configurations | Mr |  |  | - | F |  |
| Traffic Vol, veh/h | 21 | 12 | 16 | 747 | 463 | 18 |
| Future Vol, veh/h | 21 | 12 | 16 | 747 | 463 | 18 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 23 | 13 | 17 | 812 | 503 | 20 |


| Major/Minor | Minor2 |  | Major1 |  | Major2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 1359 | 513 | 523 | 0 | - | 0 |
| Stage 1 | 513 | - | - | - | - | - |
| Stage 2 | 846 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | 4.12 | - | - | - |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | 2.218 | - | - | - |
| Pot Cap-1 Maneuver | 164 | 561 | 1043 | - | - | - |
| Stage 1 | 601 | - | - | - | - | - |
| Stage 2 | 421 | - | - | - | - | - |
| Platoon blocked, \% |  |  |  | - | - | - |
| Mov Cap-1 Maneuver | 159 | 561 | 1043 | - | - | - |
| Mov Cap-2 Maneuver | 159 | - | - | - | - | - |
| Stage 1 | 583 | - | - | - | - | - |
| Stage 2 | 421 | - | - | - | - | - |
|  |  |  |  |  |  |  |
| Approach | SE |  | NE |  | SW |  |
| HCM Control Delay, s | 25.1 |  | 0.2 |  | 0 |  |
| HCM LOS | D |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NEL | NET SELn1 |  | SWT | SWR |
| Capacity (veh/h) |  | 1043 | - | 215 | - | - |
| HCM Lane V/C Ratio |  | 0.017 | - | 0.167 | - | - |
| HCM Control Delay (s) |  | 8.5 | 0 | 25.1 | - | - |
| HCM Lane LOS |  | A | A | D | - | - |
| HCM 95th \%tile Q(veh) |  | 0.1 | - | 0.6 | - | - |


| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 3 |  |  |  |  |  |  |
| Movement N | NWL | NWR | NET | NER | SWL | SWT |
| Lane Configurations | ${ }_{1}$ | 「 | 4 | F | ${ }^{*}$ | 4 |
| Traffic Vol, veh/h | 81 | 34 | 693 | 67 | 21 | 394 |
| Future Vol, veh/h | 81 | 34 | 693 | 67 | 21 | 394 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control S | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 175 | 0 | - | 250 | 150 | - |
| Veh in Median Storage, \# | \# 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 88 | 37 | 753 | 73 | 23 | 428 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.2 |  |  |  |  |  |
| Movement | SEL | SER | NEL | NET | SWT | SWR |
| Lane Configurations | Kr |  |  | $\uparrow$ | F |  |
| Traffic Vol, veh/h | 2 | 5 | 6 | 731 | 412 | 1 |
| Future Vol, veh/h | 2 | 5 | 6 | 731 | 412 | 1 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 2 | 5 | 7 | 795 | 448 | 1 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.8 |  |  |  |  |  |
| Movement | SEL | SER | NEL | NET | SWT | SWR |
| Lane Configurations | Mr |  |  | - | F |  |
| Traffic Vol, veh/h | 11 | 36 | 31 | 703 | 373 | 13 |
| Future Vol, veh/h | 11 | 36 | 31 | 703 | 373 | 13 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 12 | 39 | 34 | 764 | 405 | 14 |


| Major/Minor | Minor2 |  | Major1 |  | Major2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 1244 | 412 | 419 | 0 | - | 0 |
| Stage 1 | 412 | - | - | - | - | - |
| Stage 2 | 832 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | 4.12 | - | - | - |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | 2.218 | - | - | - |
| Pot Cap-1 Maneuver | 192 | 640 | 1140 | - | - | - |
| Stage 1 | 669 | - | - | - | - | - |
| Stage 2 | 427 | - | - | - | - | - |
| Platoon blocked, \% |  |  |  | - | - | - |
| Mov Cap-1 Maneuver | 182 | 640 | 1140 | - | - | - |
| Mov Cap-2 Maneuver | 182 | - | - | - | - | - |
| Stage 1 | 634 | - | - | - | - | - |
| Stage 2 | 427 | - | - | - | - | - |
|  |  |  |  |  |  |  |
| Approach | SE |  | NE |  | SW |  |
| HCM Control Delay, s | 15.2 |  | 0.3 |  | 0 |  |
| HCM LOS | C |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NEL | NET SELn1 |  | SWT | SWR |
| Capacity (veh/h) |  | 1140 | - | 403 | - | - |
| HCM Lane V/C Ratio |  | 0.03 | - | 0.127 | - | - |
| HCM Control Delay (s) |  | 8.3 | 0 | 15.2 | - | - |
| HCM Lane LOS |  | A | A | C | - | - |
| HCM 95th \%tile Q(veh) |  | 0.1 | - | 0.4 | - | - |




| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.1 |  |  |  |  |  |
| Movement | NBT | NBR | SBL | SBT | NWL | NWR |
| Lane Configurations | $\boldsymbol{F}$ |  |  | -1 | Mr |  |
| Traffic Vol, veh/h | 826 | 1 | 6 | 401 | 2 | 2 |
| Future Vol, veh/h | 826 | 1 | 6 | 401 | 2 | 2 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 898 | 1 | 7 | 436 | 2 | 2 |


| Major/Minor | Major1 |  | Major2 |  | Minor1 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 0 | 0 | 899 | 0 | 1349 | 899 |
| Stage 1 | - | - | - | - | 899 | - |
| Stage 2 | - | - | - | - | 450 | - |
| Critical Hdwy | - | - | 4.12 | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | - | - | 2.218 | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | - | - | 756 | - | 166 | 338 |
| Stage 1 | - | - | - | - | 397 | - |
| Stage 2 | - | - | - | - | 642 | - |
| Platoon blocked, \% | - | - |  | - |  |  |
| Mov Cap-1 Maneuver | - | - | 756 | - | 164 | 338 |
| Mov Cap-2 Maneuver | - | - | - | - | 164 | - |
| Stage 1 | - | - | - | - | 397 | - |
| Stage 2 | - | - | - | - | 634 | - |
|  |  |  |  |  |  |  |
| Approach | NB |  | SB |  | NW |  |
| HCM Control Delay, s | 0 |  | 0.1 |  | 21.6 |  |
| HCM LOS |  |  |  |  | C |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBT | NBRNWLn1 |  | SBL | SBT |
| Capacity (veh/h) |  | - | - | 221 | 756 | - |
| HCM Lane V/C Ratio |  | - | - | 0.02 | 0.009 | - |
| HCM Control Delay (s) |  | - | - | 21.6 | 9.8 | 0 |
| HCM Lane LOS |  | - | - | C | A | A |
| HCM 95th \%tile Q(veh) |  | - | - | 0.1 | 0 | - |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 1.8 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | NBL | NBT | NBR | SBL | SBT | SBR | SEL | SET | SER | NWL | NWT | NWR |  |
| Lane Configurations |  | ¢ |  |  | $\dagger$ |  |  | ¢ |  |  | ¢ |  |  |
| Traffic Vol, veh/h | 71 | 691 | 37 | 5 | 371 | 37 | 16 | 0 | 36 | 9 | 0 | 2 |  |
| Future Vol, veh/h | 71 | 691 | 37 | 5 | 371 | 37 | 16 | 0 | 36 | 9 | 0 | 2 |  |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Sign Control F | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |  |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |  |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - |  |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |  |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |  |
| Mvmt Flow | 77 | 751 | 40 | 5 | 403 | 40 | 17 | 0 | 39 | 10 | 0 | 2 |  |


| Major/Minor | Major1 | Major2 |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Conflicting Flow All | 443 | 0 | 0 | 791 | 0 | 0 | 1359 | 1378 | 423 | 1378 | 1378 |
| $\quad$ Stage 1 | - | - | - | - | - | - | 433 | 433 | - | 925 | 925 |

## Appendix D - Existing Turn Lane Warrant Evaluation Reports

Figure 2-5. Guideline for determining the need for a major-road left-turn bay at a two-way stop-controlled intersection.

## 2-lane roadway (English)

INPUT

| Variable | Value |
| :--- | :---: |
| $85^{\text {th }}$ percentile speed, $\mathrm{mph}:$ | 50 |
| Percent of left-turns in advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right), \%:$ | $3 \%$ |
| Advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 605 |
| Opposing volume $\left(\mathrm{V}_{\mathrm{O}}\right)$, veh $/ \mathrm{h}:$ | 981 |

OUTPUT

| Variable |  |  | Value |
| :--- | :---: | :---: | :---: |
| Limiting advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 313 |  |  |
| Guidance for determining the need for a major-road left-turn bay: |  |  |  |
| Left-turn treatment warranted. |  |  |  |



CALIBRATION CONSTANTS

| Variable | Value |
| :--- | :---: |
| Average time for making left-turn, s: | 3.0 |
| Critical headway, s: | 5.0 |
| Average time for left-turn vehicle to clear the advancing lane, s: | 1.9 |

Figure 2-6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-controlled intersection.

OUTPUT

| Variable | Value |
| :--- | :---: |
| Limiting right-turn volume, veh/h: | 11 |
| Guidance for determining the need for a major-road <br> right-turn bay for a 2-lane roadway: <br> Do NOT add right-turn bay. |  |$.$| Dr\| |
| :--- |



Figure 2-5. Guideline for determining the need for a major-road left-turn bay at a two-way stop-controlled intersection.

2-lane roadway (English)
INPUT

| Variable | Value |
| :--- | :---: |
| $85^{\text {th }}$ percentile speed, $\mathrm{mph}:$ | 50 |
| Percent of left-turns in advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right), \%:$ | $9 \%$ |
| Advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 990 |
| Opposing volume $\left(\mathrm{V}_{\mathrm{O}}\right)$, veh $/ \mathrm{h}:$ | 606 |

## OUTPUT

| Variable | Value |
| :--- | :---: |
| Limiting advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 276 |
| Guidance for determining the need for a major-road left-turn bay: |  |
| Left-turn treatment warranted. |  |



CALIBRATION CONSTANTS

| Variable | Value |
| :--- | :---: |
| Average time for making left-turn, s: | 3.0 |
| Critical headway, s: | 5.0 |
| Average time for left-turn vehicle to clear the advancing lane, s: | 1.9 |

Figure 2-6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-controlled intersection.

OUTPUT

| Variable | Value |
| :--- | :---: |
| Limiting right-turn volume, veh/h: | 19 |
| Guidance for determining the need for a major-road <br> right-turn bay for a 2-lane roadway: <br> Do NOT add right-turn bay. |  |$.$| Dr\| |
| :--- |



Figure 2-6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-controlled intersection.
INPUT

| Roadway geometry: | Variable | 2-lane roadway |
| :--- | :---: | :---: |
| Value |  |  |
| Major-road speed, mph: | 55 |  |
| Major-road volume (one direction), veh/h: | 325 |  |
| Right-turn volume, veh/h: | 0 |  |

OUTPUT

| Variable | Value |
| :--- | :---: |
| Limiting right-turn volume, veh/h: | 22 |
| Guidance for determining the need for a major-road <br> right-turn bay for a 2-lane roadway: |  |
| Do NOT add right-turn bay. |  |



Figure 2-5. Guideline for determining the need for a major-road left-turn bay at a two-way stop-controlled intersection.

## 2-lane roadway (English)

INPUT

| Variable | Value |
| :--- | :---: |
| $85^{\text {th }}$ percentile speed, $\mathrm{mph}:$ | 55 |
| Percent of left-turns in advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right), \%:$ | $1 \%$ |
| Advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh $/ \mathrm{h}:$ | 917 |
| Opposing volume $\left(\mathrm{V}_{\mathrm{O}}\right), \mathrm{veh} / \mathrm{h}:$ | 325 |

OUTPUT

| Variable | Value |  |
| :--- | :---: | :---: |
| Limiting advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 950 |  |
| Guidance for determining the need for a major-road left-turn bay: |  |  |
| Left-turn treatment NOT warranted. |  |  |



CALIBRATION CONSTANTS

| Variable | Value |
| :--- | :---: |
| Average time for making left-turn, s: | 3.0 |
| Critical headway, s: | 5.0 |
| Average time for left-turn vehicle to clear the advancing lane, s: | 1.9 |

Figure 2-6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-controlled intersection.
INPUT

| Roadway geometry: | Variable | 2-lane roadway $\quad-$ |
| :--- | :---: | :---: |
| Major-road speed, mph: | 55 |  |
| Major-road volume (one direction), veh/h: | 827 |  |
| Right-turn volume, veh/h: | 1 |  |

OUTPUT

| Variable | Value |
| :--- | :---: |
| Limiting right-turn volume, veh/h: | 11 |
| Guidance for determining the need for a major-road <br> right-turn bay for a 2-lane roadway: |  |
| Do NOT add right-turn bay. |  |



Figure 2-5. Guideline for determining the need for a major-road left-turn bay at a two-way stop-controlled intersection.

## 2-lane roadway (English)

INPUT

| Variable | Value |
| :--- | :---: |
| $85^{\text {th }}$ percentile speed, $\mathrm{mph}:$ | 55 |
| Percent of left-turns in advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right), \%:$ | $1 \%$ |
| Advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 407 |
| Opposing volume $\left(\mathrm{V}_{\mathrm{O}}\right)$, veh $/ \mathrm{h}:$ | 827 |

OUTPUT

| Variable |  |  |
| :--- | :---: | :---: |
| Limiting advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 569 |  |
| Guidance for determining the need for a major-road left-turn bay: |  |  |
| Left-turn treatment NOT warranted. |  |  |



CALIBRATION CONSTANTS

| Variable | Value |
| :--- | :---: |
| Average time for making left-turn, s: | 3.0 |
| Critical headway, s: | 5.0 |
| Average time for left-turn vehicle to clear the advancing lane, s: | 1.9 |

Figure 2-5. Guideline for determining the need for a major-road left-turn bay at a two-way stop-controlled intersection.

## 2-lane roadway (English)

INPUT

| Variable | Value |
| :--- | :---: |
| $85^{\text {th }}$ percentile speed, $\mathrm{mph}:$ | 50 |
| Percent of left-turns in advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right), \%:$ | $1 \%$ |
| Advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 587 |
| Opposing volume $\left(\mathrm{V}_{\mathrm{O}}\right)$, veh $/ \mathrm{h}:$ | 889 |

OUTPUT

| Variable |  |  | Value |
| :--- | :---: | :---: | :---: |
| Limiting advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 587 |  |  |
| Guidance for determining the need for a major-road left-turn bay: |  |  |  |
| Left-turn treatment warranted. |  |  |  |



CALIBRATION CONSTANTS

| Variable | Value |
| :--- | :---: |
| Average time for making left-turn, s: | 3.0 |
| Critical headway, s: | 5.0 |
| Average time for left-turn vehicle to clear the advancing lane, s: | 1.9 |

Figure 2-6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-controlled intersection.

OUTPUT

| Variable | Value |
| :--- | :---: |
| Limiting right-turn volume, veh/h: | 12 |
| Guidance for determining the need for a major-road <br> right-turn bay for a 2-lane roadway: |  |
| Add right-turn bay. |  |



Figure 2-5. Guideline for determining the need for a major-road left-turn bay at a two-way stop-controlled intersection.

## 2-lane roadway (English)

INPUT

| Variable | Value |
| :--- | :---: |
| $85^{\text {th }}$ percentile speed, $\mathrm{mph}:$ | 50 |
| Percent of left-turns in advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right), \%:$ | $2 \%$ |
| Advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 763 |
| Opposing volume $\left(\mathrm{V}_{\mathrm{O}}\right)$, veh $/ \mathrm{h}:$ | 481 |

OUTPUT

| Variable |  |  | Value |
| :--- | :---: | :---: | :---: |
| Limiting advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 627 |  |  |
| Guidance for determining the need for a major-road left-turn bay: |  |  |  |
| Left-turn treatment warranted. |  |  |  |



CALIBRATION CONSTANTS

| Variable | Value |
| :--- | :---: |
| Average time for making left-turn, s: | 3.0 |
| Critical headway, s: | 5.0 |
| Average time for left-turn vehicle to clear the advancing lane, s: | 1.9 |

Figure 2-6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-controlled intersection.

| Roadway geometry: | 2-lane roadway |  |
| :--- | :--- | :---: |
| Major-road speed, mph: | Variable | 50 |
| Major-road volume (one direction), veh/h: | 481 |  |
| Right-turn volume, veh/h: | 18 |  |

OUTPUT

| Variable | Value |
| :--- | :---: |
| Limiting right-turn volume, veh/h: | 26 |
| Guidance for determining the need for a major-road <br> right-turn bay for a 2-lane roadway: |  |
| Do NOT add right-turn bay. |  |



## AM Existing

Figure 2-5. Guideline for determining the need for a major-road left-turn bay at a two-way stop-controlled intersection.

2-lane roadway (English)
INPUT

| Variable | Value |
| :--- | :---: |
| $85^{\text {th }}$ percentile speed, $\mathrm{mph}:$ | 50 |
| Percent of left-turns in advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right), \%:$ | $4 \%$ |
| Advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 417 |
| Opposing volume $\left(\mathrm{V}_{\mathrm{O}}\right)$, veh $/ \mathrm{h}:$ | 723 |

## OUTPUT

| Variable | Value |  |
| :--- | :---: | :---: |
| Limiting advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 374 |  |
| Guidance for determining the need for a major-road left-turn bay: |  |  |
| Left-turn treatment warranted. |  |  |



CALIBRATION CONSTANTS

| Variable | Value |
| :--- | :---: |
| Average time for making left-turn, s: | 3.0 |
| Critical headway, s: | 5.0 |
| Average time for left-turn vehicle to clear the advancing lane, s: | 1.9 |

Figure 2-6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-controlled intersection.

OUTPUT

| Variable | Value |
| :--- | :---: |
| Limiting right-turn volume, veh/h: | 16 |
| Guidance for determining the need for a major-road <br> right-turn bay for a 2-lane roadway: |  |
| Do NOT add right-turn bay. |  |


PM Existing

Figure 2-5. Guideline for determining the need for a major-road left-turn bay at a two-way stop-controlled intersection.

2-lane roadway (English)
INPUT

| Variable | Value |
| :--- | :---: |
| $85^{\text {th }}$ percentile speed, $\mathrm{mph}:$ | 50 |
| Percent of left-turns in advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right), \%:$ | $4 \%$ |
| Advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 734 |
| Opposing volume $\left(\mathrm{V}_{\mathrm{O}}\right)$, veh $/ \mathrm{h}:$ | 386 |

## OUTPUT

| Variable | Value |  |
| :--- | :---: | :---: |
| Limiting advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 528 |  |
| Guidance for determining the need for a major-road left-turn bay: |  |  |
| Left-turn treatment warranted. |  |  |



CALIBRATION CONSTANTS

| Variable | Value |
| :--- | :---: |
| Average time for making left-turn, s: | 3.0 |
| Critical headway, s: | 5.0 |
| Average time for left-turn vehicle to clear the advancing lane, s: | 1.9 |

Figure 2-6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-controlled intersection.

OUTPUT

| Variable | Value |
| :--- | :---: |
| Limiting right-turn volume, veh/h: | 33 |
| Guidance for determining the need for a major-road <br> right-turn bay for a 2-lane roadway: |  |
| Do NOT add right-turn bay. |  |



Figure 2-5. Guideline for determining the need for a major-road left-turn bay at a two-way stop-controlled intersection.

## 2-lane roadway (English)

INPUT

| Variable | Value |
| :--- | :---: |
| $85^{\text {th }}$ percentile speed, $\mathrm{mph}:$ | 55 |
| Percent of left-turns in advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right), \%:$ | $1 \%$ |
| Advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh $/ \mathrm{h}:$ | 335 |
| Opposing volume $\left(\mathrm{V}_{\mathrm{O}}\right)$, veh $/ \mathrm{h}:$ | 924 |

OUTPUT

| Variable |  |  |
| :--- | :---: | :---: |
| Limiting advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 518 |  |
| Guidance for determining the need for a major-road left-turn bay: |  |  |
| Left-turn treatment NOT warranted. |  |  |



CALIBRATION CONSTANTS

| Variable | Value |
| :--- | :---: |
| Average time for making left-turn, s: | 3.0 |
| Critical headway, s: | 5.0 |
| Average time for left-turn vehicle to clear the advancing lane, s: | 1.9 |

Figure 2-6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-controlled intersection.
INPUT

| Roadway geometry: | 2-lane roadway |
| :--- | :--- | :---: |
| Variable | Value |
| Major-road speed, mph: | 55 |
| Major-road volume (one direction), veh/h: | 335 |
| Right-turn volume, veh/h: | 10 |

OUTPUT

| Variable | Value |
| :--- | :---: |
| Limiting right-turn volume, veh/h: | 22 |
| Guidance for determining the need for a major-road <br> right-turn bay for a 2-lane roadway: |  |
| Do NOT add right-turn bay. |  |

Figure 2-5. Guideline for determining the need for a major-road left-turn bay at a two-way stop-controlled intersection.

## 2-lane roadway (English)

INPUT

| Variable | Value |
| :--- | :---: |
| $85^{\text {th }}$ percentile speed, $\mathrm{mph}:$ | 55 |
| Percent of left-turns in advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right), \%:$ | $1 \%$ |
| Advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 927 |
| Opposing volume $\left(\mathrm{V}_{\mathrm{O}}\right)$, veh $/ \mathrm{h}:$ | 331 |

OUTPUT

| Variable |  |  | Value |
| :--- | :---: | :---: | :---: |
| Limiting advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 944 |  |  |
| Guidance for determining the need for a major-road left-turn bay: |  |  |  |
| Left-turn treatment NOT warranted. |  |  |  |



CALIBRATION CONSTANTS

| Variable | Value |
| :--- | :---: |
| Average time for making left-turn, s: | 3.0 |
| Critical headway, s: | 5.0 |
| Average time for left-turn vehicle to clear the advancing lane, s: | 1.9 |

Figure 2-6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-controlled intersection.
INPUT

| Roadway geometry: | Variable | 2-lane roadway |
| :--- | :---: | :---: |
| Value |  |  |
| Major-road speed, mph: | 55 |  |
| Major-road volume (one direction), veh/h: | 927 |  |
| Right-turn volume, veh/h: | 4 |  |

OUTPUT

| Variable | Value |
| :--- | :---: |
| Limiting right-turn volume, veh/h: | 10 |
| Guidance for determining the need for a major-road <br> right-turn bay for a 2-lane roadway: |  |
| Do NOT add right-turn bay. |  |



Figure 2-5. Guideline for determining the need for a major-road left-turn bay at a two-way stop-controlled intersection.

## 2-lane roadway (English)

INPUT

| Variable | Value |
| :--- | :---: |
| $85^{\text {th }}$ percentile speed, $\mathrm{mph}:$ | 55 |
| Percent of left-turns in advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right), \%:$ | $1 \%$ |
| Advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh $/ \mathrm{h}:$ | 856 |
| Opposing volume $\left(\mathrm{V}_{\mathrm{O}}\right)$, veh $/ \mathrm{h}:$ | 399 |

OUTPUT

| Variable |  |  |
| :--- | :---: | :---: |
| Limiting advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 878 |  |
| Guidance for determining the need for a major-road left-turn bay: |  |  |
| Left-turn treatment NOT warranted. |  |  |



CALIBRATION CONSTANTS

| Variable | Value |
| :--- | :---: |
| Average time for making left-turn, s: | 3.0 |
| Critical headway, s: | 5.0 |
| Average time for left-turn vehicle to clear the advancing lane, s: | 1.9 |

Figure 2-6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-controlled intersection.
INPUT

| Roadway geometry: | Variable | 2-lane roadway |
| :--- | :---: | :---: |
| Value |  |  |
| Major-road speed, mph: | 55 |  |
| Major-road volume (one direction), veh/h: | 856 |  |
| Right-turn volume, veh/h: | 27 |  |

OUTPUT

| Variable | Value |
| :--- | :---: |
| Limiting right-turn volume, veh/h: | 10 |
| Guidance for determining the need for a major-road <br> right-turn bay for a 2-lane roadway: |  |
| Add right-turn bay. |  |



Figure 2-5. Guideline for determining the need for a major-road left-turn bay at a two-way stop-controlled intersection.

## 2-lane roadway (English)

INPUT

| Variable | Value |
| :--- | :---: |
| $85^{\text {th }}$ percentile speed, $\mathrm{mph}:$ | 55 |
| Percent of left-turns in advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right), \%:$ | $1 \%$ |
| Advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 403 |
| Opposing volume $\left(\mathrm{V}_{\mathrm{O}}\right)$, veh $/ \mathrm{h}:$ | 844 |

OUTPUT

| Variable |  |  |
| :--- | :---: | :---: |
| Limiting advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 559 |  |
| Guidance for determining the need for a major-road left-turn bay: |  |  |
| Left-turn treatment NOT warranted. |  |  |



CALIBRATION CONSTANTS

| Variable | Value |
| :--- | :---: |
| Average time for making left-turn, s: | 3.0 |
| Critical headway, s: | 5.0 |
| Average time for left-turn vehicle to clear the advancing lane, s: | 1.9 |

Figure 2-6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-controlled intersection.
INPUT

| Roadway geometry: | Variable | 2-lane roadway |
| :--- | :---: | :---: |
| Value |  |  |
| Major-road speed, mph: | 55 |  |
| Major-road volume (one direction), veh/h: | 403 |  |
| Right-turn volume, veh/h: | 3 |  |

OUTPUT

| Variable | Value |
| :--- | :---: |
| Limiting right-turn volume, veh/h: | 19 |
| Guidance for determining the need for a major-road <br> right-turn bay for a 2-lane roadway: |  |
| Do NOT add right-turn bay. |  |



Figure 2-5. Guideline for determining the need for a major-road left-turn bay at a two-way stop-controlled intersection.

## 2-lane roadway (English)

INPUT

| Variable | Value |
| :--- | :---: |
| $85^{\text {th }}$ percentile speed, $\mathrm{mph}:$ | 50 |
| Percent of left-turns in advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right), \%:$ | $2 \%$ |
| Advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 592 |
| Opposing volume $\left(\mathrm{V}_{\mathrm{O}}\right)$, veh $/ \mathrm{h}:$ | 854 |

OUTPUT

| Variable |  |  |  | Value |
| :--- | :---: | :---: | :---: | :---: |
| Limiting advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 431 |  |  |  |
| Guidance for determining the need for a major-road left-turn bay: |  |  |  |  |
| Left-turn treatment warranted. |  |  |  |  |



CALIBRATION CONSTANTS

| Variable | Value |
| :--- | :---: |
| Average time for making left-turn, s: | 3.0 |
| Critical headway, s: | 5.0 |
| Average time for left-turn vehicle to clear the advancing lane, s: | 1.9 |

Figure 2-6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-controlled intersection.

OUTPUT

| Variable | Value |
| :--- | :---: |
| Limiting right-turn volume, veh/h: | 13 |
| Guidance for determining the need for a major-road <br> right-turn bay for a 2-lane roadway: |  |
| Do NOT add right-turn bay. |  |



Figure 2-5. Guideline for determining the need for a major-road left-turn bay at a two-way stop-controlled intersection.

## 2-lane roadway (English)

INPUT

| Variable | Value |
| :--- | :---: |
| $85^{\text {th }}$ percentile speed, $\mathrm{mph}:$ | 50 |
| Percent of left-turns in advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right), \%:$ | $8 \%$ |
| Advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 836 |
| Opposing volume $\left(\mathrm{V}_{\mathrm{O}}\right)$, veh $/ \mathrm{h}:$ | 494 |

OUTPUT

| Variable |  |  |  | Value |
| :--- | :---: | :---: | :---: | :---: |
| Limiting advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 319 |  |  |  |
| Guidance for determining the need for a major-road left-turn bay: |  |  |  |  |
| Left-turn treatment warranted. |  |  |  |  |



CALIBRATION CONSTANTS

| Variable | Value |
| :--- | :---: |
| Average time for making left-turn, s: | 3.0 |
| Critical headway, s: | 5.0 |
| Average time for left-turn vehicle to clear the advancing lane, s: | 1.9 |

Figure 2-6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-controlled intersection.

OUTPUT

| Variable | Value |
| :--- | :---: |
| Limiting right-turn volume, veh/h: | 25 |
| Guidance for determining the need for a major-road <br> right-turn bay for a 2-lane roadway: <br> Do NOT add right-turn bay. |  |$.$| Dr\| |
| :--- |



Figure 2-5. Guideline for determining the need for a major-road left-turn bay at a two-way stop-controlled intersection.

## 2-lane roadway (English)

INPUT

| Variable | Value |
| :--- | :---: |
| $85^{\text {th }}$ percentile speed, $\mathrm{mph}:$ | 55 |
| Percent of left-turns in advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right), \%:$ | $4 \%$ |
| Advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 333 |
| Opposing volume $\left(\mathrm{V}_{\mathrm{O}}\right)$, veh $/ \mathrm{h}:$ | 829 |

OUTPUT

| Variable | Value |  |
| :--- | :---: | :---: |
| Limiting advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 288 |  |
| Guidance for determining the need for a major-road left-turn bay: |  |  |
| Left-turn treatment warranted. |  |  |



CALIBRATION CONSTANTS

| Variable | Value |
| :--- | :---: |
| Average time for making left-turn, s: | 3.0 |
| Critical headway, s: | 5.0 |
| Average time for left-turn vehicle to clear the advancing lane, s: | 1.9 |

Figure 2-6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-controlled intersection.
INPUT

| Roadway geometry: | 2-lane roadway |
| :--- | :---: |
| Variable |  |
| Major-road speed, mph: | Value |
| Major-road volume (one direction), veh/h: | 55 |
| Right-turn volume, veh/h: | 333 |

OUTPUT

| Variable | Value |
| :--- | :---: |
| Limiting right-turn volume, veh/h: | 22 |
| Guidance for determining the need for a major-road <br> right-turn bay for a 2-lane roadway: |  |
| Do NOT add right-turn bay. |  |



Figure 2-5. Guideline for determining the need for a major-road left-turn bay at a two-way stop-controlled intersection.

## 2-lane roadway (English)

INPUT

| Variable | Value |
| :--- | :---: |
| $85^{\text {th }}$ percentile speed, $\mathrm{mph}:$ | 55 |
| Percent of left-turns in advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right), \%:$ | $1 \%$ |
| Advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh $/ \mathrm{h}:$ | 831 |
| Opposing volume $\left(\mathrm{V}_{\mathrm{O}}\right)$, veh $/ \mathrm{h}:$ | 319 |

OUTPUT

| Variable |  |
| :--- | :---: |
| Limiting advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | Value |
| Guidance for determining the need for a major-road left-turn bay: |  |
| Left-turn treatment NOT warranted. |  |



CALIBRATION CONSTANTS

| Variable | Value |
| :--- | :---: |
| Average time for making left-turn, s: | 3.0 |
| Critical headway, s: | 5.0 |
| Average time for left-turn vehicle to clear the advancing lane, s: | 1.9 |

Figure 2-6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-controlled intersection.
INPUT

| Roadway geometry: | 2-lane roadway |
| :--- | :--- | :---: |
| Variable | Value |
| Major-road speed, mph: | 55 |
| Major-road volume (one direction), veh/h: | 831 |
| Right-turn volume, veh/h: | 9 |

OUTPUT

| Variable | Value |
| :--- | :---: |
| Limiting right-turn volume, veh/h: | 11 |
| Guidance for determining the need for a major-road <br> right-turn bay for a 2-lane roadway: |  |
| Do NOT add right-turn bay. |  |



Figure 2-5. Guideline for determining the need for a major-road left-turn bay at a two-way stop-controlled intersection.

## 2-lane roadway (English)

INPUT

| Variable | Value |
| :--- | :---: |
| $85^{\text {th }}$ percentile speed, $\mathrm{mph}:$ | 55 |
| Percent of left-turns in advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right), \%:$ | $8 \%$ |
| Advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 799 |
| Opposing volume $\left(\mathrm{V}_{\mathrm{O}}\right)$, veh $/ \mathrm{h}:$ | 408 |

OUTPUT

| Variable | Value |  |
| :--- | :---: | :---: |
| Limiting advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 319 |  |
| Guidance for determining the need for a major-road left-turn bay: |  |  |
| Left-turn treatment warranted. |  |  |



CALIBRATION CONSTANTS

| Variable | Value |
| :--- | :---: |
| Average time for making left-turn, s: | 3.0 |
| Critical headway, s: | 5.0 |
| Average time for left-turn vehicle to clear the advancing lane, s: | 1.9 |

Figure 2-6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-controlled intersection.
INPUT

| Roadway geometry: | 2-lane roadway |  |
| :--- | :--- | :---: |
| Variable |  | Value |
| Major-road speed, mph: | 55 |  |
| Major-road volume (one direction), veh/h: | 799 |  |
| Right-turn volume, veh/h: | 37 |  |

OUTPUT

| Variable | Value |
| :--- | :---: |
| Limiting right-turn volume, veh/h: | 11 |
| Guidance for determining the need for a major-road <br> right-turn bay for a 2-lane roadway: |  |
| Add right-turn bay. |  |



Figure 2-5. Guideline for determining the need for a major-road left-turn bay at a two-way stop-controlled intersection.

## 2-lane roadway (English)

INPUT

| Variable | Value |
| :--- | :---: |
| $85^{\text {th }}$ percentile speed, $\mathrm{mph}:$ | 55 |
| Percent of left-turns in advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right), \%:$ | $1 \%$ |
| Advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 413 |
| Opposing volume $\left(\mathrm{V}_{\mathrm{O}}\right)$, veh $/ \mathrm{h}:$ | 728 |

OUTPUT

| Variable | Value |  |
| :--- | :---: | :---: |
| Limiting advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 627 |  |
| Guidance for determining the need for a major-road left-turn bay: |  |  |
| Left-turn treatment NOT warranted. |  |  |



CALIBRATION CONSTANTS

| Variable | Value |
| :--- | :---: |
| Average time for making left-turn, s: | 3.0 |
| Critical headway, s: | 5.0 |
| Average time for left-turn vehicle to clear the advancing lane, s: | 1.9 |

Figure 2-6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-controlled intersection.
INPUT

| Roadway geometry: | Variable | 2-lane roadway |
| :--- | :---: | :---: |
| Value |  |  |
| Major-road speed, mph: | 55 |  |
| Major-road volume (one direction), veh/h: | 413 |  |
| Right-turn volume, veh/h: | 37 |  |

OUTPUT

| Variable | Value |
| :--- | :---: |
| Limiting right-turn volume, veh/h: | 18 |
| Guidance for determining the need for a major-road <br> right-turn bay for a 2-lane roadway: |  |
| Add right-turn bay. |  |



Figure 2-5. Guideline for determining the need for a major-road left-turn bay at a two-way stop-controlled intersection.

## 2-lane roadway (English)

INPUT

| Variable | Value |
| :--- | :---: |
| $85^{\text {th }}$ percentile speed, $\mathrm{mph}:$ | 50 |
| Percent of left-turns in advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right), \%:$ | $1 \%$ |
| Advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh $/ \mathrm{h:}$ | 413 |
| Opposing volume $\left(\mathrm{V}_{\mathrm{O}}\right)$, veh/h: | 781 |

OUTPUT

| Variable | Value |
| :--- | :---: |
| Limiting advancing volume $\left(V_{\mathrm{A}}\right)$, veh/h: | 652 |
| Guidance for determining the need for a major-road left-turn bay: |  |
| Left-turn treatment NOT warranted. |  |



CALIBRATION CONSTANTS

| Variable | Value |
| :--- | :---: |
| Average time for making left-turn, s: | 3.0 |
| Critical headway, $\mathrm{s}:$ | 5.0 |
| Average time for left-turn vehicle to clear the advancing lane, $\mathrm{s}:$ | 1.9 |

Figure 2-6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-controlled intersection.
INPUT

| Roadway geometry: | Variable | 2-lane roadway |
| :--- | :--- | :---: |
| Major-road speed, mph: | 50 |  |
| Major-road volume (one direction), veh/h: | 781 |  |
| Right-turn volume, veh/h: | 0 |  |

OUTPUT

| Variable | Value |
| :--- | :---: |
| Limiting right-turn volume, veh/h: | 14 |
| Guidance for determining the need for a major-road <br> right-turn bay for a 2-lane roadway: |  |
| Do NOT add right-turn bay. |  |



Figure 2-5. Guideline for determining the need for a major-road left-turn bay at a two-way stop-controlled intersection.

## 2-lane roadway (English)

INPUT

| Variable | Value |
| :--- | :---: |
| $85^{\text {th }}$ percentile speed, $\mathrm{mph}:$ | 50 |
| Percent of left-turns in advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right), \%:$ | $1 \%$ |
| Advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 737 |
| Opposing volume $\left(\mathrm{V}_{\mathrm{O}}\right)$, veh $/ \mathrm{h}:$ | 413 |

OUTPUT

| Variable |  |  | Value |
| :--- | :---: | :---: | :---: |
| Limiting advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 947 |  |  |
| Guidance for determining the need for a major-road left-turn bay: |  |  |  |
| Left-turn treatment NOT warranted. |  |  |  |



CALIBRATION CONSTANTS

| Variable | Value |
| :--- | :---: |
| Average time for making left-turn, s: | 3.0 |
| Critical headway, s: | 5.0 |
| Average time for left-turn vehicle to clear the advancing lane, s: | 1.9 |

Figure 2-6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-controlled intersection.
INPUT

| Roadway geometry: | 2-lane roadway |
| :--- | :--- | :---: |
| Major-road speed, mph: | Value |
| Major-road volume (one direction), veh/h: | 50 |
| Right-turn volume, veh/h: | 413 |

OUTPUT

| Variable | Value |
| :--- | :---: |
| Limiting right-turn volume, veh/h: | 31 |
| Guidance for determining the need for a major-road <br> right-turn bay for a 2-lane roadway: |  |
| Do NOT add right-turn bay. |  |


AM Existing

Figure 2-5. Guideline for determining the need for a major-road left-turn bay at a two-way stop-controlled intersection.

## 2-lane roadway (English)

INPUT

| Variable | Value |
| :--- | :---: |
| $85^{\text {th }}$ percentile speed, $\mathrm{mph}:$ | 50 |
| Percent of left-turns in advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right), \%:$ | $1 \%$ |
| Advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 595 |
| Opposing volume $\left(\mathrm{V}_{\mathrm{O}}\right)$, veh $/ \mathrm{h}:$ | 886 |

OUTPUT

| Variable |  |  |  | Value |
| :--- | :---: | :---: | :---: | :---: |
| Limiting advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 588 |  |  |  |
| Guidance for determining the need for a major-road left-turn bay: |  |  |  |  |
| Left-turn treatment warranted. |  |  |  |  |



CALIBRATION CONSTANTS

| Variable | Value |
| :--- | :---: |
| Average time for making left-turn, s: | 3.0 |
| Critical headway, s: | 5.0 |
| Average time for left-turn vehicle to clear the advancing lane, s: | 1.9 |

Figure 2-6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-controlled intersection.

OUTPUT

| Variable | Value |
| :--- | :---: |
| Limiting right-turn volume, veh/h: | 20 |
| Guidance for determining the need for a major-road <br> right-turn bay for a 2-lane roadway: |  |
| Add right-turn bay. |  |



Figure 2-5. Guideline for determining the need for a major-road left-turn bay at a two-way stop-controlled intersection.

2-lane roadway (English)
INPUT

| Variable | Value |
| :--- | :---: |
| $85^{\text {th }}$ percentile speed, $\mathrm{mph}:$ | 50 |
| Percent of left-turns in advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right), \%:$ | $2 \%$ |
| Advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 903 |
| Opposing volume $\left(\mathrm{V}_{\mathrm{O}}\right)$, veh $/ \mathrm{h}:$ | 590 |

## OUTPUT

| Variable | Value |
| :--- | :---: |
| Limiting advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 561 |
| Guidance for determining the need for a major-road left-turn bay: |  |
| Left-turn treatment warranted. |  |



CALIBRATION CONSTANTS

| Variable | Value |
| :--- | :---: |
| Average time for making left-turn, s: | 3.0 |
| Critical headway, s: | 5.0 |
| Average time for left-turn vehicle to clear the advancing lane, s: | 1.9 |

Figure 2-6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-controlled intersection.

OUTPUT

| Variable | Value |
| :--- | :---: |
| Limiting right-turn volume, veh/h: | 12 |
| Guidance for determining the need for a major-road <br> right-turn bay for a 2-lane roadway: <br> Do NOT add right-turn bay. |  |$.$| Dr\| |
| :--- |



Figure 2-5. Guideline for determining the need for a major-road left-turn bay at a two-way stop-controlled intersection.

## 2-lane roadway (English)

| Variable | Value |
| :--- | :---: |
| P5 ${ }^{\text {th }}$ percentile speed, mph: | 50 |
| Percent of left-turns in advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right), \%:$ | $2 \%$ |
| Advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 913 |
| Opposing volume $\left(\mathrm{V}_{\mathrm{O}}\right)$, veh $/ \mathrm{h}:$ | 545 |

OUTPUT

| Variable | Value |  |
| :--- | :---: | :---: |
| Limiting advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 587 |  |
| Guidance for determining the need for a major-road left-turn bay: |  |  |
| Left-turn treatment warranted. |  |  |



CALIBRATION CONSTANTS

| Variable | Value |
| :--- | :---: |
| Average time for making left-turn, s: | 3.0 |
| Critical headway, s: | 5.0 |
| Average time for left-turn vehicle to clear the advancing lane, s: | 1.9 |

Figure 2-6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-controlled intersection.

OUTPUT

| Variable | Value |
| :--- | :---: |
| Limiting right-turn volume, veh/h: | 12 |
| Guidance for determining the need for a major-road <br> right-turn bay for a 2-lane roadway: |  |
| Add right-turn bay. |  |



Figure 2-5. Guideline for determining the need for a major-road left-turn bay at a two-way stop-controlled intersection.

## 2-lane roadway (English)

INPUT

| Variable | Value |
| :--- | :---: |
| $85^{\text {th }}$ percentile speed, $\mathrm{mph}:$ | 50 |
| Percent of left-turns in advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right), \%:$ | $2 \%$ |
| Advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 558 |
| Opposing volume $\left(\mathrm{V}_{\mathrm{O}}\right)$, veh $/ \mathrm{h}:$ | 892 |

OUTPUT

| Variable |  |  | Value |
| :--- | :---: | :---: | :---: |
| Limiting advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 416 |  |  |
| Guidance for determining the need for a major-road left-turn bay: |  |  |  |
| Left-turn treatment warranted. |  |  |  |



CALIBRATION CONSTANTS

| Variable | Value |
| :--- | :---: |
| Average time for making left-turn, s: | 3.0 |
| Critical headway, s: | 5.0 |
| Average time for left-turn vehicle to clear the advancing lane, s: | 1.9 |

Figure 2-6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-controlled intersection.

OUTPUT

| Variable | Value |
| :--- | :---: |
| Limiting right-turn volume, veh/h: | 21 |
| Guidance for determining the need for a major-road <br> right-turn bay for a 2-lane roadway: <br> Do NOT add right-turn bay. |  |$.$| Dr\| |
| :--- |



## Appendix E - Signal Warrant Evaluation Reports

## TRAFFIC SIGNAL WARRANTS

| City／Town： | Moody |
| ---: | :---: |
| County： | St．Clair |
| Division： | ALDOT East Central |
| Data Date： | Pro |
| Major Route： | US－411 |
| Minor Route： | Washington Drive／Verbena Drive |

Analysis Performed By：

| DEC |
| :---: |
| $6 / 1 / 2022$ |
| 220104 |
| Overcast |


| Appr．Lanes： |  |
| :--- | :--- |
| Appr．Lanes： | $\frac{1}{1} \quad$ Critical Approach Speed（mph）：$\quad 50$ |

## Volume Level Criteria

1．Is the critical speed of major street traffic $>70 \mathrm{~km} / \mathrm{h}(40 \mathrm{mph})$ ？
2．Is the intersection in a built－up area or isolated community of＜10，000 population？

| $\mathbf{X}$ <br> Yes | $\square$ No |
| :--- | :--- |
| $\square$ Yes | $\square$ No |
| $\square \mathbf{X} 70 \%$ | $\square 100 \%$ |

## WARRANT 1 －EIGHT－HOUR VEHICULAR VOLUME

Warrant 1 is satisfied if Condition A or Condition B is＂100\％＂satisfied．
Satisfied：$\quad \square$ Yes $\quad \mathbf{X}$ No
Warrant is also satisfied if both Condition A and Condition B are＂ $80 \%$＂satisfied，given
adequate trials of other remedial measures have been tried．
Adequate trial（s）of other remedial measures tried：
List Remedial Measures Tried（Required for $80 \%$ Combination of A \＆B）
$\square$
Condition A－Minimum Vehicular Volume \＆Condition B－Interruption of Continuous Traffic 100\％Satisfied：$\quad \square$ Yes $\quad \bar{X}$ No （Used if neither Condition A or B is satisfied）80\％Satisfied：$\quad \square$ Yes $\quad \mathrm{X}$ No

|  | $\begin{gathered} \text { (volumes in veh/hr) } \\ \hline \text { Approach Lanes } \\ \text { Volume Level } \end{gathered}$ | Minimum Requirements |  |  |  | Eight Highest Hours |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | $6^{5}$ | $\hat{v}^{5}$ | $8_{8}^{5}$ | $n^{2}$ | $\mathfrak{s}^{5}$ | ＊ | が | 6 |
|  |  | 1 |  | 2 or more |  |  |  |  |  |  |  |  |  |
|  |  | 100\％ | 70\％ | 100\％ | 70\％ |  |  |  |  |  |  |  |  |
| $\left\lvert\, \begin{array}{ll} \boxed{1} & 0 \\ 1 & 0 \\ 1 & 0 \end{array}\right.$ | Both Approaches on Major Street | 500 | 350 | 600 | 420 | 950 | 1，498 | 1，017 | 1，073 | 1，394 | 1，342 | 1，471 | 1，102 |
|  | Highest Approach on Minor Street | 150 | 105 | 200 | 140 | 64 | 110 | 50 | 45 | 48 | 48 | 56 | 46 |
|  | （volumes in veh／hr） | Minimum Requirements |  |  |  | $6$ | $\hat{p}^{5}$ | $8_{8}^{5}$ | $n^{*}$ | ${ }_{3}^{5}$ | s | s | 8 |
|  | Approach Lanes | 1 |  | 2 or more |  |  |  |  |  |  |  |  |  |
|  | Volume Level | 100\％ | 70\％ | 100\％ | 70\％ |  |  |  |  |  |  |  |  |
| $\left\lvert\, \begin{array}{ll} n & \circ \\ 1 & 0 \\ s & 0 \end{array}\right.$ | Both Approaches on Major Street | 750 | 525 | 900 | 630 | 950 | 1，498 | 1，017 | 1，073 | 1，394 | 1，342 | 1，471 | 1，102 |
|  | Highest Approach on Minor Street | 75 | 53 | 100 | 70 | 64 | 110 | 50 | 45 | 48 | 48 | 56 | 46 |
|  | （volumes in veh／hr） | Minimum Requirements |  |  |  | $6$ | $1^{5}$ | $8_{8}^{5}$ | $n^{*}$ | $\mathfrak{3}^{5}$ | s | ぶ | $8^{5}$ |
|  | Approach Lanes |  |  | 2 or | ore |  |  |  |  |  |  |  |  |
|  | Volume Level | 100\％ | 70\％ | 100\％ | 70\％ |  |  |  |  |  |  |  |  |
| $\begin{array}{ll} \mathbb{1} & 0 \\ 1 & 0 \\ \vdots & \infty \end{array}$ | Both Approaches on Major Street | 400 | 280 | 480 | 336 | 950 | 1，498 | 1，017 | 1，073 | 1，394 | 1，342 | 1，471 | 1，102 |
|  | Highest Approach on Minor Street | 120 | 84 | 160 | 112 | 64 | 110 | 50 | 45 | 48 | 48 | 56 | 46 |
|  | （volumes in veh／hr） | Minimum Requirements |  |  |  | $6^{5}$ | $\hat{v}^{\stackrel{\rightharpoonup}{p}}$ | $8^{5}$ | $n^{2}$ | $\mathfrak{K}^{\text {N }}$ | $s^{s}$ | s | $6^{8}$ |
|  | Approach Lanes | 1 |  | 2 or more |  |  |  |  |  |  |  |  |  |
|  | Volume Level | 100\％ | 70\％ | 100\％ | 70\％ |  |  |  |  |  |  |  |  |
|  | Both Approaches on Major Street | 600 | 420 | 720 | 504 | 950 | 1，498 | 1，017 | 1，073 | 1，394 | 1，342 | 1，471 | 1，102 |
|  | Highest Approach on Minor Street | 60 | 42 | 80 | 56 | 64 | 110 | 50 | 45 | 48 | 48 | 56 | 46 |

## TRAFFIC SIGNAL WARRANTS



If all four points lie above the appropriate line, then this warrant is satisfied.


FIGURE W-2: Criteria for "100\%" Volume Level


* Note: 115 vph applies as the lower threshold volume for a minor route approach with two or more lanes and 80 vph applies as the lower threshold volume threshold for a minor route approach with one lane.

FIGURE W-2: Criteria for "70\%" Volume Level
(Community less-than 10,000 population or speeds greater-than $70 \mathrm{~km} / \mathrm{hr}$ [ 40 mph ] on Major Street)


* Note: 80 vph applies as the lower threshold volume for a minor route approach with two or more lanes and

60 vph applies as the lower threshold volume threshold for a minor route approach with one lane.


## TRAFFIC SIGNAL WARRANTS

| City／Town： | Moody |
| ---: | :---: |
| County： | St．Clair |
| Division： | ALDOT East Central |
| Data Date： | Pro |
| Major Route： | US－411 |
| Minor Route： | High School Drive |

Analysis Performed By：

| DEC |
| :---: |
| $6 / 1 / 2022$ |
| 220104 |
| Overcast |



## Volume Level Criteria

1．Is the critical speed of major street traffic $>70 \mathrm{~km} / \mathrm{h}(40 \mathrm{mph})$ ？
2．Is the intersection in a built－up area or isolated community of＜10，000 population？

| X Yes | $\square \mathrm{No}$ |
| :--- | :--- |
| $\square$ Yes | $\square \mathrm{No}$ |
| $\square \mathbf{X} 70 \%$ | $\square 100 \%$ |

## WARRANT 1 －EIGHT－HOUR VEHICULAR VOLUME

Warrant 1 is satisfied if Condition A or Condition B is＂100\％＂satisfied．
Satisfied：$\quad \square$ Yes $\quad \mathbf{X}$ No
Warrant is also satisfied if both Condition A and Condition B are＂ $80 \%$＂satisfied，given
adequate trials of other remedial measures have been tried．
Adequate trial（s）of other remedial measures tried：
List Remedial Measures Tried（Required for $80 \%$ Combination of A \＆B）
$\square$
Condition A－Minimum Vehicular Volume \＆Condition B－Interruption of Continuous Traffic 100\％Satisfied：$\quad \square$ Yes $\quad \bar{X}$ No （Used if neither Condition A or B is satisfied） $\mathbf{8 0 \%}$ Satisfied：$\quad \square$ Yes $\quad \mathrm{X}$ No

|  | $\begin{gathered} \text { (volumes in veh/hr) } \\ \hline \text { Approach Lanes } \\ \hline \text { Volume Level } \end{gathered}$ | Minimum Requirements |  |  |  | Eight Highest Hours |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | at | को | $n^{5}$ | N | $\imath^{s}$ | $\mathbb{B}^{N}$ | ＊ | か |
|  |  |  |  | 2 or | ore |  |  |  |  |  |  |  |  |
|  |  | 100\％ | 70\％ | 100\％ | 70\％ |  |  |  |  |  |  |  |  |
| $\left\lvert\, \begin{array}{ll} 1 & 00 \\ 1 & 0 \\ 1 & 0 \end{array}\right.$ | Both Approaches on Major Street | 500 | 350 | 600 | 420 | 1，423 | 874 | 805 | 889 | 1，096 | 1，083 | 1，102 | 1，179 |
|  | Highest Approach on Minor Street | 150 | 105 | 200 | 140 | 280 | 39 | 41 | 41 | 135 | 322 | 74 | 107 |
|  | （volumes in veh／hr） | Minimum Requirements |  |  |  | at | कt | $n^{5}$ | $\mathbb{N}^{N}$ | $\overbrace{}^{s}$ | $\widehat{3}^{5}$ | s | ぶ |
|  | Approach Lanes | 1 |  | 2 or more |  |  |  |  |  |  |  |  |  |
|  | Volume Level | 100\％ | 70\％ | 100\％ | 70\％ |  |  |  |  |  |  |  |  |
| $\left\lvert\, \begin{array}{ll} n & \text { o } \\ 1 & 0 \\ 3 & 0 \end{array}\right.$ | Both Approaches on Major Street | 750 | 525 | 900 | 630 | 1，423 | 874 | 805 | 889 | 1，096 | 1，083 | 1，102 | 1，179 |
|  | Highest Approach on Minor Street | 75 | 53 | 100 | 70 | 280 | 39 | 41 | 41 | 135 | 322 | 74 | 107 |
|  | （volumes in veh／hr） | Minimum Requirements |  |  |  | at | of | $n^{5}$ | $n^{s}$ | $\imath^{s}$ | か | a | ぶ |
|  | Approach Lanes |  |  | 2 or | ore |  |  |  |  |  |  |  |  |
|  | Volume Level | 100\％ | 70\％ | 100\％ | 70\％ |  |  |  |  |  |  |  |  |
| $\left\lvert\, \begin{array}{ll} \mathbb{1} & 0 \\ 1 & 0 \\ \mathfrak{1} & \infty \end{array}\right.$ | Both Approaches on Major Street | 400 | 280 | 480 | 336 | 1，423 | 874 | 805 | 889 | 1，096 | 1，083 | 1，102 | 1，179 |
|  | Highest Approach on Minor Street | 120 | 84 | 160 | 112 | 280 | 39 | 41 | 41 | 135 | 322 | 74 | 107 |
|  | （volumes in veh／hr） | Minimum Requirements |  |  |  | at | of | $n^{5}$ | N | が | か | os | os |
|  | Approach Lanes | 1 |  | 2 or more |  |  |  |  |  |  |  |  |  |
|  | Volume Level | 100\％ | 70\％ | 100\％ | 70\％ |  |  |  |  |  |  |  |  |
| $\frac{m}{\sim}$ | Both Approaches on Major Street | 600 | 420 | 720 | 504 | 1，423 | 874 | 805 | 889 | 1，096 | 1，083 | 1，102 | 1，179 |
| 1 | Highest Approach on Minor Street | 60 | 42 | 80 | 56 | 280 | 39 | 41 | 41 | 135 | 322 | 74 | 107 |

## TRAFFIC SIGNAL WARRANTS

WARRANT 2 - FOUR-HOUR VEHICULAR VOLUME Satisfied: $\quad \mathrm{X}$ Yes $\square$ No
If all four points lie above the appropriate line, then this warrant is satisfied.


FIGURE W-2: Criteria for "100\%" Volume Level


* Note: 115 vph applies as the lower threshold volume for a minor route approach with two or more lanes and

80 vph applies as the lower threshold volume threshold for a minor route approach with one lane.
FIGURE W-2: Criteria for "70\%" Volume Level
(Community less-than 10,000 population or speeds greater-than $70 \mathrm{~km} / \mathrm{hr}$ [ 40 mph ] on Major Street)


* Note: 80 vph applies as the lower threshold volume for a minor route approach with two or more lanes and

60 vph applies as the lower threshold volume threshold for a minor route approach with one lane.


## Appendix F - Verbena Drive Plat and Technical Memorandum



## Technical Memorandum

## TO: Keith Hager

From: D. Scott Skipper
Date: $\quad$ March 23, 2018
Subject: US 411 at Verbena Drive/Washington Drive Moody, Alabama Traffic Signal Warrant Assessment

The document outlines preliminary traffic signal warrant analyses conducted for the U.S. Highway 411 at Verbena Drive/Washington Drive intersection in Moody, Alabama. U.S. Highway 411 is a two-lane roadway with a posted speed limit of 50 miles per hour. Both Verbena Drive and Washington Drive are two-lane local roadways providing access to primarily residential development. Currently, the study intersection is controlled by side street stop signs.

Peak period traffic counts were conducted at the study intersection from 7:00 a.m. to 9:00 a.m. and 4:00 p.m. to 6:00 p.m. Additionally, hourly approach traffic counts for a 24 -hour period were conducted for each approach of the study intersection. Traffic count data is also provided in the attached for reference.

Signal warrant evaluations were conducted for the subject intersection based on existing traffic counts and signal warrant criteria contained in the Federal Highway Administration's Manual on Uniform Traffic Control Devices, $9^{\text {th }}$ Edition (MUTCD). The evaluations consisted of comparing existing traffic volumes with signal warrant criteria of the MUTCD for Warrant 1 (Eight-Hour Vehicular Volumes), Warrant 2 (FourHour Vehicular Volume) and Warrant 3 (Peak Hour). The results of these comparisons indicate that existing traffic volumes are not sufficient to meet the minimum criteria for traffic signalization based on MUTCD criteria. For reference, the signal warrant summary for existing conditions is provided in the attachment.

Since existing volumes would not be sufficient to meet the signal warrant criteria of the MUTCD, projected volumes for the proposed residential development to the east along Verbena Drive was considered. The proposed residential includes 35 lots. Traffic projected as a result of the proposed 35 lots was estimated based upon information contained in the Institute of Transportation Engineers' publication Trip Generation. The trip generation estimates for the proposed 35 residential homes is provided in the following table.

## Trip Generation Estimates

| Land Use (ITE\#) | p Generation Estimate |  |  |  | PM Peak |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | D.U, | Weekday Trips | AM Peak |  |  |  |
|  |  |  | In | Out | In | Out |
| Single-Family Detached Housing (210) | 35 | 396 | 7 | 22 | 23 | 14 |

The trips expected to be generated by the proposed residential development was assigned to the study intersection based upon the current distribution patterns which exist.

Using projected hourly traffic volumes for the study intersection, signal warrant analyses were conducted by comparing projected hourly traffic volumes with the signal warrant criteria of the MUTCD. Based upon this comparison, it appears projected traffic volumes resulting from the additional residential homes plus existing traffic volumes would be sufficient to meet traffic signal warrant criteria. It is anticipated traffic generated by approximately $15-20$ occupied homes plus existing traffic volumes would be sufficient meet the signal warrant criteria of the MUTCD. For reference, signal warrant worksheets for projected volumes (assuming development of 35 residential homes) are provided in the attached.

It should be noted that approval of traffic signal warrants would be based on review and approval by the Alabama Department of Transportation. It should also be noted that turn lanes on U.S. Highway 411 are justified by current volumes and consideration for installation of a traffic signal should include consideration for construction of left-turn lanes and possibly right-turn lanes on U.S. Highway 411. Also, consideration for side street turn lanes should be considered.

## Appendix G - NCRS Web Soil Survey



## Farmland Classification

| Map unit symbol | Map unit name | Rating | Acres in AOI | Percent of AOI |
| :--- | :--- | :--- | ---: | ---: |
| DeB | Dewey loam, 2 to 6 <br> percent slopes | Farmland of statewide <br> importance | 12.3 | $51.5 \%$ |
| TaA | Tanyard silt loam, 0 to 2 <br> percent slopes | Farmland of statewide <br> importance | 4.7 | $19.5 \%$ |
| WaA | Wax loam, 0 to 3 <br> percent slopes | All areas are prime <br> farmland | $\mathbf{7 . 0}$ | $\mathbf{2 9 . 0 \%}$ |
| Totals for Area of Interest | $\mathbf{2 3 . 9}$ | $\mathbf{1 0 0 . 0 \%}$ |  |  |

## Description

Farmland classification identifies map units as prime farmland, farmland of statewide importance, farmland of local importance, or unique farmland. It identifies the location and extent of the soils that are best suited to food, feed, fiber, forage, and oilseed crops. NRCS policy and procedures on prime and unique farmlands are published in the "Federal Register," Vol. 43, No. 21, January 31, 1978.

## Rating Options

Aggregation Method: No Aggregation Necessary
Tie-break Rule: Lower


## Farmland Classification

| Map unit symbol | Map unit name | Rating | Acres in AOI | Percent of AOI |
| :--- | :--- | :--- | ---: | ---: |
| DeB | Dewey loam, 2 to 6 <br> percent slopes | Farmland of statewide <br> importance | 24.7 | $80.7 \%$ |
| TaA | Tanyard silt loam, 0 to 2 <br> percent slopes | Farmland of statewide <br> importance | 3.3 | $10.9 \%$ |
| WaA | Wax loam, 0 to 3 <br> percent slopes | All areas are prime <br> farmland | 2.6 | $8.4 \%$ |
| Totals for Area of Interest | $\mathbf{3 0 . 6}$ | $\mathbf{1 0 0 . 0 \%}$ |  |  |

## Description

Farmland classification identifies map units as prime farmland, farmland of statewide importance, farmland of local importance, or unique farmland. It identifies the location and extent of the soils that are best suited to food, feed, fiber, forage, and oilseed crops. NRCS policy and procedures on prime and unique farmlands are published in the "Federal Register," Vol. 43, No. 21, January 31, 1978.

## Rating Options

Aggregation Method: No Aggregation Necessary
Tie-break Rule: Lower


## Farmland Classification

| Map unit symbol | Map unit name | Rating | Acres in AOI | Percent of AOI |
| :--- | :--- | :--- | ---: | ---: |
| CaB | Cane loam, 2 to 8 <br> percent slopes | All areas are prime <br> farmland | 9.0 | $35.9 \%$ |
| McD | Minvale cherty loam, 8 <br> to 15 percent slopes | Not prime farmland | 0.8 | $3.2 \%$ |
| W | Water | Not prime farmland | 0.0 | $0.1 \%$ |
| WaA | Wax loam, 0 to 3 <br> percent slopes | All areas are prime <br> farmland | $\mathbf{1 5 . 3}$ | $60.8 \%$ |
| Totals for Area of Interest |  | $\mathbf{2 5 . 1}$ | $\mathbf{1 0 0 . 0 \%}$ |  |

## Description

Farmland classification identifies map units as prime farmland, farmland of statewide importance, farmland of local importance, or unique farmland. It identifies the location and extent of the soils that are best suited to food, feed, fiber, forage, and oilseed crops. NRCS policy and procedures on prime and unique farmlands are published in the "Federal Register," Vol. 43, No. 21, January 31, 1978.

## Rating Options

Aggregation Method: No Aggregation Necessary
Tie-break Rule: Lower

## EJScreen Report (Version 2.0)

 the User Specified Area, ALABAMA, EPA Region 4Approximate Population: 952
Input Area (sq. miles): 3.95

| Selected Variables | State <br> Percentile |  | EPA Region <br> Percentile |
| :--- | :---: | :---: | :---: |
| Environmental Justice Indexes |  | USA <br> Percentile |  |
| EJ Index for Particulate Matter 2.5 | 2 | 3 |  |
| EJ Index for Ozone | 3 | 3 | 2 |
| EJ Index for 2017 Diesel Particulate Matter* | 4 | 5 | 3 |
| EJ Index for 2017 Air Toxics Cancer Risk* | 2 | 2 | 4 |
| EJ Index for 2017 Air Toxics Respiratory HI |  | 1 |  |
| EJ Index for Traffic Proximity | 2 | 2 | 1 |
| EJ Index for Lead Paint | 20 | 23 | 5 |
| EJ Index for Superfund Proximity | 5 | 5 | 30 |
| EJ Index for RMP Facility Proximity | 4 | 20 | 8 |
| EJ Index for Hazardous Waste Proximity | 15 | 13 | 9 |
| EJ Index for Underground Storage Tanks | 13 | 9 | 9 |
| EJ Index for Wastewater Discharge |  |  | 23 |

EJ Index for the Selected Area Compared to All People's Blockgroups in the State/Region/US


State Percentile $\quad$ Regional Percentile $\square$ USA Percentile

[^1]
## EJScreen Report (Version 2.0)

 the User Specified Area, ALABAMA, EPA Region 4
## Approximate Population: 952

Input Area (sq. miles): 3.95


## Sites reporting to EPA

| Superfund NPL | 0 |
| :--- | :--- |
| Hazardous Waste Treatment, Storage, and Disposal Facilities (TSDF) | 0 |

EJScreen Report (Version 2.0)<br>the User Specified Area, ALABAMA, EPA Region 4<br>Approximate Population: 952<br>Input Area (sq. miles): 3.95

| Selected Variables | Value | State <br> Avg. | \%ile in <br> State | EPA Region Avg. | \%ile in EPA <br> Region | USA <br> Avg. | \%ile in USA |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Pollution and Sources |  |  |  |  |  |  |  |
| Particulate Matter $2.5\left(\mu \mathrm{~g} / \mathrm{m}^{3}\right)$ | 9.33 | 8.9 | 82 | 8.18 | 89 | 8.74 | 70 |
| Ozone (ppb) | 41.9 | 39.1 | 80 | 37.9 | 74 | 42.6 | 47 |
| 2017 Diesel Particulate Matter* ( $\mu \mathrm{g} / \mathrm{m}^{3}$ ) | 0.215 | 0.216 | 60 | 0.261 | <50th | 0.295 | <50th |
| 2017 Air Toxics Cancer Risk* (lifetime risk per million) | 40 | 34 | 98 | 31 | 95-100th | 29 | 95-100th |
| 2017 Air Toxics Respiratory HI* | 0.5 | 0.47 | 90 | 0.4 | 95-100th | 0.36 | 90-95th |
| Traffic Proximity (daily traffic count/distance to road) | 35 | 230 | 31 | 430 | 25 | 710 | 18 |
| Lead Paint (\% Pre-1960 Housing) | 0.073 | 0.18 | 37 | 0.15 | 50 | 0.28 | 34 |
| Superfund Proximity (site count/km distance) | 0.058 | 0.054 | 73 | 0.083 | 63 | 0.13 | 47 |
| RMP Facility Proximity (facility count/km distance) | 0.1 | 0.41 | 30 | 0.6 | 20 | 0.75 | 15 |
| Hazardous Waste Proximity (facility count/km distance) | 0.31 | 0.83 | 46 | 0.62 | 59 | 2.2 | 37 |
| Underground Storage Tanks (count/km²) | 0.39 | 1.7 | 42 | 3.5 | 33 | 3.9 | 33 |
| Wastewater Discharge (toxicity-weighted concentration/m distance) | 0.0036 | 0.42 | 68 | 0.45 | 73 | 12 | 60 |
| Socioeconomic Indicators |  |  |  |  |  |  |  |
| Demographic Index | 17\% | 36\% | 18 | 37\% | 16 | 36\% | 23 |
| People of Color | 11\% | 34\% | 23 | 39\% | 20 | 40\% | 23 |
| Low Income | 22\% | 37\% | 25 | 35\% | 29 | 31\% | 39 |
| Unemployment Rate | 4\% | 6\% | 41 | 6\% | 41 | 5\% | 43 |
| Linguistically Isolated | 1\% | 1\% | 73 | 3\% | 53 | 5\% | 47 |
| Less Than High School Education | 9\% | 14\% | 35 | 13\% | 41 | 12\% | 48 |
| Under Age 5 | 8\% | 6\% | 70 | 6\% | 72 | 6\% | 70 |
| Over Age 64 | 14\% | 17\% | 37 | 17\% | 43 | 16\% | 47 |

*Diesel particular matter, air toxics cancer risk, and air toxics respiratory hazard index are from the EPA's 2017 Air Toxics Data Update, which is the Agency's ongoing, comprehensive evaluation of air toxics in the United States. This effort aims to prioritize air toxics, emission sources, and locations of interest for further study. It is important to remember that the air toxics data presented here provide broad estimates of health risks over geographic areas of the country, not definitive risks to specific individuals or locations. Cancer risks and hazard indices from the Air Toxics Data Update are reported to one significant figure and any additional significant figures here are due to rounding. More information on the Air Toxics Data Update can be found at: https://www.epa.gov/haps/air-toxics-data-update.

For additional information, see: www.epa.gov/environmentaljustice

[^2]
## Appendix H - Future Turn Lane Warrant Evaluation Reports

Figure 2-6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-controlled intersection.
INPUT

| Roadway geometry: | Variable | 2-rane roadway |
| :--- | :---: | :---: |
|  |  |  |
| Major-road speed, mph: | 50 |  |
| Major-road volume (one direction), veh/h: | 1231 |  |
| Right-turn volume, veh/h: | 5 |  |

OUTPUT

| Variable | Value |
| :--- | :---: |
| Limiting right-turn volume, veh/h: | 8 |
| Guidance for determining the need for a major-road <br> right-turn bay for a 2-lane roadway: |  |
| Do NOT add right-turn bay. |  |



Figure 2-6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-controlled intersection.

OUTPUT

| Variable | Value |
| :--- | :---: |
| Limiting right-turn volume, veh/h: | 15 |
| Guidance for determining the need for a major-road <br> right-turn bay for a 2-lane roadway: |  |
| Add right-turn bay. |  |



Figure 2-6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-controlled intersection.

| Roadway geometry: | [\|l 2-rane roadway $\quad$-1] |  |
| :---: | :---: | :---: |
| Variable |  | Value |
| Major-road speed, mph: |  | 55 |
| Major-road volume (one direction), veh/h: |  | 408 |
| Right-turn volume, veh/h: |  | 0 |
| OUTPUT |  |  |
| Variable |  | Value |
| Limiting right-turn volume, veh/h: |  | 18 |
| Guidance for determining the need for a major-road right-turn bay for a 2-lane roadway: |  |  |
| Do NOT add right-turn bay. |  |  |



Figure 2-5. Guideline for determining the need for a major-road left-turn bay at a two-way stop-controlled intersection.

## 2-lane roadway (English)

INPUT

| Variable | Value |
| :--- | :---: |
| $85^{\text {th }}$ percentile speed, $\mathrm{mph}:$ | 55 |
| Percent of left-turns in advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right), \%:$ | $0 \%$ |
| Advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 1151 |
| Opposing volume $\left(\mathrm{V}_{\mathrm{O}}\right)$, veh $/ \mathrm{h}:$ | 408 |

OUTPUT

| Variable | Value |  |
| :--- | :---: | :---: |
| Limiting advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 1697 |  |
| Guidance for determining the need for a major-road left-turn bay: |  |  |
| Left-turn treatment NOT warranted. |  |  |



CALIBRATION CONSTANTS

| Variable | Value |
| :--- | :---: |
| Average time for making left-turn, s: | 3.0 |
| Critical headway, s: | 5.0 |
| Average time for left-turn vehicle to clear the advancing lane, s: | 1.9 |

Figure 2-6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-controlled intersection.
INPUT

| Roadway geometry: | Variable | 2-tane roadway |
| :--- | :--- | :---: |
| Major-road speed, mph: | 55 |  |
| Major-road volume (one direction), veh/h: | 1037 |  |
| Right-turn volume, veh/h: | 1 |  |

OUTPUT

| Variable | Value |
| :--- | :---: |
| Limiting right-turn volume, veh/h: | 9 |
| Guidance for determining the need for a major-road <br> right-turn bay for a 2-lane roadway: |  |
| Do NOT add right-turn bay. |  |



Figure 2-5. Guideline for determining the need for a major-road left-turn bay at a two-way stop-controlled intersection.

## 2-lane roadway (English)

INPUT

| Variable | Value |
| :--- | :---: |
| $85^{\text {th }}$ percentile speed, $\mathrm{mph}:$ | 55 |
| Percent of left-turns in advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right), \%:$ | $2 \%$ |
| Advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 511 |
| Opposing volume $\left(\mathrm{V}_{\mathrm{O}}\right)$, veh $/ \mathrm{h}:$ | 1038 |

OUTPUT

| Variable |  |  |  | Value |
| :--- | :---: | :---: | :---: | :---: |
| Limiting advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 372 |  |  |  |
| Guidance for determining the need for a major-road left-turn bay: |  |  |  |  |
| Left-turn treatment warranted. |  |  |  |  |



CALIBRATION CONSTANTS

| Variable | Value |
| :--- | :---: |
| Average time for making left-turn, s: | 3.0 |
| Critical headway, s: | 5.0 |
| Average time for left-turn vehicle to clear the advancing lane, s: | 1.9 |

Figure 2-6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-controlled intersection.

OUTPUT

| Variable | Value |
| :--- | :---: |
| Limiting right-turn volume, veh/h: | 19 |
| Guidance for determining the need for a major-road <br> right-turn bay for a 2-lane roadway: |  |
| Add right-turn bay. |  |



## AM Future

Figure 2-6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-controlled intersection.
INPUT

| Roadway geometry: | Variable | 2-lane roadway |
| :--- | :--- | :---: |
|  |  | Value |
| Major-road speed, mph: | 50 |  |
| Major-road volume (one direction), veh/h: | 908 |  |
| Right-turn volume, veh/h: | 13 |  |

OUTPUT

| Variable | Value |
| :--- | :---: |
| Limiting right-turn volume, veh/h: | 12 |
| Guidance for determining the need for a major-road <br> right-turn bay for a 2-lane roadway: |  |
| Add right-turn bay. |  |



Figure 2-6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-controlled intersection.
INPUT

| Roadway geometry: | Variable | 2-rane roadway |
| :--- | :---: | :---: |
|  |  |  |
| Major-road speed, mph: | 50 |  |
| Major-road volume (one direction), veh/h: | 485 |  |
| Right-turn volume, veh/h: | 16 |  |

OUTPUT

| Variable | Value |
| :--- | :---: |
| Limiting right-turn volume, veh/h: | 25 |
| Guidance for determining the need for a major-road <br> right-turn bay for a 2-lane roadway: |  |
| Do NOT add right-turn bay. |  |



Figure 2-5. Guideline for determining the need for a major-road left-turn bay at a two-way stop-controlled intersection.

2-lane roadway (English)
INPUT

| Variable | Value |
| :--- | :---: |
| $85^{\text {th }}$ percentile speed, mph: | 55 |
| Percent of left-turns in advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right), \%:$ | $1 \%$ |
| Advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 421 |
| Opposing volume $\left(\mathrm{V}_{\mathrm{O}}\right)$, veh $/ \mathrm{h}:$ | 1164 |

OUTPUT

| Variable | Value |  |
| :--- | :---: | :---: |
| Limiting advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 377 |  |
| Guidance for determining the need for a major-road left-turn bay: |  |  |
| Left-turn treatment warranted. |  |  |

CALIBRATION CONSTANTS

| Variable | Value |
| :--- | :---: |
| Average time for making left-turn, s: | 3.0 |
| Critical headway, s: | 5.0 |
| Average time for left-turn vehicle to clear the advancing lane, s: | 1.9 |

Figure 2-6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-controlled intersection.
INPUT

| Roadway geometry: | 2-lane roadway |
| :--- | :---: |
| Variable | Value |
| Major-road speed, mph: | 55 |
| Major-road volume (one direction), veh/h: | 421 |
| Right-turn volume, veh/h: | 13 |

OUTPUT

| Variable | Value |
| :--- | :---: |
| Limiting right-turn volume, veh/h: | 18 |
| Guidance for determining the need for a major-road <br> right-turn bay for a 2-lane roadway: |  |
| Do NOT add right-turn bay. |  |

Figure 2-5. Guideline for determining the need for a major-road left-turn bay at a two-way stop-controlled intersection.

## 2-lane roadway (English)

INPUT

| Variable | Value |
| :--- | :---: |
| $85^{\text {th }}$ percentile speed, $\mathrm{mph}:$ | 55 |
| Percent of left-turns in advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right), \%:$ | $0 \%$ |
| Advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh $/ \mathrm{h}:$ | 1164 |
| Opposing volume $\left(\mathrm{V}_{\mathrm{O}}\right)$, veh $/ \mathrm{h}:$ | 416 |

OUTPUT

| Variable | Value |  |
| :--- | :---: | :---: |
| Limiting advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 1466 |  |
| Guidance for determining the need for a major-road left-turn bay: |  |  |
| Left-turn treatment NOT warranted. |  |  |



CALIBRATION CONSTANTS

| Variable | Value |
| :--- | :---: |
| Average time for making left-turn, s: | 3.0 |
| Critical headway, s: | 5.0 |
| Average time for left-turn vehicle to clear the advancing lane, s: | 1.9 |

Figure 2-6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-controlled intersection.

OUTPUT

| Variable | Value |
| :--- | :---: |
| Limiting right-turn volume, veh/h: | 8 |
| Guidance for determining the need for a major-road <br> right-turn bay for a 2-lane roadway: |  |
| Do NOT add right-turn bay. |  |



Figure 2-5. Guideline for determining the need for a major-road left-turn bay at a two-way stop-controlled intersection.

## 2-lane roadway (English)

INPUT

| Variable | Value |
| :--- | :---: |
| $85^{\text {th }}$ percentile speed, $\mathrm{mph}:$ | 55 |
| Percent of left-turns in advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right), \%:$ | $1 \%$ |
| Advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 1075 |
| Opposing volume $\left(\mathrm{V}_{\mathrm{O}}\right)$, veh $/ \mathrm{h}:$ | 501 |

OUTPUT

| Variable |  |  |  | Value |
| :--- | :---: | :---: | :---: | :---: |
| Limiting advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 669 |  |  |  |
| Guidance for determining the need for a major-road left-turn bay: |  |  |  |  |
| Left-turn treatment warranted. |  |  |  |  |



CALIBRATION CONSTANTS

| Variable | Value |
| :--- | :---: |
| Average time for making left-turn, s: | 3.0 |
| Critical headway, s: | 5.0 |
| Average time for left-turn vehicle to clear the advancing lane, s: | 1.9 |

Figure 2-5. Guideline for determining the need for a major-road left-turn bay at a two-way stop-controlled intersection.

2-lane roadway (English)
INPUT

| Variable | Value |
| :--- | :---: |
| $85^{\text {th }}$ percentile speed, $\mathrm{mph}:$ | 55 |
| Percent of left-turns in advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right), \%:$ | $1 \%$ |
| Advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 506 |
| Opposing volume $\left(\mathrm{V}_{\mathrm{O}}\right)$, veh $/ \mathrm{h}:$ | 1059 |

## OUTPUT

| Variable | Value |
| :--- | :---: |
| Limiting advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 457 |
| Guidance for determining the need for a major-road left-turn bay: |  |
| Left-turn treatment warranted. |  |



CALIBRATION CONSTANTS

| Variable | Value |
| :--- | :---: |
| Average time for making left-turn, s: | 3.0 |
| Critical headway, s: | 5.0 |
| Average time for left-turn vehicle to clear the advancing lane, s: | 1.9 |

Figure 2-6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-controlled intersection.
INPUT

| Roadway geometry: | Variable | 2-tane roadway |
| :--- | :--- | :---: |
| Major-road speed, mph: | 55 |  |
| Major-road volume (one direction), veh/h: | 506 |  |
| Right-turn volume, veh/h: | 4 |  |

OUTPUT

| Variable | Value |
| :--- | :---: |
| Limiting right-turn volume, veh/h: | 16 |
| Guidance for determining the need for a major-road <br> right-turn bay for a 2-lane roadway: |  |
| Do NOT add right-turn bay. |  |



Figure 2-6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-controlled intersection.
INPUT

| Roadway geometry: | Variable | 2-rane roadway |
| :--- | :---: | :---: |
|  |  |  |
| Major-road speed, mph: | 50 |  |
| Major-road volume (one direction), veh/h: | 1072 |  |
| Right-turn volume, veh/h: | 1 |  |

OUTPUT

| Variable | Value |
| :--- | :---: |
| Limiting right-turn volume, veh/h: | 10 |
| Guidance for determining the need for a major-road <br> right-turn bay for a 2-lane roadway: |  |
| Do NOT add right-turn bay. |  |



Figure 2-6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-controlled intersection.
INPUT

| Roadway geometry: | Variable | 2-lane roadway |
| :--- | :--- | :---: |
| Major-road speed, mph: | 50 |  |
| Major-road volume (one direction), veh/h: | 1072 |  |
| Right-turn volume, veh/h: | 1 |  |

OUTPUT

| Variable | Value |
| :--- | :---: |
| Limiting right-turn volume, veh/h: | 10 |
| Guidance for determining the need for a major-road <br> right-turn bay for a 2-lane roadway: |  |
| Do NOT add right-turn bay. |  |



Figure 2-6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-controlled intersection.
INPUT

| Roadway geometry: | Variable | 2-lane roadway |
| :--- | :--- | :---: |
| Major-road speed, mph: | Value |  |
| Major-road volume (one direction), veh/h: | 55 |  |
| Right-turn volume, veh/h: | 419 |  |

OUTPUT

| Variable | Value |
| :--- | :---: |
| Limiting right-turn volume, veh/h: | 18 |
| Guidance for determining the need for a major-road <br> right-turn bay for a 2-lane roadway: |  |
| Do NOT add right-turn bay. |  |



Figure 2-5. Guideline for determining the need for a major-road left-turn bay at a two-way stop-controlled intersection.

## 2-lane roadway (English)

INPUT

| Variable | Value |
| :--- | :---: |
| $85^{\text {th }}$ percentile speed, $\mathrm{mph}:$ | 55 |
| Percent of left-turns in advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right), \%:$ | $1 \%$ |
| Advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 1043 |
| Opposing volume $\left(\mathrm{V}_{\mathrm{O}}\right)$, veh $/ \mathrm{h}:$ | 400 |

OUTPUT

| Variable |  |  | Value |
| :--- | :---: | :---: | :---: |
| Limiting advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 877 |  |  |
| Guidance for determining the need for a major-road left-turn bay: |  |  |  |
| Left-turn treatment warranted. |  |  |  |



CALIBRATION CONSTANTS

| Variable | Value |
| :--- | :---: |
| Average time for making left-turn, s: | 3.0 |
| Critical headway, s: | 5.0 |
| Average time for left-turn vehicle to clear the advancing lane, s: | 1.9 |

Figure 2-5. Guideline for determining the need for a major-road left-turn bay at a two-way stop-controlled intersection.

## 2-lane roadway (English)

INPUT

| Variable | Value |
| :--- | :---: |
| $85^{\text {th }}$ percentile speed, $\mathrm{mph}:$ | 55 |
| Percent of left-turns in advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right), \%:$ | $1 \%$ |
| Advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh $/ \mathrm{h}:$ | 518 |
| Opposing volume $\left(\mathrm{V}_{\mathrm{O}}\right)$, veh $/ \mathrm{h}:$ | 914 |

OUTPUT

| Variable | Value |  |
| :--- | :---: | :---: |
| Limiting advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 523 |  |
| Guidance for determining the need for a major-road left-turn bay: |  |  |
| Left-turn treatment NOT warranted. |  |  |



CALIBRATION CONSTANTS

| Variable | Value |
| :--- | :---: |
| Average time for making left-turn, s: | 3.0 |
| Critical headway, s: | 5.0 |
| Average time for left-turn vehicle to clear the advancing lane, s: | 1.9 |

Figure 2-5. Guideline for determining the need for a major-road left-turn bay at a two-way stop-controlled intersection.

## 2-lane roadway (English)

INPUT

| Variable | Value |
| :--- | :---: |
| $85^{\text {th }}$ percentile speed, $\mathrm{mph}:$ | 50 |
| Percent of left-turns in advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right), \%:$ | $1 \%$ |
| Advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 518 |
| Opposing volume $\left(\mathrm{V}_{\mathrm{O}}\right)$, veh $/ \mathrm{h}:$ | 980 |

OUTPUT

| Variable |  |  |
| :--- | :---: | :---: |
| Limiting advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 537 |  |
| Guidance for determining the need for a major-road left-turn bay: |  |  |
| Left-turn treatment NOT warranted. |  |  |



CALIBRATION CONSTANTS

| Variable | Value |
| :--- | :---: |
| Average time for making left-turn, s: | 3.0 |
| Critical headway, s: | 5.0 |
| Average time for left-turn vehicle to clear the advancing lane, s: | 1.9 |

## AM Future

Figure 2-6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-controlled intersection.
INPUT

| Roadway geometry: | V-lane roadway |  |
| :--- | :--- | :---: |
| Variable |  | Value |
| Major-road speed, mph: | 50 |  |
| Major-road volume (one direction), veh/h: | 980 |  |
| Right-turn volume, veh/h: | 0 |  |

OUTPUT

| Variable | Value |
| :--- | :---: |
| Limiting right-turn volume, veh/h: | 11 |
| Guidance for determining the need for a major-road <br> right-turn bay for a 2-lane roadway: |  |
| Do NOT add right-turn bay. |  |



Figure 2-5. Guideline for determining the need for a major-road left-turn bay at a two-way stop-controlled intersection.

## 2-lane roadway (English)

INPUT

| Variable | Value |
| :--- | :---: |
| $85^{\text {th }}$ percentile speed, $\mathrm{mph}:$ | 50 |
| Percent of left-turns in advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right), \%:$ | $1 \%$ |
| Advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 925 |
| Opposing volume $\left(\mathrm{V}_{\mathrm{O}}\right)$, veh $/ \mathrm{h}:$ | 518 |

OUTPUT

| Variable | Value |
| :--- | :---: |
| Limiting advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 849 |
| Guidance for determining the need for a major-road left-turn bay: |  |
| Left-turn treatment warranted. |  |



CALIBRATION CONSTANTS

| Variable | Value |
| :--- | :---: |
| Average time for making left-turn, s: | 3.0 |
| Critical headway, s: | 5.0 |
| Average time for left-turn vehicle to clear the advancing lane, s: | 1.9 |

Figure 2-6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-controlled intersection.
INPUT

| Roadway geometry: | Variable | Value |
| :--- | :---: | :---: |
| Major-road speed, mph: | 50 |  |
| Major-road volume (one direction), veh/h: | 518 |  |
| Right-turn volume, veh/h: | 1 |  |

OUTPUT

| Variable | Value |
| :--- | :---: |
| Limiting right-turn volume, veh/h: | 23 |
| Guidance for determining the need for a major-road <br> right-turn bay for a 2-lane roadway: |  |
| Do NOT add right-turn bay. |  |



Figure 2-6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-controlled intersection.
INPUT

| Roadway geometry: | Variable | 2-tane roadway |
| :--- | :--- | :---: |
| Major-road speed, mph: | 50 |  |
| Major-road volume (one direction), veh/h: | 1134 |  |
| Right-turn volume, veh/h: | 13 |  |

OUTPUT

| Variable | Value |
| :--- | :---: |
| Limiting right-turn volume, veh/h: | 9 |
| Guidance for determining the need for a major-road <br> right-turn bay for a 2-lane roadway: |  |
| Add right-turn bay. |  |



Figure 2-6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-controlled intersection.
INPUT

| Roadway geometry: | Variable | 2-rane roadway |
| :--- | :---: | :---: |
|  |  |  |
| Major-road speed, mph: | 50 |  |
| Major-road volume (one direction), veh/h: | 700 |  |
| Right-turn volume, veh/h: | 10 |  |

OUTPUT

| Variable | Value |
| :--- | :---: |
| Limiting right-turn volume, veh/h: | 16 |
| Guidance for determining the need for a major-road <br> right-turn bay for a 2-lane roadway: |  |
| Do NOT add right-turn bay. |  |

 CELEBRATING 50 YEARS

## Appendix I - Future Conditions Capacity Analysis Reports

| Movement | SEL | SET | SER | NWL | NWT | NWR | NEL | NET | NER | SWL | SWT | SWR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | ¢ |  |  | \$ |  | \% | $\uparrow$ | 「 | ${ }^{7}$ | F |  |
| Traffic Volume (veh/h) | 26 | 1 | 41 | 99 | 0 | 39 | 6 | 707 | 34 | 21 | 1100 | 13 |
| Future Volume (veh/h) | 26 | 1 | 41 | 99 | 0 | 39 | 6 | 707 | 34 | 21 | 1100 | 13 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate, veh/h | 28 | 1 | 45 | 108 | 0 | 42 | 7 | 768 | 37 | 23 | 1196 | 14 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, \% | 2 | 2 |  | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 112 | 25 | 123 | 203 | 2 | 52 | 164 | 1275 | 1080 | 438 | 1286 | 15 |
| Arrive On Green | 0.12 | 0.12 | 0.12 | 0.12 | 0.00 | 0.12 | 0.01 | 0.68 | 0.68 | 0.02 | 0.70 | 0.70 |
| Sat Flow, veh/h | 451 | 208 | 1024 | 1093 | 20 | 433 | 1781 | 1870 | 1585 | 1781 | 1845 | 22 |
| Grp Volume(v), veh/h | 74 | 0 | 0 | 150 | 0 | 0 | 7 | 768 | 37 | 23 | 0 | 1210 |
| Grp Sat Flow(s),veh/h/n | 1683 | 0 | 0 | 1546 | 0 | 0 | 1781 | 1870 | 1585 | 1781 | 0 | 1866 |
| Q Serve(g_s), s | 0.0 | 0.0 | 0.0 | 4.5 | 0.0 | 0.0 | 0.1 | 19.1 | 0.7 | 0.3 | 0.0 | 48.1 |
| Cycle Q Clear(g_c), s | 3.5 | 0.0 | 0.0 | 7.9 | 0.0 | 0.0 | 0.1 | 19.1 | 0.7 | 0.3 | 0.0 | 48.1 |
| Prop In Lane | 0.38 |  | 0.61 | 0.72 |  | 0.28 | 1.00 |  | 1.00 | 1.00 |  | 0.01 |
| Lane Grp Cap(c), veh/h | 259 | 0 | 0 | 257 | 0 | 0 | 164 | 1275 | 1080 | 438 | 0 | 1301 |
| V/C Ratio(X) | 0.29 | 0.00 | 0.00 | 0.58 | 0.00 | 0.00 | 0.04 | 0.60 | 0.03 | 0.05 | 0.00 | 0.93 |
| Avail Cap(c_a), veh/h | 393 | 0 | 0 | 383 | 0 | 0 | 292 | 1519 | 1287 | 539 | 0 | 1516 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 34.9 | 0.0 | 0.0 | 36.6 | 0.0 | 0.0 | 17.0 | 7.4 | 4.5 | 6.0 | 0.0 | 11.2 |
| Incr Delay (d2), s/veh | 0.6 | 0.0 | 0.0 | 2.1 | 0.0 | 0.0 | 0.1 | 0.5 | 0.0 | 0.0 | 0.0 | 9.6 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 1.5 | 0.0 | 0.0 | 3.2 | 0.0 | 0.0 | 0.1 | 5.2 | 0.1 | 0.1 | 0.0 | 15.5 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh | 35.5 | 0.0 | 0.0 | 38.7 | 0.0 | 0.0 | 17.1 | 7.9 | 4.5 | 6.0 | 0.0 | 20.9 |
| LnGrp LOS | D | A | A | D | A | A | B | A | A | A | A | C |
| Approach Vol, veh/h |  | 74 |  |  | 150 |  |  | 812 |  |  | 1233 |  |
| Approach Delay, s/veh |  | 35.5 |  |  | 38.7 |  |  | 7.8 |  |  | 20.6 |  |
| Approach LOS |  | D |  |  | D |  |  | A |  |  | C |  |


| Timer - Assigned Phs | 1 | 2 | 4 | 5 | 6 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration (G+Y+Rc), s | 7.1 | 63.7 | 15.3 | 5.8 | 65.1 | 15.3 |
| Change Period (Y+Rc), s | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Max Green Setting (Gmax), s | 7.0 | 70.0 | 18.0 | 7.0 | 70.0 | 18.0 |
| Max Q Clear Time (g_c+11), s | 2.3 | 21.1 | 5.5 | 2.1 | 50.1 | 9.9 |
| Green Ext Time (p_c), s | 0.0 | 5.7 | 0.2 | 0.0 | 10.0 | 0.5 |

Intersection Summary
HCM 6th Ctrl Delay
HCM 6th LOS


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 6.9 |  |  |  |  |  |
| Movement | SEL | SER | NEL | NET | SWT | SWR |
| Lane Configurations | M |  |  | 4 | F |  |
| Traffic Vol, veh/h | 15 | 102 | 23 | 737 | 1226 | 5 |
| Future Vol, veh/h | 15 | 102 | 23 | 737 | 1226 | 5 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | 245 | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 16 | 111 | 25 | 801 | 1333 | 5 |





| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 8 |  |  |  |  |  |
| Movement | SEL | SER | NEL | NET | SWT | SWR |
| Lane Configurations | $\mathbf{Y}$ |  |  | 4 | 4 | $\mathbf{T}$ |
| Traffic Vol, veh/h | 60 | 15 | 8 | 729 | 1066 | 50 |
| Future Vol, veh/h | 60 | 15 | 8 | 729 | 1066 | 50 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | 245 | - | - | 245 |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 65 | 16 | 9 | 792 | 1159 | 54 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.4 |  |  |  |  |  |
| Movement | SEL | SER | NEL | NET | SWT | SWR |
| Lane Configurations | 1 |  |  | - | 个 |  |
| Traffic Vol, veh/h | 5 | 14 | 5 | 513 | 980 | 0 |
| Future Vol, veh/h | 5 | 14 | 5 | 513 | 980 | 0 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 5 | 15 | 5 | 558 | 1065 | 0 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 2.5 |  |  |  |  |  |
| Movement | SEL | SER | NEL | NET | SWT | SWR |
| Lane Configurations | M |  |  | 4 | $\mathbf{F}$ |  |
| Traffic Vol, veh/h | 28 | 65 | 19 | 505 | 895 | 13 |
| Future Vol, veh/h | 28 | 65 | 19 | 505 | 895 | 13 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | 245 | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 30 | 71 | 21 | 549 | 973 | 14 |


| Major/Minor | Minor2 |  | Major1 |  | Major2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 1571 | 980 | 987 | 0 | - | 0 |
| Stage 1 | 980 | - | - | - | - | - |
| Stage 2 | 591 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | 4.12 | - | - | - |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | 2.218 | - | - | - |
| Pot Cap-1 Maneuver | 122 | 303 | 700 | - | - | - |
| Stage 1 | 364 | - | - | - | - | - |
| Stage 2 | 553 | - | - | - | - | - |
| Platoon blocked, \% |  |  |  | - | - | - |
| Mov Cap-1 Maneuver | 118 | 303 | 700 | - | - | - |
| Mov Cap-2 Maneuver | 118 | - | - | - | - | - |
| Stage 1 | 353 | - | - | - | - | - |
| Stage 2 | 553 | - | - | - | - | - |
|  |  |  |  |  |  |  |
| Approach | SE |  | NE |  | SW |  |
| HCM Control Delay, s | 38.2 |  | 0.4 |  | 0 |  |
| HCM LOS | E |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NEL | NET SELn1 |  | SWT | SWR |
| Capacity (veh/h) |  | 700 | - | 206 | - | - |
| HCM Lane V/C Ratio |  | 0.03 | - | 0.491 | - | - |
| HCM Control Delay (s) |  | 10.3 | - | 38.2 | - | - |
| HCM Lane LOS |  | B | - | E | - | - |
| HCM 95th \%tile Q(veh) |  | 0.1 | - | 2.4 | - | - |






| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 9.6 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement N | NBL | NBT | NBR | SBL | SBT | SBR | SEL | SET | SER | NWL | NWT | NWR |  |
| Lane Configurations | ${ }^{7}$ | $\uparrow$ | F | \% | $\hat{\beta}$ |  |  | \$ |  |  | \$ |  |  |
| Traffic Vol, veh/h | 18 | 393 | 8 | , | 1029 | 11 | 30 | 1 | 88 | 31 | 0 | 1 |  |
| Future Vol, veh/h | 18 | 393 | 8 | 3 | 1029 | 11 | 30 | 1 | 88 | 31 | 0 | 1 |  |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Sign Control Fr | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |  |
| RT Channelized | - | - | None | - | - | None | - | - | None | - |  | None |  |
| Storage Length | 295 | - | 295 | 245 | - | - | - | - | - | - | - | - |  |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |  |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |  |
| Mvmt Flow | 20 | 427 | 9 | 3 | 1118 | 12 | 33 | 1 | 96 | 34 | 0 | 1 |  |



| Movement | SEL | SET | SER | NWL | NWT | NWR | NEL | NET | NER | SWL | SWT | SWR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | ${ }_{*}$ |  |  | \$ |  | ${ }^{7}$ | $\uparrow$ | F' | ${ }_{1}$ | $\hat{F}$ |  |
| Traffic Volume (veh/h) | 9 | 1 | 25 | 45 | 4 | 21 | 26 | 1022 | 98 | 16 | 674 | 10 |
| Future Volume (veh/h) | 9 | 1 | 25 | 45 | 4 | 21 | 26 | 1022 | 98 | 16 | 674 | 10 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate, veh/h | 10 | 1 | 27 | 49 | 4 | 23 | 28 | 1111 | 0 | 17 | 733 | 11 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 97 | 12 | 84 | 169 | 6 | 33 | 475 | 1238 |  | 240 | 1197 | 18 |
| Arrive On Green | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 | 0.03 | 0.66 | 0.00 | 0.02 | 0.65 | 0.65 |
| Sat Flow, veh/h | 317 | 170 | 1194 | 1010 | 82 | 474 | 1781 | 1870 | 1585 | 1781 | 1838 | 28 |
| Grp Volume(v), veh/h | 38 | 0 | 0 | 76 | 0 | 0 | 28 | 1111 | 0 | 17 | 0 | 744 |
| Grp Sat Flow(s),veh/h/ln | 1681 | 0 | 0 | 1567 | 0 | 0 | 1781 | 1870 | 1585 | 1781 | 0 | 1865 |
| Q Serve(g_s), s | 0.0 | 0.0 | 0.0 | 1.5 | 0.0 | 0.0 | 0.3 | 30.0 | 0.0 | 0.2 | 0.0 | 14.0 |
| Cycle Q Clear(g_c), s | 1.3 | 0.0 | 0.0 | 2.8 | 0.0 | 0.0 | 0.3 | 30.0 | 0.0 | 0.2 | 0.0 | 14.0 |
| Prop In Lane | 0.26 |  | 0.71 | 0.64 |  | 0.30 | 1.00 |  | 1.00 | 1.00 |  | 0.01 |
| Lane Grp Cap(c), veh/h | 194 | 0 | 0 | 208 | 0 | 0 | 475 | 1238 |  | 240 | 0 | 1215 |
| V/C Ratio(X) | 0.20 | 0.00 | 0.00 | 0.37 | 0.00 | 0.00 | 0.06 | 0.90 |  | 0.07 | 0.00 | 0.61 |
| Avail Cap(c_a), veh/h | 540 | 0 | 0 | 538 | 0 | 0 | 625 | 1542 |  | 409 | 0 | 1538 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 26.8 | 0.0 | 0.0 | 27.4 | 0.0 | 0.0 | 4.8 | 8.6 | 0.0 | 10.7 | 0.0 | 6.1 |
| Incr Delay (d2), s/veh | 0.5 | 0.0 | 0.0 | 1.1 | 0.0 | 0.0 | 0.1 | 6.3 | 0.0 | 0.1 | 0.0 | 0.5 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 0.5 | 0.0 | 0.0 | 1.1 | 0.0 | 0.0 | 0.1 | 7.4 | 0.0 | 0.1 | 0.0 | 2.8 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh | 27.3 | 0.0 | 0.0 | 28.5 | 0.0 | 0.0 | 4.9 | 14.9 | 0.0 | 10.8 | 0.0 | 6.6 |
| LnGrp LOS | C | A | A | C | A | A | A | B |  | B | A | A |
| Approach Vol, veh/h |  | 38 |  |  | 76 |  |  | 1139 | A |  | 761 |  |
| Approach Delay, s/veh |  | 27.3 |  |  | 28.5 |  |  | 14.6 |  |  | 6.7 |  |
| Approach LOS |  | C |  |  | C |  |  | B |  |  | A |  |


| Timer - Assigned Phs | 1 | 2 | 4 | 5 | 6 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration (G+Y+Rc), s | 6.2 | 45.1 | 9.3 | 6.9 | 44.5 | 9.3 |
| Change Period (Y+Rc), s | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Max Green Setting (Gmax), s | 7.0 | 50.0 | 18.0 | 7.0 | 50.0 | 18.0 |
| Max Q Clear Time (g_c+11), s | 2.2 | 32.0 | 3.3 | 2.3 | 16.0 | 4.8 |
| Green Ext Time (p_c), s | 0.0 | 8.1 | 0.1 | 0.0 | 5.2 | 0.2 |

Intersection Summary
HCM 6th Ctrl Delay 12.4

HCM 6th LOS B

## Notes

Unsignalized Delay for [NER] is excluded from calculations of the approach delay and intersection delay.

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 2.7 |  |  |  |  |  |
| Movement | SEL | SER | NEL | NET | SWT | SWR |
| Lane Configurations | Ki |  | 1 | 个 | F |  |
| Traffic Vol, veh/h | 13 | 70 | 107 | 1136 | 738 | 23 |
| Future Vol, veh/h | 13 | 70 | 107 | 1136 | 738 | 23 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | 245 | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 14 | 76 | 116 | 1235 | 802 | 25 |





| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1.2 |  |  |  |  |  |
| Movement | SEL | SER | NEL | NET | SWT | SWR |
| Lane Configurations | Mr |  |  | 4 | 4 | $\mathbf{T}$ |
| Traffic Vol, veh/h | 26 | 15 | 20 | 938 | 581 | 23 |
| Future Vol, veh/h | 26 | 15 | 20 | 938 | 581 | 23 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | 245 | - | - | 245 |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 28 | 16 | 22 | 1020 | 632 | 25 |


| Major/Minor | Minor2 |  | Major1 |  | Major2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 1696 | 632 | 657 | 0 | - | 0 |
| Stage 1 | 632 | - | - | - | - | - |
| Stage 2 | 1064 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | 4.12 | - | - | - |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | 2.218 | - | - | - |
| Pot Cap-1 Maneuver | 102 | 480 | 931 | - | - | - |
| Stage 1 | 530 | - | - | - | - | - |
| Stage 2 | 332 | - | - | - | - | - |
| Platoon blocked, \% |  |  |  | - | - | - |
| Mov Cap-1 Maneuver | 100 | 480 | 931 | - | - | - |
| Mov Cap-2 Maneuver | 100 | - | - | - | - | - |
| Stage 1 | 517 | - | - | - | - | - |
| Stage 2 | 332 | - | - | - | - | - |
|  |  |  |  |  |  |  |
| Approach | SE |  | NE |  | SW |  |
| HCM Control Delay, s | 41.9 |  | 0.2 |  | 0 |  |
| HCM LOS | E |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NEL | NET SELn1 |  | SWT | SWR |
| Capacity (veh/h) |  | 931 | - | 141 | - | - |
| HCM Lane V/C Ratio |  | 0.023 | - | 0.316 | - | - |
| HCM Control Delay (s) |  | 9 | - | 41.9 | - | - |
| HCM Lane LOS |  | A | - | E | - | - |
| HCM 95th \%tile Q(veh) |  | 0.1 | - | 1.3 | - | - |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.2 |  |  |  |  |  |
| Movement | SEL | SER | NEL | NET | SWT | SWR |
| Lane Configurations | M |  |  | - | 个 |  |
| Traffic Vol, veh/h | 3 | 6 | 8 | 918 | 517 | 1 |
| Future Vol, veh/h | 3 | 6 | 8 | 918 | 517 | 1 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 3 | 7 | 9 | 998 | 562 | 1 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1.1 |  |  |  |  |  |
| Movement | SEL | SER | NEL | NET | SWT | SWR |
| Lane Configurations | M |  |  | 4 | $\mathbf{F}$ |  |
| Traffic Vol, veh/h | 14 | 45 | 39 | 882 | 468 | 16 |
| Future Vol, veh/h | 14 | 45 | 39 | 882 | 468 | 16 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | 245 | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 15 | 49 | 42 | 959 | 509 | 17 |


| Major/Minor | Minor2 |  | Major1 |  | Major2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 1561 | 518 | 526 | 0 | - | 0 |
| Stage 1 | 518 | - | - | - | - | - |
| Stage 2 | 1043 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | 4.12 | - | - | - |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | 2.218 | - | - | - |
| Pot Cap-1 Maneuver | 123 | 558 | 1041 | - | - | - |
| Stage 1 | 598 | - | - | - | - | - |
| Stage 2 | 339 | - | - | - | - | - |
| Platoon blocked, \% |  |  |  | - | - | - |
| Mov Cap-1 Maneuver | 118 | 558 | 1041 | - | - | - |
| Mov Cap-2 Maneuver | 118 | - | - | - | - | - |
| Stage 1 | 574 | - | - | - | - | - |
| Stage 2 | 339 | - | - | - | - | - |
|  |  |  |  |  |  |  |
| Approach | SE |  | NE |  | SW |  |
| HCM Control Delay, s | 20.5 |  | 0.4 |  | 0 |  |
| HCM LOS | C |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NEL | NET SELn1 |  | SWT | SWR |
| Capacity (veh/h) |  | 1041 | - | 296 | - | - |
| HCM Lane V/C Ratio |  | 0.041 | - | 0.217 | - | - |
| HCM Control Delay (s) |  | 8.6 | - | 20.5 | - | - |
| HCM Lane LOS |  | A | - | C | - | - |
| HCM 95th \%tile Q(veh) |  | 0.1 | - | 0.8 | - | - |








## Appendix J - Opinions of Probable Cost

| US-411 at Washington Drive and Verbena Drive |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Traffic Signal, Northbound Left Turn Lane, Southbound Left Turn Lane, and Northbound Right Turn Lane on US-411 |  |  |  |  |  |  |
| Item Description | Unit | Quantity | Unit Price |  | Amount |  |
| Clearing \& Grubbing (Max ALDOT Bid = \$8,000/Acre) | LS | 1 | \$ | 4,000.00 | \$ | 4,000.00 |
| Unclassified Excavation | CY | 1000 | \$ | 25.00 | \$ | 25,000.00 |
| Borrow Excavation | CY | 2500 | \$ | 25.00 | \$ | 62,500.00 |
| Micro-Milling | SY | 5600 | \$ | 5.00 | \$ | 28,000.00 |
| Wearing Surface (1.5") | TN | 668 | \$ | 200.00 | \$ | 133,650.00 |
| Upper Binder Layer (1.5") | TN | 206 | \$ | 190.00 | \$ | 39,187.50 |
| Lower Binder Layer (5") | TN | 675 | \$ | 180.00 | \$ | 121,500.00 |
| Aggregate Base (6") | SY | 2500 | \$ | 15.00 | \$ | 37,500.00 |
| Tack Coat | GAL | 1048 | \$ | 8.00 | \$ | 8,384.00 |
| Bituminous Treatment | SY | 2500 | \$ | 8.00 | \$ | 20,000.00 |
| Topsoil | CY | 500 | \$ | 35.00 | \$ | 17,500.00 |
| Temporary Seeding | AC | 2 | \$ | 1,200.00 | \$ | 2,400.00 |
| Permanent Seeding | AC | 1 | \$ | 1,200.00 | \$ | 1,200.00 |
| Curb \& Gutter | LF | 250 | \$ | 35.00 | \$ | 8,750.00 |
| Storm Pipe | LF | 75 | \$ | 150.00 | \$ | 11,250.00 |
| Storm Inlets | EA | 2 | \$ | 6,000.00 | \$ | 12,000.00 |
| Traffic Stripe, Markings, Legends | LS | 1 | \$ | 33,500.00 | \$ | 33,500.00 |
| Erosion Control | LS | 1 | \$ | 30,000.00 | \$ | 30,000.00 |
| Traffic Control | LS | 1 | \$ | 40,000.00 | \$ | 40,000.00 |
| Traffic Signal | LS | 1 |  | 250,000.00 | \$ | 250,000.00 |
| Mobilization (9.7\% of Overall Cost) | LS | 1 | \$ | 61,723.19 | \$ | 61,723.19 |
| Engineering Controls (1.3\% of Overall Cost) | LS | 1 | \$ | 12,324.58 | \$ | 12,324.58 |
|  | Roadway Total |  |  |  | \$ | 960,369.27 |
|  |  | Preliminary Engineering (15\%) |  |  | \$ | 144,055.39 |
|  |  | Utility Cost: |  |  | \$ | 100,000.00 |
|  |  | Right-of-Way Cost: |  |  | \$ | - |
|  |  | Contingency (20\%) |  |  | \$ | 192,073.85 |
|  |  | Local Funds Grand Total: |  |  | \$ | 1,396,498.51 |
|  |  | CE\& and Indirect Costs (25\%) |  |  | \$ | 349,124.63 |
|  |  | Federal Funds Grand Total: |  |  | \$ | 1,745,623.14 |

NOTE: ENGINEER'S OPINION OF PROBABLE CONSTRUCTION COST PROVIDED IS MADE ON THE BASIS OF ENGINEER'S EXPERIENCES AND QUALIFICATION AND REPRESENTS ENGINEER'S BEST JUDGMENT WITHIN THE INDUSTRY. ENGINEER DOES NOT GUARANTEE THAT PROPOSALS, BIDS OR ACTUAL COST WILL NOT VARY FROM ENGINEER'S OPINION OF PROBABLE COST.

NOTE: THE TOTAL ESTIMATED PROJECT COST WAS PREPARED FOR THE 2022 PLANNING YEAR. THIS NUMBER SHOULD BE INCREASED TO ACCOUNT FOR RISING COSTS DUE TO INFLATION SHOULD THE IMPROVEMENTS NOT BE IMPLEMENTED IN 2022.


NOTE: ENGINEER'S OPINION OF PROBABLE CONSTRUCTION COST PROVIDED IS MADE ON THE BASIS OF ENGINEER'S EXPERIENCES AND QUALIFICATION AND REPRESENTS ENGINEER'S BEST JUDGMENT WITHIN THE INDUSTRY. ENGINEER DOES NOT GUARANTEE THAT PROPOSALS, BIDS OR ACTUAL COST WILL NOT VARY FROM ENGINEER'S OPINION OF PROBABLE COST.

NOTE: THE TOTAL ESTIMATED PROJECT COST WAS PREPARED FOR THE 2022 PLANNING YEAR. THIS NUMBER SHOULD BE INCREASED TO ACCOUNT FOR RISING COSTS DUE TO INFLATION SHOULD THE IMPROVEMENTS NOT BE IMPLEMENTED IN 2022.

| US-411 at James Taylor Road |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Northbound Left Turn Lane and Southbound Right Turn Lane |  |  |  |  |  |  |
| Item Description | Unit | Quantity |  | nit Price |  | Amount |
| Clearing \& Grubbing (Max ALDOT Bid = \$8,000/Acre) | LS | 1 | \$ | 8,000.00 | \$ | 8,000.00 |
| Unclassified Excavation | CY | 1000 | \$ | 25.00 | \$ | 25,000.00 |
| Borrow Excavation | CY | 2500 | \$ | 25.00 | \$ | 62,500.00 |
| Micro-Milling | SY | 3200 | \$ | 5.00 | \$ | 16,000.00 |
| Wearing Surface (1.5") | TN | 479 | \$ | 200.00 | \$ | 95,700.00 |
| Upper Binder Layer (1.5") | TN | 215 | \$ | 190.00 | \$ | 40,755.00 |
| Lower Binder Layer (5") | TN | 702 | \$ | 180.00 | \$ | 126,360.00 |
| Aggregate Base (6") | SY | 2600 | \$ | 15.00 | \$ | 39,000.00 |
| Tack Coat | GAL | 880 | \$ | 8.00 | \$ | 7,040.00 |
| Bituminous Treatment | SY | 2600 | \$ | 8.00 | \$ | 20,800.00 |
| Topsoil | CY | 400 | \$ | 35.00 | \$ | 14,000.00 |
| Temporary Seeding | AC | 2 | \$ | 1,200.00 | \$ | 2,400.00 |
| Permanent Seeding | AC | 1 | \$ | 1,200.00 | \$ | 1,200.00 |
| Storm Pipe | LF | 130 | \$ | 150.00 | \$ | 19,500.00 |
| Pipe End Treatment | EA | 4 | \$ | 2,000.00 | \$ | 8,000.00 |
| Traffic Stripe, Markings, Legends | LS | 1 | \$ | 26,500.00 | \$ | 26,500.00 |
| Erosion Control | LS | 1 | \$ | 30,000.00 | \$ | 30,000.00 |
| Traffic Control | LS | 1 | \$ | 40,000.00 | \$ | 40,000.00 |
| Mobilization (9.7\% of Overall Cost) | LS | 1 | \$ | 56,527.24 | \$ | 56,527.24 |
| Engineering Controls (1.3\% of Overall Cost) | LS | 1 | \$ | 8,310.67 | \$ | 8,310.67 |
| Roadway Total |  |  |  |  | \$ | 647,592.90 |
| Preliminary Engineering (15\%) \$ 97,138.94 |  |  |  |  |  |  |
|  |  | Utility Cost: |  |  | \$ | 200,000.00 |
|  |  | Right-of-Way Cost: |  |  | \$ | 25,000.00 |
|  |  | Contingency (20\%) |  |  | \$ | 129,518.58 |
|  |  | Local Funds Grand Total: |  |  | \$ | 1,099,250.42 |
|  |  | CE\& and Indirect Costs (25\%) |  |  | \$ | 274,812.61 |
|  |  | Federal Funds Grand Total: |  |  | \$ | 1,374,063.03 |

NOTE: ENGINEER'S OPINION OF PROBABLE CONSTRUCTION COST PROVIDED IS MADE ON THE BASIS OF ENGINEER'S EXPERIENCES AND QUALIFICATION AND REPRESENTS ENGINEER'S BEST JUDGMENT WITHIN THE INDUSTRY. ENGINEER DOES NOT GUARANTEE THAT PROPOSALS, BIDS OR ACTUAL COST WILL NOT VARY FROM ENGINEER'S OPINION OF PROBABLE COST.

NOTE: THE TOTAL ESTIMATED PROJECT COST WAS PREPARED FOR THE 2022 PLANNING YEAR. THIS NUMBER SHOULD BE INCREASED TO ACCOUNT FOR RISING COSTS DUE TO INFLATION SHOULD THE IMPROVEMENTS NOT BE IMPLEMENTED IN 2022.


[^0]:    *Note that a police officer is posted at the High School Drive intersection during the AM peak hour. Synchro results do not account for this.

[^1]:    This report shows the values for environmental and demographic indicators and EJSCREEN indexes. It shows environmental and demographic raw data (e.g., the estimated concentration of ozone in the air), and also shows what percentile each raw data value represents. These percentiles provide perspective on how the selected block group or buffer area compares to the entire state, EPA region, or nation. For example, if a given location is at the 95th percentile nationwide, this means that only 5 percent of the US population has a higher block group value than the average person in the location being analyzed. The years for which the data are available, and the methods used, vary across these indicators. Important caveats and uncertainties apply to this screening-level information, so it is essential to understand the limitations on appropriate interpretations and applications of these indicators. Please see EJSCREEN documentation for discussion of these issues before using reports.

[^2]:    
    
     screening-level information, so it is essential to understand the limitations on appropriate interpretations and applications of these indicators. Please see EJScreen documentation for discussion of these issues before using reports. This screening tool does not provide data on every environmental impact and demographic factor that may be relevant to a particular location. EJScreen outputs should be supplemented with additional information and local knowledge before taking any action to address potential EJ concerns.

